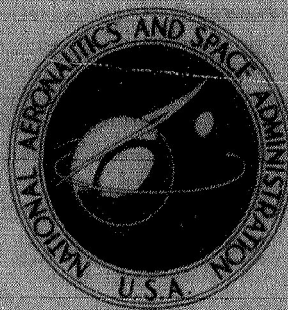


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MEMORANDUM**



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**PERFORMANCE OF LOW-PRESSURE-RATIO
FAN STAGE AT TWO OFF-DESIGN
BLADE SETTING ANGLES**

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PERFORMANCE OF LOW-PRESSURE-RATIO FAN STAGE AT TWO OFF-DESIGN BLADE SETTING ANGLES

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SUMMARY

The overall and blade-element performance are presented for a low pressure ratio fan stage at two off-design rotor blade setting angles. The rotor design tip speed is 243.8 meters per second and the weight flow per unit annulus area is 175.8 kilograms per second. Design value of weight flow and pressure ratio are 29.9 kilograms per second and 1.51, respectively. Rotor experimental peak efficiency of 0.918 occurred at a weight flow of 32.41 kilograms per second.

At design speed for a $+3^{\circ}$ (closed) rotor blade setting angle, rotor peak efficiency was 0.943 at a weight flow of 30.25 kilograms per second; for a -3° (opened) rotor blade setting angle, rotor peak efficiency was 0.907 at a weight flow of 34.01 kilograms per second.

At the peak efficiency weight flows, radial distributions of rotor suction surface incidence angles for the two off-design settings agreed within about 1° of the design reference values. Radial distributions of rotor deviation angles also agreed within $\pm 1^{\circ}$.

Rotor and stator losses were relatively low and did not vary significantly over the range of incidence angles when the rotor blade setting angle was changed.

INTRODUCTION

NASA is currently engaged in investigating short-haul-type aircraft for commercial application. These aircraft must be dependable, economical, and have an efficient and reliable propulsion system which satisfies the low noise requirement for urban communities. The aircraft engines must be capable of a variety of operating conditions including takeoff, cruise, and approach, as well as possible thrust reversal on landing.

In support of this program, the Lewis Research Center is investigating a variety of fan stages for short-haul engines. Fans under investigation may have adjustable rotor

blades to provide for varied flight demands with optimum fan performance. A reduced number of rotor blades and low solidity permit using devices for changing the rotor blade setting angle during engine operation. In addition, reverse pitch may be used for reverse thrust braking after landing thereby eliminating the weight penalty of conventional aircraft thrust reversers.

A 51-centimeter-diameter experimental fan stage incorporating provisions for manually adjusting the rotor blade setting angle has been designed, fabricated, and tested. The performance with the rotor blades at design setting angle is reported in reference 1.

This report presents the performance of the fan stage of reference 1 (designated stage 51BA-51) when the rotor blades were set at two off-design angle settings. In the first configuration (designated stage 51BC-51), the rotor blade setting angle, measured from the axial direction, was increased 3° (closed) from design. In the second configuration (designated stage 51BB-51) the rotor blade setting angle was decreased 3° (opened) from design.

Overall performance for both rotor and stage along with blade-element performance for both rotor and stator are presented for both configurations tested. The data are presented over the stable operating flow range at design speed.

AERODYNAMIC DESIGN

The design of the fan stage 51BA-51 used in this investigation is discussed in detail in reference 1. The stage was designed for an overall pressure ratio of 1.151 at a weight flow of 29.9 kilograms per second (175.8 kg/sec/m^2 of annulus area). The design rotor tip speed is 243.8 meters per second. The flow path of the stage is shown in figure 1. The convention designating rotor blade setting angles is also illustrated in figure 1. There are 12 rotor blades having a solidity of 0.65 at the tip, increasing to a value of 0.98 at the hub. Having a solidity of less than unity allows the blades to pass through "flat pitch" for reverse thrust applications. The aspect ratio of the rotor blade based on chord at the hub is 2.9. There are 32 stator blades with a hub solidity of 2.48. The stator blade aspect ratio is 3.1.

All significant design parameters for fan stage 51BA-51 are listed in tables I to V. The symbols are defined in appendix A. The equations used for calculating the overall and blade-element performance parameters are presented in appendix B. All abbreviations along with units presented in the tables are listed in appendix C.

APPARATUS AND PROCEDURE

Compressor Test Facility

The compressor stage was tested in the Lewis single-stage compressor facility, which is described in detail in reference 2. A schematic diagram of the facility is shown in figure 2. Atmospheric air enters the test facility at an inlet located on the roof of the building and flows through the flow-measuring orifice and into the plenum chamber upstream of the test stage. The air then passes through the experimental compressor stage into the collector and is exhausted to the atmosphere.

Test Stage

The rotor 51B and stator 51 are shown in figures 3 and 4, respectively. The rotor blades are mounted in a split rotor disk with the blades prevented from turning by friction pins in each half of the disk. The compression of the friction pins against the blade bases is adjustable from the front side of the rotor disk allowing the blade angle to be reset without disassembling the rotor. The ambient nonrotating radial tip clearance of the rotor was a nominal 0.05 centimeter at the stacking line. However, the radial tip clearances at the leading and trailing edges of the blades were approximately three times greater due to the convex contour of the blade tip. The stator blade leading edge was located two rotor hub chord lengths behind the rotor blade trailing edge.

Instrumentation

The fan stage weight flow was determined from measurements on a calibrated thin-plate orifice. The temperature at the orifice was measured with two chromel-constantan thermocouples. Pressures at the orifice were measured by calibrated transducers.

Radial surveys of the flow were made upstream of the rotor, between the rotor and the stator, and downstream of the stator (fig. 1). The survey probes are shown in figure 5. Total pressure, total temperature, and flow angle were measured with the combination probe (fig. 5(a)), and static pressure was measured with an 8° C-shaped wedge probe (fig. 5(b)). Each probe was positioned with a null-balancing, stream-directional sensitive control system that automatically aligned the probe to the direction of the flow. The probes were angularly pre-aligned in an air tunnel. Two combination probes and two wedge probes were used at each measuring station. The probe thermocouple material was chromel-constantan. The temperatures downstream of the rotor and stator were

measured as differences above temperatures upstream of the rotor.

Inner and outer wall static pressure taps were located at the same axial stations as the survey probes. The circumferential locations of both types of survey probes, along with inner and outer wall static pressure taps, are shown in figure 6. The combination probes downstream of the stator (station 3) were circumferentially traversed one stator blade passage (11.2°) counterclockwise from the nominal values shown. All pressures were obtained with calibrated strain-gage transducers.

An electronic speed counter, in conjunction with a magnetic pickup, was used to measure rotative speed (rpm).

The estimated errors of the data based on inherent accuracies of the instrumentation and recording system are as follows:

| | |
|--|------------|
| Weight flow, kg/sec | ± 0.3 |
| Rotative speed, rpm | ± 30 |
| Flow angle, deg | ± 1 |
| Temperature, K | ± 0.6 |
| Rotor-inlet total pressure, N/cm^2 | ± 0.01 |
| Rotor-outlet total pressure, N/cm^2 | ± 0.10 |
| Stator-outlet total pressure, N/cm^2 | ± 0.10 |
| Rotor-inlet static pressure, N/cm^2 | ± 0.04 |
| Rotor-outlet static pressure, N/cm^2 | ± 0.07 |
| Stator-outlet static pressure, N/cm^2 | ± 0.07 |

An indication of the consistency of the data can be observed by comparing the integrated weight flow at each measuring station to the orifice weight flow.

Test Procedure

The stage survey data were taken over a range of weight flows from maximum flow to the near-stall conditions at design speed. Data were recorded at nine radial positions for each weight flow.

At each radial position the two combination probes behind the stator were circumferentially traversed to nine different locations across the stator gap. The two wedge probes were set at midgap because previous studies showed that the static pressure across the stator gap was constant. Values of pressure, temperature, and flow angle were recorded at each circumferential position. At the last circumferential position, values of pressure, temperature, and flow angle were also recorded at stations 1 and 2. All probes were then traversed to the next radial position and the circumferential traverse procedure repeated.

For each configuration the backpressure on the stage was increased by closing the sleeve valve in the collector until a drop in total pressure at the blade tip was detected. This was accomplished by comparing the radial distribution of discharge total pressures between succeeding on-line computer printouts obtained as the valve was closed. This point was arbitrarily taken as the limit of stable operation at the low end of the weight flow range and usually occurred before any definite indications of stall were observed such as change in noise level or increase in blade stresses.

Calculation Procedure

Measured total temperatures and total pressures were corrected for Mach number and streamline slope. These corrections were based on instrument probe calibrations given in reference 3. The stream static pressure was corrected for Mach number and streamline slope based on an average calibration for the type of probe used.

Because of the physical construction of the C-shaped static pressure wedges, it was not possible to obtain static pressure measurements at 5, 10, and 95 percent of span. The static pressure at 95 percent of span was obtained by assuming a linear variation in static pressure between the values at the inner wall and the probe measurement at 90 percent of span. A linear variation was also assumed between the static pressure measurements at the outer wall and the 15-percent span to obtain the static pressure at 5 and 10 percent of span.

At each radial position, averaged values of the nine circumferential measurements of pressure, temperature, and flow angle downstream of the stator (station 3) were obtained. The nine values of total temperature were mass-averaged to obtain the stator-outlet total temperature presented. The nine values of total pressure were energy averaged. The measured values of pressure, temperature, and flow angle were used to calculate axial and tangential velocities at each circumferential position. The flow angles presented for each radial position were calculated based on these mass-averaged axial and tangential velocities. To obtain the overall performance, the radial values of total temperature were mass-averaged and the values of total pressure were energy averaged. At each measuring station, the integrated weight flow was computed based on the radial survey data.

The data, measured at the three measuring stations, have been translated to the blade leading and trailing edges by the method presented in reference 2.

Orifice weight flows, total pressures, static pressures, and temperatures were all corrected to standard-day conditions based on the rotor-inlet conditions.

RESULTS AND DISCUSSION

The results of this investigation are presented in three main sections. The overall performance at design speed for both rotor and stage are compared at the two off-design rotor blade settings with the overall performance at the design setting angle. Radial distributions of several performance parameters for both rotor and stator of each configuration are then compared. Finally comparisons of blade-element data for rotor and stator of each configuration are made. The data presented are computer plotted, and occasionally a data point is omitted when it falls outside the range of parameters shown in the figures.

All of the plotted data together with some additional parameters are presented in tabular form for each off-design stage configuration. The overall performance data are presented in table VI. The blade-element data are presented first for the rotor in tables VII to IX and then for the stator in tables X to XII. The definitions and units used for the tabular data are presented in appendix C.

Overall Performance

The overall performance for the rotor at the two off-design blade settings are shown in figure 7 and for the stage in figure 8. The overall performance at design rotor blade setting (ref. 1) is also shown for comparison. Data are presented for several weight flows at design speed.

The step which occurs in both rotor and stage performance curves has been discussed in reference 1; a rapid forward movement of the flow separation point on the suction surface of the rotor blade may be occurring over a small portion of the suction surface incidence range.

As was expected weight flow increased with the opened rotor blade setting angle and decreased with the closed blade setting angle. Maximum flow increased 1.5 kilograms per second with the -3° (opened) rotor blade setting angle and decreased 1.5 kilograms per second with the $+3^{\circ}$ (closed) blade setting angle. Rotor peak efficiency at design setting angle was 0.918 (ref. 1). Rotor peak efficiency increased 2.5 points for the closed rotor blade setting angle and decreased 1.1 points for the open setting angle. For the $+3^{\circ}$ (closed) rotor blade setting angle, rotor peak efficiency pressure ratio was 1.134 at a weight flow of 30.25 kilograms per second and for the -3° (opened) setting angle, 1.148 at a weight flow of 34.01 kilograms per second.

The trends in stage performance were similar to those for the rotor for corresponding changes in rotor blade setting angles.

Radial Distributions

The radial distributions of selected flow and performance parameters at design speed for both rotor and stator are shown in figures 9 and 10. The results are presented for the two off-design configurations at the peak efficiency flow rates. Radial distributions of flow and performance for the design configuration are included for reference.

Rotor. - In general, the changes in radial distribution of the flow and performance parameters occurred evenly over the entire blade span. Some small differences were noted in the extreme hub and tip regions. For example, the decrease in rotor efficiency in the hub region as the rotor is reset is the greatest as the angle is changed from $+3^{\circ}$ to design angle. At peak efficiencies the suction surface incidence angles agreed within about 1° with the reference values over the entire blade span. The diffusion factor radial distribution did not change over the range of blade setting angles although the total loss parameters showed small increases with the increases in weight flow over the range of blade setting angles tested. Deviation angles for each configuration agreed with the reference values within about 1° .

Stator. - Radial distribution of suction surface incidence angles were unchanged from design for each configuration. No significant changes from design in radial distribution of the stator performance parameters occurred with the change of rotor blade setting angles. For all three rotor setting angles, the losses seemed to rise rapidly in the hub region from 85 to 95 percent span. Losses in the tip region were also high.

Variations with Incidence Angle

The variations of selected blade-element performance parameters are presented in figure 11 for the rotor and in figure 12 for the stator. The data are presented for the two off-design configurations for 100 percent design speed at the 5, 10, 30, 50, 70, 90, and 95 percent of blade span (measured from the tip). Data for the design stage configuration is included for comparison.

Measured suction-surface incidence angles corresponding to minimum losses were not conclusively defined for either the rotor or stator. The blade elements for rotor 51B seem to be mismatched. At 90 and 95 percent spans, peak efficiency occurs near minimum flow whereas at 30, 50, and 70 percent span, it occurs near maximum flow. At 5 and 10 percent span locations, peak efficiency occurred at about midflow. This mismatch was observed with all three rotor setting angles. For each element peak efficiency was highest for the design $+3^{\circ}$ angle. This may be due to lower inlet relative Mach numbers and lower choke margins as the blades were closed down. The change

in slope of the pressure ratio curve observed in the overall rotor performance plot is also observed in the blade-element curves. The greatest changes were noted in the midspan of the blade and less pronounced in the end regions.

SUMMARY OF RESULTS

The overall and blade-element performance are presented for a low pressure ratio fan stage at two off-design rotor blade setting angles. The first fan stage rotor blade setting angle measured from the axial direction was closed 3° from design and the second was opened 3° from design. Design values of weight flow, pressure ratio, and temperature ratio are 29.9 kilograms per second, 1.151, and 1.047, respectively. The rotor design tip speed is 243.8 meters per second, and the weight flow per unit annulus area is 175.8 kilograms per second. Rotor peak efficiency for the design configuration was 0.918 at a weight flow of 32.41 kilograms per second. The following principal results were obtained:

1. At design speed, the rotor peak efficiency for the off-design fan stage with rotor blades 3° closed was 0.943 at a weight flow of 30.25 kilograms per second. The rotor peak efficiency for the off-design fan stage with rotor blades 3° opened was 0.905 at a weight flow of 34.01 kilograms per second.

2. The radial distributions of rotor suction surface incidence angles at the peak efficiency weight flows were within about 1° of the reference design values. The radial distributions of rotor deviation angles were essentially unchanged with reset (within about 1°). Stator suction surface incidence angles were unchanged with rotor blade reset.

3. Stator losses were relatively constant for each configuration.

Lewis Research Center,

National Aeronautics and Space Administration,

Cleveland, Ohio, November 5, 1976,

505-04.

APPENDIX A

SYMBOLS

| | |
|------------|---|
| A_{an} | annulus area at rotor leading edge, m^2 |
| A_f | frontal area at rotor leading edge, m^2 |
| C_p | specific heat at constant pressure, 1004 J/kg/K |
| c | aerodynamic chord, cm |
| D | diffusion factor |
| i_{mc} | mean incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, deg |
| i_{ss} | suction-surface incidence angle, angle between inlet air direction and line tangent to blade suction surface at leading edge, deg |
| N | rotative speed, rpm |
| P | total pressure, N/cm^2 |
| p | static pressure, N/cm^2 |
| r | radius, cm |
| T | total temperature, K |
| U | wheel speed, m/sec |
| V | air velocity, m/sec |
| W | weight flow, kg/sec |
| Z | axial distance referenced from rotor-blade-hub leading edge, cm |
| α_c | cone angle, deg |
| α_s | slope of streamline, deg |
| β | air angle, angle between air velocity and axial direction, deg |
| β'_c | relative meridional air angle based on cone angle, $\arctan(\tan \beta'_m \cos \alpha_c / \cos \alpha_s)$, deg |
| γ | ratio of specific heats |
| γ_b | blade setting angle |

| | |
|-----------------------|---|
| δ | ratio of rotor-inlet total pressure to standard pressure of 10.13 N/cm ² |
| δ^0 | deviation angle, angle between exit air direction and tangent to blade mean camber line at trailing edge, deg |
| η | efficiency |
| θ | ratio of rotor-inlet total temperature to standard temperature of 288.2 K |
| κ_{mc} | angle between blade mean camber line and meridional plane, deg |
| κ_{ss} | angle between blade suction-surface camber line at leading edge and meridional plane, deg |
| σ | solidity, ratio of chord to spacing |
| $\overline{\omega}$ | total loss coefficient |
| $\overline{\omega}_p$ | profile loss coefficient |
| $\overline{\omega}_s$ | shock loss coefficient |

Subscripts:

| | |
|----------|--|
| ad | adiabatic (temperature rise) |
| id | ideal |
| LE | blade leading edge |
| m | meridional direction |
| mom | momentum-rise |
| p | polytropic |
| r | radial direction |
| TE | blade trailing edge |
| tip | tip |
| z | axial direction |
| θ | tangential direction |
| 1 | instrumentation plane upstream of rotor |
| 2 | instrumentation plane between rotor and stator |
| 3 | instrumentation plane downstream of stator |

Superscript:

| | |
|---|-------------------|
| ' | relative to blade |
|---|-------------------|

APPENDIX B

EQUATIONS

Suction-surface incidence angle:

$$i_{ss} = (\beta'_c)_{LE} - \kappa_{ss} \quad (B1)$$

Mean incidence angle:

$$i_{mc} = (\beta'_c)_{LE} - (\kappa_{mc})_{LE} \quad (B2)$$

Deviation angle:

$$\delta^0 = (\beta'_c)_{TE} - (\kappa_{mc})_{TE} \quad (B3)$$

Diffusion factor:

$$D = 1 - \frac{V'_{TE}}{V'_{LE}} + \left| \frac{(rV_\theta)_{TE} - (rV_\theta)_{LE}}{(r_{TE} + r_{LE})^\sigma (V'_{LE})} \right| \quad (B4)$$

Total loss coefficient:

$$\bar{\omega} = \frac{(\mathbf{P}'_{id})_{TE} - \mathbf{P}'_{TE}}{\mathbf{P}'_{LE} - \mathbf{p}_{LE}} \quad (B5)$$

Profile loss coefficient:

$$\bar{\omega}_p = \bar{\omega} - \bar{\omega}_s \quad (B6)$$

Total loss parameter:

$$\frac{\bar{\omega} \cos (\beta'_m)_{TE}}{2\sigma} \quad (B7)$$

Profile loss parameter:

$$\frac{\overline{\omega}_p \cos(\beta_m')_{TE}}{2\sigma} \quad (B8)$$

Adiabatic (temperature-rise) efficiency:

$$\eta_{ad} = \frac{\left(\frac{P_{TE}}{P_{LE}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{T_{TE}}{T_{LE}} - 1} \quad (B9)$$

Momentum-rise efficiency:

$$\eta_{mom} = \frac{\left(\frac{P_{TE}}{P_{LE}}\right)^{(\gamma-1)/\gamma} - 1}{\frac{(UV_\theta)_{TE} - (UV_\theta)_{LE}}{T_{LE} C_p}} \quad (B10)$$

Equivalent weight flow:

$$\frac{W\sqrt{\theta}}{\delta} \quad (B11)$$

Equivalent rotative speed:

$$\frac{N}{\sqrt{\theta}} \quad (B12)$$

Weight flow per unit annulus area:

$$\frac{\frac{W\sqrt{\theta}}{\delta}}{A_{an}} \quad (B13)$$

Weight flow per unit frontal area:

$$\frac{\frac{W\sqrt{\theta}}{\delta}}{A_f} \quad (B14)$$

Head-rise coefficient:

$$\frac{C_p T_{LE}}{U_{tip}^2} \left[\left(\frac{P_{TE}}{P_{LE}} \right)^{(\gamma-1)/\gamma} - 1 \right] \quad (B15)$$

Flow coefficient:

$$\left(\frac{V_z}{U_{tip}} \right)_{LE} \quad (B16)$$

Polytropic efficiency:

$$\eta_p = \frac{\ln \left(\frac{P_{TE}}{P_{LE}} \right)^{(\gamma-1)/\gamma}}{\ln \frac{T_{TE}}{T_{LE}}} \quad (B17)$$

APPENDIX C

DEFINITIONS AND UNITS USED IN TABLES

| | |
|--------------|---|
| ABS | absolute |
| AERO CHORD | aerodynamic chord, cm |
| AREA RATIO | ratio of actual minimum flow area to critical area (where local Mach number is 1) |
| BETAM | meridional air angle, deg |
| CONE ANGLE | angle between axial direction and conical surface representing blade element, deg |
| DELTA INC | difference between mean camber blade angle and suction-surface blade angle at leading edge, deg |
| DEV | deviation angle (defined by eq. (B3)), deg |
| D-FACT | diffusion factor (defined by eq. (B4)) |
| EFF | adiabatic efficiency (defined by eq. (B9)) |
| IN | inlet (leading edge of blade) |
| INCIDENCE | incidence angle (suction surface defined by eq. (B1) and mean defined by eq. (B2)), deg |
| KIC | angle between blade mean camber line at leading edge and meridional plane, deg |
| KOC | angle between blade mean camber line at trailing edge and meridional plane, deg |
| KTC | angle between blade mean camber line at transition point and meridional plane, deg |
| LOSS COEFF | loss coefficient (total defined by eq. (B5) and profile defined by eq. (B6)) |
| LOSS PARAM | loss parameter (total defined by eq. (B7) and profile defined by eq. (B8)) |
| MERID | meridional |
| MERID VEL R | meridional velocity ratio |
| OUT | outlet (trailing edge of blade) |
| PERCENT SPAN | percent of blade span from tip at rotor outlet |

| | |
|------------------|---|
| PHISS | suction-surface camber ahead of assumed shock location, deg |
| PRESS | pressure, N/cm^2 |
| PROF | profile |
| RADII | radius, cm |
| REL | relative to blade |
| RI | inlet radius (leading edge of blade), cm |
| RO | outlet radius (trailing edge of blade), cm |
| RP | radial position |
| RPM | equivalent rotative speed, rpm |
| SETTING ANGLE | angle between aerodynamic chord and meridional plane, deg |
| SOLIDITY | ratio of aerodynamic chord to blade spacing |
| SPEED | speed, m/sec |
| SS | suction surface |
| STREAMLINE SLOPE | slope of streamline, deg |
| TANG | tangential |
| TEMP | temperature, K |
| TI | thickness of blade at leading edge, cm |
| TM | thickness of blade at maximum thickness, cm |
| TO | thickness of blade at trailing edge, cm |
| TOT | total |
| TOTAL CAMBER | difference between inlet and outlet blade mean camber lines, deg |
| VEL | velocity, m/sec |
| WT FLOW | equivalent weight flow, kg/sec |
| X FACTOR | ratio of suction-surface camber ahead of assumed shock location of multiple-circular-arc blade section to that of double-circular-arc blade section |
| ZIC | axial distance to blade leading edge from inlet, cm |
| ZMC | axial distance to blade maximum thickness point from inlet, cm |
| ZOC | axial distance to blade trailing edge from inlet, cm |
| ZTC | axial distance to transition point from inlet, cm |

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TABLE I. - DESIGN OVERALL PARAMETERS

FOR FAN STAGE 51B-51

| | |
|------------------------------------|----------|
| ROTOR TOTAL PRESSURE RATIO..... | 1.159 |
| STAGE TOTAL PRESSURE RATIO | 1.151 |
| ROTOR TOTAL TEMPERATURE RATIO..... | 1.047 |
| STAGE TOTAL TEMPERATURE RATIO | 1.047 |
| ROTOR ADIABATIC EFFICIENCY..... | 0.911 |
| STAGE ADIABATIC EFFICIENCY | 0.865 |
| ROTOR POLYTROPIC EFFICIENCY..... | 0.913 |
| STAGE POLYTROPIC EFFICIENCY | 0.868 |
| ROTOR HEAD RISE COEFFICIENT..... | 0.210 |
| STAGE HEAD RISE COEFFICIENT | 0.199 |
| FLOW COEFFICIENT..... | 0.681 |
| WT FLOW PER UNIT FRONTAL AREA | 147.704 |
| WT FLOW PER UNIT ANNULUS AREA..... | 175.838 |
| WT FLOW | 29.937 |
| RPM..... | 9167.300 |
| TIP SPEED | 243.839 |

TABLE II. - DESIGN BLADE-ELEMENT PARAMETERS FOR ROTOR 51A

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|-----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| TIP | 25.400 | 25.400 | 0. | 24.4 | 55.3 | 48.9 | 288.2 | 1.058 | 10.14 | 1.184 |
| 1 | 24.647 | 24.638 | -0. | 24.5 | 54.5 | 47.5 | 288.2 | 1.057 | 10.14 | 1.183 |
| 2 | 23.868 | 23.876 | 0. | 24.6 | 53.6 | 46.0 | 288.2 | 1.056 | 10.14 | 1.183 |
| 3 | 23.085 | 23.114 | 0. | 24.8 | 52.7 | 44.5 | 288.2 | 1.055 | 10.14 | 1.182 |
| 4 | 20.732 | 20.828 | 0. | 25.6 | 49.8 | 39.5 | 288.2 | 1.051 | 10.14 | 1.175 |
| 5 | 17.607 | 17.780 | 0. | 27.1 | 45.5 | 31.6 | 288.2 | 1.046 | 10.14 | 1.159 |
| 6 | 14.533 | 14.732 | 0. | 28.9 | 40.6 | 22.2 | 288.2 | 1.040 | 10.14 | 1.134 |
| 7 | 12.294 | 12.446 | 0. | 30.0 | 36.2 | 14.2 | 288.2 | 1.034 | 10.14 | 1.111 |
| 8 | 11.565 | 11.684 | 0. | 30.2 | 34.7 | 11.6 | 288.2 | 1.032 | 10.14 | 1.102 |
| 9 | 10.844 | 10.922 | 0. | 30.3 | 33.0 | 9.0 | 288.2 | 1.030 | 10.14 | 1.092 |
| HUB | 10.160 | 10.160 | -0. | 30.4 | 31.4 | 6.3 | 288.2 | 1.028 | 10.14 | 1.083 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|-----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| TIP | 169.0 | 167.5 | 296.7 | 231.8 | 169.0 | 152.5 | 0. | 69.2 | 243.8 | 243.8 |
| 1 | 169.0 | 168.2 | 290.8 | 226.3 | 169.0 | 153.0 | -0. | 69.8 | 236.6 | 236.5 |
| 2 | 168.9 | 168.8 | 284.7 | 220.8 | 168.9 | 153.4 | 0. | 70.4 | 229.1 | 229.2 |
| 3 | 168.8 | 169.3 | 278.6 | 215.3 | 168.8 | 153.7 | 0. | 71.1 | 221.6 | 221.9 |
| 4 | 168.0 | 170.1 | 260.5 | 198.8 | 168.0 | 153.4 | 0. | 73.5 | 199.0 | 199.9 |
| 5 | 165.9 | 169.9 | 236.8 | 177.6 | 165.9 | 151.2 | 0. | 77.5 | 169.0 | 170.7 |
| 6 | 163.0 | 168.3 | 214.6 | 159.1 | 163.0 | 147.3 | 0. | 81.4 | 139.5 | 141.4 |
| 7 | 161.0 | 166.0 | 199.6 | 148.2 | 161.0 | 143.7 | 0. | 83.0 | 118.0 | 119.5 |
| 8 | 160.5 | 164.8 | 195.2 | 145.4 | 160.5 | 142.4 | 0. | 82.9 | 111.0 | 112.2 |
| 9 | 160.2 | 163.5 | 191.0 | 142.9 | 160.2 | 141.1 | 0. | 82.5 | 104.1 | 104.9 |
| HUB | 159.8 | 162.1 | 187.2 | 140.7 | 159.8 | 139.9 | -0. | 82.0 | 97.5 | 97.5 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | STREAMLINE SLOPE | | MERID PEAK SS | |
|-----|-------------|-------|-------------|-------|---------------|-------|------------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| TIP | 0.509 | 0.490 | 0.894 | 0.678 | 0.509 | 0.446 | -0.22 | -0.28 | 0.903 | 1.233 |
| 1 | 0.509 | 0.492 | 0.876 | 0.662 | 0.509 | 0.448 | -0.07 | -0.13 | 0.906 | 1.199 |
| 2 | 0.509 | 0.494 | 0.858 | 0.647 | 0.509 | 0.449 | 0.09 | 0.03 | 0.908 | 1.166 |
| 3 | 0.509 | 0.496 | 0.840 | 0.631 | 0.509 | 0.450 | 0.27 | 0.21 | 0.910 | 1.136 |
| 4 | 0.506 | 0.500 | 0.785 | 0.584 | 0.506 | 0.451 | 0.83 | 0.78 | 0.913 | 1.015 |
| 5 | 0.499 | 0.500 | 0.713 | 0.523 | 0.499 | 0.445 | 1.46 | 1.46 | 0.912 | 0.764 |
| 6 | 0.490 | 0.497 | 0.645 | 0.470 | 0.490 | 0.435 | 1.67 | 1.76 | 0.904 | 0.645 |
| 7 | 0.484 | 0.491 | 0.600 | 0.438 | 0.484 | 0.425 | 1.31 | 1.48 | 0.892 | 0.600 |
| 8 | 0.483 | 0.488 | 0.587 | 0.430 | 0.483 | 0.422 | 1.04 | 1.20 | 0.887 | 0.587 |
| 9 | 0.481 | 0.484 | 0.574 | 0.423 | 0.481 | 0.418 | 0.70 | 0.84 | 0.881 | 0.574 |
| HUB | 0.480 | 0.481 | 0.563 | 0.417 | 0.480 | 0.415 | 0.37 | 0.47 | 0.875 | 0.563 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|-----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| TIP | 0. | -1.0 | -5.6 | 5.5 | 0.398 | 0.846 | 0.072 | 0.072 | 0.037 | 0.036 |
| 1 | 5.00 | -1.0 | -5.6 | 5.3 | 0.405 | 0.865 | 0.064 | 0.064 | 0.033 | 0.033 |
| 2 | 10.00 | -0.8 | -5.7 | 5.2 | 0.411 | 0.882 | 0.057 | 0.057 | 0.030 | 0.030 |
| 3 | 15.00 | -0.7 | -5.9 | 5.5 | 0.417 | 0.896 | 0.050 | 0.050 | 0.027 | 0.027 |
| 4 | 30.00 | -0.1 | -7.2 | 7.2 | 0.439 | 0.929 | 0.036 | 0.036 | 0.020 | 0.020 |
| 5 | 50.00 | 1.0 | -9.3 | 10.4 | 0.470 | 0.941 | 0.031 | 0.031 | 0.018 | 0.018 |
| 6 | 70.00 | 2.2 | -11.2 | 14.0 | 0.494 | 0.922 | 0.043 | 0.043 | 0.024 | 0.024 |
| 7 | 85.00 | 3.1 | -11.8 | 13.8 | 0.494 | 0.887 | 0.060 | 0.060 | 0.033 | 0.033 |
| 8 | 90.00 | 3.5 | -11.7 | 12.6 | 0.489 | 0.872 | 0.067 | 0.067 | 0.036 | 0.036 |
| 9 | 95.00 | 3.8 | -11.6 | 10.9 | 0.481 | 0.854 | 0.074 | 0.074 | 0.039 | 0.039 |
| HUB | 100.00 | 4.1 | -11.5 | 9.0 | 0.471 | 0.832 | 0.081 | 0.081 | 0.041 | 0.041 |

TABLE III. - DESIGN BLADE-ELEMENT PARAMETERS FOR STATOR 51

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|-----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| TIP | 25.400 | 25.400 | 23.4 | -0. | 23.4 | -0. | 305.0 | 1.000 | 12.00 | 0.993 |
| 1 | 24.595 | 24.608 | 23.5 | 0. | 23.5 | 0. | 304.6 | 1.000 | 11.99 | 0.994 |
| 2 | 23.861 | 23.887 | 23.6 | -0. | 23.6 | -0. | 304.2 | 1.000 | 11.99 | 0.994 |
| 3 | 23.128 | 23.166 | 23.8 | -0. | 23.8 | -0. | 303.9 | 1.000 | 11.98 | 0.994 |
| 4 | 20.917 | 20.995 | 24.7 | -0. | 24.7 | -0. | 302.8 | 1.000 | 11.91 | 0.994 |
| 5 | 17.955 | 18.080 | 26.6 | -0. | 26.6 | -0. | 301.3 | 1.000 | 11.74 | 0.993 |
| 6 | 14.946 | 15.110 | 29.0 | -0. | 29.0 | -0. | 299.6 | 1.000 | 11.50 | 0.992 |
| 7 | 12.647 | 12.787 | 30.7 | -0. | 30.7 | -0. | 298.1 | 1.000 | 11.26 | 0.990 |
| 8 | 11.870 | 11.967 | 31.1 | -0. | 31.1 | -0. | 297.4 | 1.000 | 11.17 | 0.989 |
| 9 | 11.087 | 11.125 | 31.3 | -0. | 31.3 | -0. | 296.8 | 1.000 | 11.07 | 0.987 |
| HUB | 10.160 | 10.160 | 31.6 | 0. | 31.6 | 0. | 296.0 | 1.000 | 10.96 | 0.986 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|-----|---------|-------|---------|-------|-----------|-------|----------|-----|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| TIP | 174.6 | 161.8 | 174.6 | 161.8 | 160.2 | 161.8 | 69.4 | -0. | 0. | 0. |
| 1 | 175.2 | 161.7 | 175.2 | 161.7 | 160.6 | 161.7 | 69.9 | 0. | 0. | 0. |
| 2 | 175.6 | 161.4 | 175.6 | 161.4 | 160.8 | 161.4 | 70.4 | -0. | 0. | 0. |
| 3 | 175.7 | 161.0 | 175.7 | 161.0 | 160.8 | 161.0 | 71.0 | -0. | 0. | 0. |
| 4 | 175.1 | 158.4 | 175.1 | 158.4 | 159.0 | 158.4 | 73.1 | -0. | 0. | 0. |
| 5 | 171.6 | 151.7 | 171.6 | 151.7 | 153.5 | 151.7 | 76.7 | -0. | 0. | 0. |
| 6 | 165.6 | 140.7 | 165.6 | 140.7 | 144.9 | 140.7 | 80.2 | -0. | 0. | 0. |
| 7 | 160.0 | 128.1 | 160.0 | 128.1 | 137.6 | 128.1 | 81.7 | -0. | 0. | 0. |
| 8 | 158.2 | 122.2 | 158.2 | 122.2 | 135.5 | 122.2 | 81.6 | -0. | 0. | 0. |
| 9 | 156.3 | 115.5 | 156.3 | 115.5 | 133.5 | 115.5 | 81.3 | -0. | 0. | 0. |
| HUB | 154.1 | 107.8 | 154.1 | 107.8 | 131.2 | 107.8 | 80.8 | 0. | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | STREAMLINE SLOPE | | MERID PEAK SS | |
|-----|-------------|-------|-------------|-------|---------------|-------|------------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| TIP | 0.512 | 0.472 | 0.512 | 0.472 | 0.469 | 0.472 | -0.07 | -0.04 | 1.010 | 0.512 |
| 1 | 0.514 | 0.472 | 0.514 | 0.472 | 0.471 | 0.472 | 0.10 | 0.13 | 1.007 | 0.514 |
| 2 | 0.515 | 0.472 | 0.515 | 0.472 | 0.472 | 0.472 | 0.24 | 0.27 | 1.004 | 0.515 |
| 3 | 0.516 | 0.471 | 0.516 | 0.471 | 0.472 | 0.471 | 0.38 | 0.41 | 1.001 | 0.516 |
| 4 | 0.515 | 0.464 | 0.515 | 0.464 | 0.468 | 0.464 | 0.79 | 0.81 | 0.996 | 0.515 |
| 5 | 0.506 | 0.444 | 0.506 | 0.444 | 0.452 | 0.444 | 1.30 | 1.30 | 0.988 | 0.506 |
| 6 | 0.489 | 0.412 | 0.489 | 0.412 | 0.427 | 0.412 | 1.68 | 1.61 | 0.971 | 0.489 |
| 7 | 0.473 | 0.375 | 0.473 | 0.375 | 0.406 | 0.375 | 1.44 | 1.31 | 0.931 | 0.473 |
| 8 | 0.467 | 0.358 | 0.467 | 0.358 | 0.400 | 0.358 | 1.02 | 0.91 | 0.902 | 0.467 |
| 9 | 0.462 | 0.338 | 0.462 | 0.338 | 0.395 | 0.338 | 0.44 | 0.34 | 0.865 | 0.462 |
| HUB | 0.456 | 0.315 | 0.456 | 0.315 | 0.388 | 0.315 | -0.26 | -0.31 | 0.821 | 0.456 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|-----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| TIP | 0. | 9.2 | -0.0 | 4.1 | 0.274 | 0. | 0.041 | 0.041 | 0.020 | 0.020 |
| 1 | 5.00 | 9.2 | -0.0 | 4.1 | 0.272 | 0. | 0.039 | 0.039 | 0.019 | 0.019 |
| 2 | 10.00 | 9.2 | -0.0 | 4.0 | 0.270 | 0. | 0.037 | 0.037 | 0.018 | 0.018 |
| 3 | 15.00 | 9.2 | -0.0 | 4.0 | 0.270 | 0. | 0.037 | 0.037 | 0.017 | 0.017 |
| 4 | 30.00 | 9.2 | -0.0 | 4.0 | 0.269 | 0. | 0.038 | 0.038 | 0.016 | 0.016 |
| 5 | 50.00 | 9.2 | -0.0 | 4.1 | 0.276 | 0. | 0.045 | 0.045 | 0.016 | 0.016 |
| 6 | 70.00 | 9.1 | -0.0 | 4.2 | 0.294 | 0. | 0.056 | 0.056 | 0.017 | 0.017 |
| 7 | 85.00 | 9.1 | 0.0 | 4.2 | 0.328 | 0. | 0.072 | 0.072 | 0.018 | 0.018 |
| 8 | 90.00 | 9.1 | 0.0 | 4.1 | 0.349 | 0. | 0.081 | 0.081 | 0.019 | 0.019 |
| 9 | 95.00 | 9.1 | 0.0 | 4.0 | 0.375 | 0. | 0.092 | 0.092 | 0.020 | 0.020 |
| HUB | 100.00 | 9.1 | 0.0 | 3.9 | 0.406 | 0. | 0.106 | 0.106 | 0.021 | 0.021 |

TABLE IV. - BLADE GEOMETRY FOR ROTOR 51B A

| RP | PERCENT | | RADII | | BLADE ANGLES | | | DELTA | CONE |
|-----|---------|--------|--------|-------|--------------|-------|-------|--------|------|
| | SPAN | RI | RO | KIC | KTC | KOC | INC | ANGLE | |
| TIP | 0. | 25.400 | 25.400 | 56.30 | 49.79 | 43.33 | 4.58 | 0.057 | |
| 1 | 5. | 24.647 | 24.638 | 55.42 | 48.81 | 42.20 | 4.66 | -0.093 | |
| 2 | 10. | 23.868 | 23.876 | 54.45 | 47.61 | 40.77 | 4.88 | 0.082 | |
| 3 | 15. | 23.085 | 23.114 | 53.40 | 46.18 | 38.96 | 5.25 | 0.290 | |
| 4 | 30. | 20.732 | 20.828 | 49.93 | 41.12 | 32.31 | 7.07 | 0.959 | |
| 5 | 50. | 17.607 | 17.780 | 44.49 | 32.84 | 21.19 | 10.36 | 1.698 | |
| 6 | 70. | 14.533 | 14.732 | 38.37 | 23.30 | 8.20 | 13.41 | 1.993 | |
| 7 | 85. | 12.294 | 12.446 | 33.12 | 16.79 | 0.44 | 14.90 | 1.590 | |
| 8 | 90. | 11.565 | 11.684 | 31.20 | 15.12 | -0.99 | 15.19 | 1.273 | |
| 9 | 95. | 10.844 | 10.922 | 29.21 | 13.68 | -1.88 | 15.39 | 0.853 | |
| HUB | 100. | 10.160 | 10.160 | 27.30 | 12.33 | -2.70 | 15.56 | 0.057 | |

| RP | BLADE THICKNESSES | | | AXIAL DIMENSIONS | | | |
|-----|-------------------|-------|-------|------------------|-------|-------|-------|
| | TI | TM | TO | ZI | ZMC | ZTC | ZO |
| TIP | 0.086 | 0.429 | 0.086 | -0.155 | 2.460 | 2.460 | 5.445 |
| 1 | 0.083 | 0.430 | 0.083 | -0.157 | 2.461 | 2.461 | 5.443 |
| 2 | 0.086 | 0.441 | 0.086 | -0.165 | 2.461 | 2.461 | 5.450 |
| 3 | 0.098 | 0.464 | 0.098 | -0.181 | 2.460 | 2.460 | 5.467 |
| 4 | 0.121 | 0.584 | 0.121 | -0.232 | 2.455 | 2.455 | 5.521 |
| 5 | 0.159 | 0.779 | 0.157 | -0.271 | 2.455 | 2.455 | 5.556 |
| 6 | 0.189 | 0.923 | 0.177 | -0.241 | 2.466 | 2.466 | 5.490 |
| 7 | 0.186 | 0.944 | 0.187 | -0.148 | 2.479 | 2.479 | 5.339 |
| 8 | 0.184 | 0.933 | 0.186 | -0.103 | 2.483 | 2.483 | 5.271 |
| 9 | 0.182 | 0.914 | 0.183 | -0.051 | 2.486 | 2.486 | 5.194 |
| HJB | 0.179 | 0.896 | 0.179 | 0. | 2.490 | 2.490 | 5.116 |

| RP | AERO SETTING | | | TOTAL | X | AREA |
|-----|--------------|-------|--------|-------|-------|-------|
| | CHORD | ANGLE | CAMBER | | | |
| TIP | 8.629 | 49.80 | 12.97 | 0.649 | 1.000 | 13.99 |
| 1 | 8.460 | 48.81 | 13.22 | 0.656 | 1.000 | 13.71 |
| 2 | 8.287 | 47.61 | 13.68 | 0.663 | 1.000 | 13.56 |
| 3 | 8.115 | 46.18 | 14.44 | 0.671 | 1.000 | 13.58 |
| 4 | 7.599 | 41.13 | 17.62 | 0.698 | 1.000 | 13.18 |
| 5 | 6.910 | 32.85 | 23.30 | 0.746 | 1.000 | 10.14 |
| 6 | 6.229 | 23.26 | 30.16 | 0.813 | 1.000 | 4.28 |
| 7 | 5.726 | 16.82 | 32.67 | 0.884 | 1.000 | -1.52 |
| 8 | 5.561 | 15.14 | 32.19 | 0.914 | 1.000 | -3.60 |
| 9 | 5.393 | 13.69 | 31.08 | 0.946 | 1.000 | -5.76 |
| HJB | 5.232 | 12.33 | 30.00 | 0.984 | 1.000 | -7.81 |

TABLE V. - BLADE GEOMETRY FOR STATOR 51

| RP | PERCENT | | RADII | | BLADE ANGLES | | | DELTA | CONE |
|-----|---------|--|--------|--------|--------------|------|-------|-------|-------|
| | SPAN | | RI | RO | KIC | KTC | KOC | INC | ANGLE |
| TIP | 0. | | 25.400 | 25.400 | 14.20 | 5.04 | -4.13 | 9.22 | 0.057 |
| 1 | 5. | | 24.595 | 24.608 | 14.30 | 5.12 | -4.07 | 9.21 | 0.144 |
| 2 | 10. | | 23.861 | 23.887 | 14.44 | 5.20 | -4.03 | 9.21 | 0.306 |
| 3 | 15. | | 23.128 | 23.166 | 14.63 | 5.31 | -4.01 | 9.21 | 0.448 |
| 4 | 30. | | 20.917 | 20.995 | 15.51 | 5.75 | -4.00 | 9.19 | 0.915 |
| 5 | 50. | | 17.955 | 18.080 | 17.40 | 6.64 | -4.11 | 9.17 | 1.461 |
| 6 | 70. | | 14.946 | 15.110 | 19.85 | 7.81 | -4.23 | 9.13 | 1.913 |
| 7 | 85. | | 12.647 | 12.787 | 21.60 | 8.70 | -4.20 | 9.11 | 1.642 |
| 8 | 90. | | 11.870 | 11.967 | 21.95 | 8.92 | -4.11 | 9.11 | 1.140 |
| 9 | 95. | | 11.087 | 11.125 | 22.20 | 9.10 | -3.99 | 9.12 | 0.439 |
| HUB | 100. | | 10.160 | 10.160 | 22.49 | 9.32 | -3.85 | 9.13 | 0.057 |

| RP | BLADE THICKNESSES | | | AXIAL DIMENSIONS | | | |
|-----|-------------------|-------|-------|------------------|--------|--------|--------|
| | TI | TM | TO | ZI | ZMC | ZTC | ZO |
| TIP | 0.099 | 0.495 | 0.099 | 25.452 | 27.898 | 27.898 | 30.379 |
| 1 | 0.099 | 0.495 | 0.099 | 25.455 | 27.900 | 27.900 | 30.381 |
| 2 | 0.099 | 0.495 | 0.099 | 25.456 | 27.900 | 27.900 | 30.381 |
| 3 | 0.099 | 0.495 | 0.099 | 25.455 | 27.899 | 27.899 | 30.380 |
| 4 | 0.099 | 0.495 | 0.099 | 25.458 | 27.897 | 27.897 | 30.378 |
| 5 | 0.099 | 0.495 | 0.099 | 25.467 | 27.896 | 27.896 | 30.378 |
| 6 | 0.099 | 0.495 | 0.099 | 25.479 | 27.894 | 27.894 | 30.379 |
| 7 | 0.099 | 0.495 | 0.099 | 25.488 | 27.891 | 27.891 | 30.377 |
| 8 | 0.099 | 0.495 | 0.099 | 25.491 | 27.891 | 27.891 | 30.377 |
| 9 | 0.099 | 0.495 | 0.099 | 25.494 | 27.892 | 27.892 | 30.378 |
| HUB | 0.099 | 0.494 | 0.099 | 25.498 | 27.894 | 27.894 | 30.380 |

| | AERO | SETTING | TOTAL | | X | | AREA |
|-----|-------|---------|--------|----------|--------|-------|-------|
| RP | CHORD | ANGLE | CAMBER | SOLIDITY | FACTOR | PHISS | RATIO |
| TIP | 4.945 | 5.04 | 18.33 | 0.992 | 1.000 | -2.24 | 0.273 |
| 1 | 4.945 | 5.12 | 18.38 | 1.024 | 1.000 | -2.36 | 0.266 |
| 2 | 4.945 | 5.20 | 18.47 | 1.055 | 1.000 | -2.43 | 0.261 |
| 3 | 4.945 | 5.31 | 18.64 | 1.088 | 1.000 | -2.48 | 0.257 |
| 4 | 4.945 | 5.76 | 19.51 | 1.202 | 1.000 | -2.50 | 0.252 |
| 5 | 4.946 | 6.65 | 21.51 | 1.398 | 1.000 | -2.26 | 0.259 |
| 6 | 4.948 | 7.83 | 24.08 | 1.677 | 1.000 | -2.03 | 0.281 |
| 7 | 4.947 | 8.72 | 25.79 | 1.981 | 1.000 | -2.19 | 0.305 |
| 8 | 4.946 | 8.94 | 26.07 | 2.114 | 1.000 | -2.41 | 0.300 |
| 9 | 4.946 | 9.11 | 26.19 | 2.268 | 1.000 | -2.72 | 0.288 |
| HUB | 4.946 | 9.32 | 26.34 | 2.479 | 1.000 | -3.09 | 0.275 |

TABLE VI. - OVERALL PERFORMANCE AT 100 PERCENT DESIGN SPEED

(a) Stage 51B A

| Parameter | Reading number | | | | |
|--------------------------------|----------------|--------|--------|--------|--------|
| | 1766 | 1767 | 1768 | 1769 | 1771 |
| ROTOR TOTAL PRESSURE RATIO | 1.127 | 1.145 | 1.137 | 1.152 | 1.155 |
| STAGE TOTAL PRESSURE RATIO | 1.117 | 1.134 | 1.126 | 1.139 | 1.141 |
| ROTOR TOTAL TEMPERATURE RATIO | 1.039 | 1.043 | 1.042 | 1.046 | 1.048 |
| STAGE TOTAL TEMPERATURE RATIO | 1.035 | 1.039 | 1.039 | 1.044 | 1.046 |
| ROTOR TEMP. RISE EFFICIENCY | 0.898 | 0.918 | 0.902 | 0.889 | 0.881 |
| STAGE TEMP. RISE EFFICIENCY | 0.908 | 0.927 | 0.894 | 0.860 | 0.856 |
| ROTOR MOMENTUM RISE EFFICIENCY | 0.880 | 0.917 | 0.897 | 0.885 | 0.872 |
| ROTOR HEAD RISE COEFFICIENT | 0.170 | 0.192 | 0.182 | 0.202 | 0.206 |
| STAGE HEAD RISE COEFFICIENT | 0.156 | 0.178 | 0.168 | 0.185 | 0.188 |
| FLOW COEFFICIENT | 0.799 | 0.762 | 0.695 | 0.618 | 0.592 |
| WT FLOW PER UNIT FRONTAL AREA | 164.92 | 159.91 | 149.87 | 136.51 | 131.78 |
| WT FLOW PER UNIT ANNULUS AREA | 196.34 | 190.37 | 178.42 | 162.52 | 156.88 |
| WT FLOW AT ORIFICE | 33.43 | 32.41 | 30.38 | 27.67 | 26.71 |
| WT FLOW AT ROTOR INLET | 35.45 | 32.45 | 30.39 | 27.76 | 26.76 |
| WT FLOW AT ROTOR OUTLET | 33.58 | 32.64 | 30.54 | 28.01 | 27.03 |
| WT FLOW AT STATOR OUTLET | 33.22 | 32.35 | 30.06 | 27.51 | 26.56 |
| ROTATIVE SPEED | 9152.1 | 9161.2 | 9169.0 | 9158.4 | 9141.9 |
| PERCENT OF DESIGN SPEED | 99.8 | 99.9 | 100.0 | 99.9 | 99.7 |

(b) Stage 51B B

| Parameter | Reading number | | | | | |
|--------------------------------|----------------|--------|--------|--------|--------|--------|
| | 1796 | 1797 | 1798 | 1800 | 1801 | 1807 |
| ROTOR TOTAL PRESSURE RATIO | 1.115 | 1.148 | 1.145 | 1.158 | 1.161 | 1.164 |
| STAGE TOTAL PRESSURE RATIO | 1.100 | 1.136 | 1.132 | 1.142 | 1.146 | 1.148 |
| ROTOR TOTAL TEMPERATURE RATIO | 1.037 | 1.044 | 1.044 | 1.047 | 1.049 | 1.051 |
| STAGE TOTAL TEMPERATURE RATIO | 1.034 | 1.041 | 1.041 | 1.045 | 1.047 | 1.048 |
| ROTOR TEMP. RISE EFFICIENCY | 0.845 | 0.907 | 0.900 | 0.901 | 0.886 | 0.875 |
| STAGE TEMP. RISE EFFICIENCY | 0.824 | 0.909 | 0.889 | 0.871 | 0.852 | 0.838 |
| ROTOR MOMENTUM RISE EFFICIENCY | 0.817 | 0.885 | 0.879 | 0.888 | 0.871 | 0.868 |
| ROTOR HEAD RISE COEFFICIENT | 0.154 | 0.196 | 0.191 | 0.207 | 0.212 | 0.216 |
| STAGE HEAD RISE COEFFICIENT | 0.135 | 0.180 | 0.175 | 0.188 | 0.193 | 0.196 |
| FLOW COEFFICIENT | 0.852 | 0.819 | 0.755 | 0.700 | 0.669 | 0.655 |
| WT FLOW PER UNIT FRONTAL AREA | 172.25 | 167.82 | 159.30 | 150.58 | 145.55 | 143.03 |
| WT FLOW PER UNIT ANNULUS AREA | 205.06 | 199.79 | 189.65 | 179.26 | 173.28 | 170.28 |
| WT FLOW AT ORIFICE | 34.91 | 34.01 | 32.29 | 30.52 | 29.50 | 28.99 |
| WT FLOW AT ROTOR INLET | 34.88 | 34.04 | 32.29 | 30.58 | 29.57 | 29.09 |
| WT FLOW AT ROTOR OUTLET | 35.37 | 34.34 | 32.47 | 30.94 | 29.87 | 29.43 |
| WT FLOW AT STATOR OUTLET | 34.68 | 33.96 | 31.96 | 30.26 | 29.28 | 28.81 |
| ROTATIVE SPEED | 9179.1 | 9175.3 | 9186.1 | 9181.5 | 9184.9 | 9177.3 |
| PERCENT OF DESIGN SPEED | 100.1 | 100.1 | 100.2 | 100.2 | 100.2 | 100.1 |

TABLE VI. - Concluded.

(c) Stage 51B C

| Parameter | Reading number | | | | | |
|--------------------------------|----------------|--------|--------|--------|--------|--------|
| | 1830 | 1829 | 1828 | 1827 | 1824 | 1841 |
| ROTOR TOTAL PRESSURE RATIO | 1.112 | 1.134 | 1.131 | 1.140 | 1.148 | 1.153 |
| STAGE TOTAL PRESSURE RATIO | 1.103 | 1.124 | 1.123 | 1.129 | 1.136 | 1.139 |
| ROTOR TOTAL TEMPERATURE RATIO | 1.034 | 1.039 | 1.039 | 1.042 | 1.046 | 1.047 |
| STAGE TOTAL TEMPERATURE RATIO | 1.031 | 1.036 | 1.037 | 1.041 | 1.044 | 1.046 |
| ROTOR TEMP. RISE EFFICIENCY | 0.912 | 0.943 | 0.924 | 0.902 | 0.881 | 0.877 |
| STAGE TEMP. RISE EFFICIENCY | 0.915 | 0.935 | 0.906 | 0.869 | 0.843 | 0.828 |
| ROTOR MOMENTUM RISE EFFICIENCY | 0.894 | 0.936 | 0.915 | 0.915 | 0.888 | 0.876 |
| ROTOR HEAD RISE COEFFICIENT | 0.150 | 0.177 | 0.175 | 0.185 | 0.196 | 0.202 |
| STAGE HEAD RISE COEFFICIENT | 0.138 | 0.166 | 0.165 | 0.171 | 0.180 | 0.184 |
| FLOW COEFFICIENT | 0.756 | 0.695 | 0.642 | 0.600 | 0.552 | 0.528 |
| WT FLOW PER UNIT FRONTAL AREA | 158.33 | 149.24 | 140.26 | 132.92 | 124.75 | 119.41 |
| WT FLOW PER UNIT ANNULUS AREA | 188.50 | 177.67 | 166.98 | 158.25 | 148.52 | 142.16 |
| WT FLOW AT ORIFICE | 32.09 | 30.25 | 28.43 | 26.94 | 25.29 | 24.20 |
| WT FLOW AT ROTOR INLET | 32.24 | 30.39 | 28.58 | 27.11 | 25.30 | 24.39 |
| WT FLOW AT ROTOR OUTLET | 32.23 | 30.46 | 28.59 | 27.27 | 25.53 | 24.63 |
| WT FLOW AT STATOR OUTLET | 31.83 | 30.05 | 28.26 | 26.73 | 25.16 | 24.22 |
| ROTATIVE SPEED | 9153.2 | 9167.4 | 9148.3 | 9171.4 | 9169.7 | 9169.1 |
| PERCENT OF DESIGN SPEED | 99.8 | 100.0 | 99.8 | 100.0 | 100.0 | 100.0 |

TABLE VII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR 51B A

AT 100 PERCENT DESIGN SPEED

(a) Reading number 1766

| RP | RADI I | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 18.0 | 50.7 | 47.1 | 289.1 | 1.044 | 10.08 | 1.122 |
| 2 | 23.868 | 23.876 | 0.0 | 15.7 | 49.6 | 44.8 | 288.9 | 1.041 | 10.13 | 1.140 |
| 3 | 23.086 | 23.114 | 0.0 | 16.2 | 48.7 | 43.1 | 288.6 | 1.041 | 10.14 | 1.139 |
| 4 | 20.731 | 20.828 | 0.0 | 18.2 | 45.2 | 37.7 | 287.9 | 1.042 | 10.14 | 1.137 |
| 5 | 17.607 | 17.780 | 0.0 | 21.3 | 40.7 | 28.9 | 287.9 | 1.039 | 10.14 | 1.134 |
| 6 | 14.531 | 14.732 | 0.0 | 23.8 | 35.7 | 18.7 | 287.8 | 1.037 | 10.14 | 1.127 |
| 7 | 12.294 | 12.446 | 0.0 | 24.2 | 31.6 | 12.8 | 287.7 | 1.030 | 10.14 | 1.096 |
| 8 | 11.565 | 11.684 | 0.0 | 24.1 | 30.1 | 11.4 | 287.8 | 1.027 | 10.14 | 1.080 |
| 9 | 10.843 | 10.922 | 0.0 | 25.5 | 28.7 | 8.9 | 287.7 | 1.027 | 10.11 | 1.069 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 193.0 | 176.9 | 304.7 | 247.3 | 193.0 | 168.3 | 0.1 | 54.6 | 235.9 | 235.8 |
| 2 | 194.6 | 186.8 | 300.2 | 253.2 | 194.6 | 179.8 | 0.1 | 50.6 | 228.7 | 228.8 |
| 3 | 194.3 | 187.9 | 294.3 | 247.4 | 194.3 | 180.5 | 0.1 | 52.3 | 221.2 | 221.5 |
| 4 | 197.0 | 190.7 | 279.7 | 228.9 | 197.0 | 181.1 | 0.1 | 59.7 | 198.8 | 199.7 |
| 5 | 196.1 | 193.9 | 258.6 | 206.4 | 196.1 | 180.6 | 0.1 | 70.5 | 168.8 | 170.4 |
| 6 | 193.6 | 198.2 | 238.5 | 191.4 | 193.6 | 181.3 | 0.1 | 80.0 | 139.4 | 141.3 |
| 7 | 191.7 | 193.4 | 225.0 | 180.9 | 191.7 | 176.4 | 0.1 | 79.3 | 117.8 | 119.3 |
| 8 | 191.2 | 188.7 | 220.9 | 175.8 | 191.2 | 172.3 | 0.1 | 77.0 | 110.8 | 111.9 |
| 9 | 189.4 | 183.4 | 216.0 | 167.6 | 189.4 | 165.6 | 0.1 | 78.9 | 104.0 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.585 | 0.522 | 0.924 | 0.729 | 0.585 | 0.496 | 0.872 | 1.138 |
| 2 | 0.591 | 0.553 | 0.911 | 0.750 | 0.591 | 0.533 | 0.924 | 1.104 |
| 3 | 0.590 | 0.558 | 0.894 | 0.734 | 0.590 | 0.535 | 0.929 | 1.075 |
| 4 | 0.600 | 0.567 | 0.852 | 0.680 | 0.600 | 0.538 | 0.919 | 0.941 |
| 5 | 0.597 | 0.578 | 0.787 | 0.615 | 0.597 | 0.538 | 0.921 | 0.787 |
| 6 | 0.589 | 0.592 | 0.725 | 0.572 | 0.589 | 0.542 | 0.936 | 0.725 |
| 7 | 0.583 | 0.579 | 0.684 | 0.542 | 0.583 | 0.528 | 0.920 | 0.684 |
| 8 | 0.581 | 0.565 | 0.671 | 0.526 | 0.581 | 0.516 | 0.901 | 0.671 |
| 9 | 0.575 | 0.548 | 0.656 | 0.501 | 0.575 | 0.495 | 0.874 | 0.656 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -4.7 | -9.4 | 4.9 | 0.324 | 0.766 | 0.080 | 0.080 | 0.041 | 0.041 |
| 2 | 10.00 | -4.9 | -9.7 | 4.0 | 0.283 | 0.921 | 0.026 | 0.026 | 0.014 | 0.014 |
| 3 | 15.00 | -4.7 | -10.0 | 4.2 | 0.292 | 0.924 | 0.026 | 0.026 | 0.014 | 0.014 |
| 4 | 30.00 | -4.7 | -11.8 | 5.4 | 0.335 | 0.902 | 0.036 | 0.036 | 0.020 | 0.020 |
| 5 | 50.00 | -3.8 | -14.2 | 7.8 | 0.385 | 0.929 | 0.028 | 0.028 | 0.017 | 0.017 |
| 6 | 70.00 | -2.7 | -16.1 | 10.5 | 0.405 | 0.942 | 0.025 | 0.025 | 0.014 | 0.014 |
| 7 | 85.00 | -1.6 | -16.5 | 12.3 | 0.396 | 0.882 | 0.044 | 0.044 | 0.025 | 0.025 |
| 8 | 90.00 | -1.1 | -16.3 | 12.4 | 0.396 | 0.824 | 0.062 | 0.062 | 0.033 | 0.033 |
| 9 | 95.00 | -0.5 | -15.9 | 10.8 | 0.418 | 0.716 | 0.103 | 0.103 | 0.054 | 0.054 |

TABLE VII. - Continued.

(b) Reading number 1767

| RP | RADI I | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 20.6 | 51.8 | 47.5 | 289.1 | 1.051 | 10.09 | 1.148 |
| 2 | 23.868 | 23.876 | 0.0 | 18.4 | 50.8 | 44.8 | 288.9 | 1.048 | 10.13 | 1.167 |
| 3 | 23.086 | 23.114 | 0.0 | 18.6 | 49.9 | 43.2 | 288.6 | 1.047 | 10.14 | 1.166 |
| 4 | 20.731 | 20.828 | 0.0 | 20.9 | 46.4 | 37.4 | 288.0 | 1.046 | 10.14 | 1.161 |
| 5 | 17.607 | 17.780 | 0.0 | 23.8 | 42.1 | 29.0 | 287.8 | 1.043 | 10.14 | 1.149 |
| 6 | 14.531 | 14.732 | 0.0 | 25.8 | 37.1 | 19.2 | 287.8 | 1.038 | 10.14 | 1.132 |
| 7 | 12.294 | 12.446 | 0.0 | 25.9 | 32.9 | 14.0 | 287.7 | 1.031 | 10.14 | 1.095 |
| 8 | 11.565 | 11.684 | 0.0 | 25.5 | 31.4 | 12.3 | 287.8 | 1.028 | 10.14 | 1.086 |
| 9 | 10.843 | 10.922 | 0.0 | 28.1 | 30.1 | 8.5 | 287.8 | 1.029 | 10.11 | 1.076 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 185.8 | 172.0 | 300.6 | 238.3 | 185.8 | 161.0 | 0.1 | 60.6 | 236.4 | 236.3 |
| 2 | 186.7 | 182.0 | 295.3 | 243.4 | 186.7 | 172.7 | 0.1 | 57.5 | 229.0 | 229.0 |
| 3 | 186.5 | 183.4 | 289.4 | 238.4 | 186.5 | 173.8 | 0.1 | 58.6 | 221.5 | 221.7 |
| 4 | 188.5 | 186.3 | 273.6 | 219.0 | 188.5 | 174.0 | 0.1 | 66.5 | 198.4 | 199.4 |
| 5 | 186.9 | 187.5 | 251.9 | 196.1 | 186.9 | 171.6 | 0.1 | 75.7 | 169.0 | 170.6 |
| 6 | 184.3 | 188.6 | 231.0 | 179.8 | 184.3 | 169.7 | 0.1 | 82.1 | 139.5 | 141.4 |
| 7 | 181.9 | 180.6 | 216.8 | 167.4 | 181.9 | 162.4 | 0.1 | 78.9 | 118.0 | 119.4 |
| 8 | 181.4 | 178.6 | 212.6 | 165.0 | 181.4 | 161.2 | 0.1 | 77.0 | 111.0 | 112.1 |
| 9 | 179.4 | 174.2 | 207.4 | 155.4 | 179.4 | 153.7 | 0.1 | 81.9 | 104.2 | 104.9 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.562 | 0.505 | 0.909 | 0.699 | 0.562 | 0.472 | 0.866 | 1.158 |
| 2 | 0.565 | 0.537 | 0.894 | 0.718 | 0.565 | 0.509 | 0.925 | 1.124 |
| 3 | 0.565 | 0.541 | 0.877 | 0.704 | 0.565 | 0.513 | 0.932 | 1.096 |
| 4 | 0.572 | 0.551 | 0.830 | 0.648 | 0.572 | 0.515 | 0.923 | 0.964 |
| 5 | 0.567 | 0.556 | 0.764 | 0.582 | 0.567 | 0.509 | 0.918 | 0.764 |
| 6 | 0.559 | 0.561 | 0.700 | 0.535 | 0.559 | 0.505 | 0.921 | 0.700 |
| 7 | 0.551 | 0.538 | 0.657 | 0.499 | 0.551 | 0.484 | 0.893 | 0.657 |
| 8 | 0.549 | 0.533 | 0.644 | 0.492 | 0.549 | 0.481 | 0.888 | 0.644 |
| 9 | 0.543 | 0.518 | 0.628 | 0.463 | 0.543 | 0.457 | 0.857 | 0.628 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -3.6 | -8.3 | 5.3 | 0.361 | 0.785 | 0.087 | 0.087 | 0.045 | 0.045 |
| 2 | 10.00 | -3.7 | -8.5 | 4.0 | 0.322 | 0.942 | 0.023 | 0.023 | 0.012 | 0.012 |
| 3 | 15.00 | -3.5 | -8.8 | 4.2 | 0.327 | 0.948 | 0.021 | 0.021 | 0.011 | 0.011 |
| 4 | 30.00 | -3.5 | -10.6 | 5.1 | 0.374 | 0.947 | 0.022 | 0.022 | 0.013 | 0.013 |
| 5 | 50.00 | -2.4 | -12.8 | 7.8 | 0.423 | 0.949 | 0.023 | 0.023 | 0.013 | 0.013 |
| 6 | 70.00 | -1.3 | -14.7 | 11.0 | 0.442 | 0.938 | 0.029 | 0.029 | 0.017 | 0.017 |
| 7 | 85.00 | -0.2 | -15.1 | 13.6 | 0.434 | 0.856 | 0.059 | 0.059 | 0.033 | 0.033 |
| 8 | 90.00 | 0.2 | -15.0 | 13.3 | 0.423 | 0.845 | 0.061 | 0.061 | 0.033 | 0.033 |
| 9 | 95.00 | 0.9 | -14.5 | 10.4 | 0.460 | 0.732 | 0.113 | 0.113 | 0.059 | 0.059 |

TABLE VII. - Continued.

(c) Reading number 1768

| RP | RADI I | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 21.6 | 54.4 | 48.2 | 289.1 | 1.050 | 10.10 | 1.158 |
| 2 | 23.868 | 23.876 | 0.0 | 19.7 | 53.3 | 46.1 | 288.8 | 1.048 | 10.13 | 1.167 |
| 3 | 23.086 | 23.114 | 0.0 | 19.7 | 52.4 | 44.8 | 288.4 | 1.047 | 10.13 | 1.163 |
| 4 | 20.731 | 20.828 | 0.0 | 21.5 | 49.1 | 40.3 | 288.0 | 1.044 | 10.14 | 1.147 |
| 5 | 17.607 | 17.780 | 0.0 | 24.5 | 44.8 | 33.5 | 287.9 | 1.039 | 10.14 | 1.127 |
| 6 | 14.531 | 14.732 | 0.0 | 26.8 | 39.8 | 23.3 | 287.8 | 1.036 | 10.14 | 1.116 |
| 7 | 12.294 | 12.446 | 0.0 | 28.1 | 35.5 | 14.3 | 287.8 | 1.032 | 10.13 | 1.107 |
| 8 | 11.565 | 11.684 | 0.0 | 28.4 | 34.0 | 11.3 | 287.8 | 1.031 | 10.14 | 1.103 |
| 9 | 10.843 | 10.922 | 0.0 | 30.9 | 32.5 | 7.6 | 287.8 | 1.031 | 10.11 | 1.091 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 169.5 | 168.1 | 290.9 | 234.3 | 169.5 | 156.3 | 0.1 | 62.0 | 236.6 | 236.5 |
| 2 | 171.1 | 174.5 | 286.1 | 236.8 | 171.1 | 164.3 | 0.1 | 58.8 | 229.4 | 229.5 |
| 3 | 170.7 | 174.2 | 279.5 | 231.3 | 170.7 | 164.0 | 0.1 | 58.6 | 221.5 | 221.7 |
| 4 | 172.2 | 172.6 | 262.8 | 210.6 | 172.2 | 160.6 | 0.1 | 63.3 | 198.6 | 199.5 |
| 5 | 170.2 | 168.1 | 239.9 | 183.5 | 170.2 | 153.0 | 0.1 | 69.6 | 169.2 | 170.9 |
| 6 | 167.3 | 169.0 | 217.6 | 164.4 | 167.3 | 150.9 | 0.1 | 76.2 | 139.4 | 141.3 |
| 7 | 165.4 | 171.7 | 203.2 | 156.3 | 165.4 | 151.5 | 0.1 | 80.9 | 118.2 | 119.6 |
| 8 | 164.9 | 172.3 | 198.8 | 154.5 | 164.9 | 151.5 | 0.1 | 82.0 | 111.2 | 112.3 |
| 9 | 163.4 | 167.1 | 193.7 | 144.6 | 163.4 | 143.3 | 0.1 | 85.8 | 104.1 | 104.9 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.510 | 0.493 | 0.876 | 0.687 | 0.510 | 0.458 | 0.922 | 1.196 |
| 2 | 0.516 | 0.513 | 0.862 | 0.697 | 0.516 | 0.483 | 0.960 | 1.161 |
| 3 | 0.515 | 0.513 | 0.843 | 0.681 | 0.515 | 0.483 | 0.961 | 1.130 |
| 4 | 0.520 | 0.509 | 0.793 | 0.621 | 0.520 | 0.474 | 0.933 | 1.003 |
| 5 | 0.514 | 0.497 | 0.724 | 0.542 | 0.514 | 0.452 | 0.899 | 0.736 |
| 6 | 0.504 | 0.500 | 0.656 | 0.487 | 0.504 | 0.447 | 0.902 | 0.656 |
| 7 | 0.498 | 0.510 | 0.612 | 0.464 | 0.498 | 0.450 | 0.916 | 0.612 |
| 8 | 0.497 | 0.512 | 0.599 | 0.459 | 0.497 | 0.450 | 0.919 | 0.599 |
| 9 | 0.492 | 0.496 | 0.583 | 0.429 | 0.492 | 0.425 | 0.877 | 0.583 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -1.0 | -5.7 | 6.0 | 0.357 | 0.847 | 0.065 | 0.065 | 0.033 | 0.033 |
| 2 | 10.00 | -1.2 | -6.1 | 5.3 | 0.327 | 0.931 | 0.029 | 0.029 | 0.015 | 0.015 |
| 3 | 15.00 | -1.0 | -6.3 | 5.9 | 0.328 | 0.939 | 0.026 | 0.026 | 0.014 | 0.014 |
| 4 | 30.00 | -0.9 | -7.9 | 8.0 | 0.371 | 0.910 | 0.039 | 0.039 | 0.021 | 0.021 |
| 5 | 50.00 | 0.3 | -10.0 | 12.3 | 0.430 | 0.899 | 0.045 | 0.045 | 0.025 | 0.025 |
| 6 | 70.00 | 1.4 | -12.0 | 15.1 | 0.461 | 0.881 | 0.058 | 0.058 | 0.033 | 0.033 |
| 7 | 85.00 | 2.4 | -12.5 | 13.9 | 0.457 | 0.915 | 0.042 | 0.042 | 0.023 | 0.023 |
| 8 | 90.00 | 2.8 | -12.4 | 12.3 | 0.449 | 0.918 | 0.040 | 0.040 | 0.022 | 0.022 |
| 9 | 95.00 | 3.3 | -12.1 | 9.5 | 0.488 | 0.824 | 0.088 | 0.088 | 0.046 | 0.046 |

TABLE VII. - Continued.

(d) Reading number 1769

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 26.9 | 57.2 | 49.4 | 288.8 | 1.059 | 10.10 | 1.180 |
| 2 | 23.868 | 23.876 | 0.0 | 24.4 | 56.3 | 47.1 | 288.7 | 1.056 | 10.13 | 1.188 |
| 3 | 23.086 | 23.114 | 0.0 | 25.0 | 55.5 | 45.7 | 288.4 | 1.054 | 10.14 | 1.183 |
| 4 | 20.731 | 20.828 | 0.0 | 26.7 | 52.4 | 41.5 | 288.0 | 1.049 | 10.13 | 1.164 |
| 5 | 17.607 | 17.780 | 0.0 | 29.2 | 48.1 | 35.0 | 287.9 | 1.042 | 10.14 | 1.137 |
| 6 | 14.531 | 14.732 | 0.0 | 30.9 | 43.2 | 24.4 | 287.9 | 1.038 | 10.14 | 1.127 |
| 7 | 12.294 | 12.446 | 0.0 | 31.9 | 38.9 | 15.3 | 287.9 | 1.034 | 10.14 | 1.114 |
| 8 | 11.565 | 11.684 | 0.0 | 32.6 | 37.4 | 11.6 | 287.9 | 1.033 | 10.13 | 1.110 |
| 9 | 10.843 | 10.922 | 0.0 | 35.5 | 36.0 | 7.6 | 287.9 | 1.032 | 10.12 | 1.098 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 152.3 | 158.2 | 281.1 | 217.0 | 152.3 | 141.2 | 0.1 | 71.5 | 236.3 | 236.2 |
| 2 | 152.6 | 164.3 | 274.8 | 219.7 | 152.6 | 149.6 | 0.1 | 67.8 | 228.6 | 228.7 |
| 3 | 152.5 | 164.1 | 268.9 | 213.1 | 152.5 | 148.8 | 0.1 | 69.3 | 221.6 | 221.9 |
| 4 | 153.4 | 161.4 | 251.2 | 192.4 | 153.4 | 144.1 | 0.1 | 72.6 | 199.0 | 199.9 |
| 5 | 151.2 | 155.0 | 226.4 | 165.3 | 151.2 | 135.4 | 0.1 | 75.5 | 168.7 | 170.3 |
| 6 | 148.3 | 156.5 | 203.4 | 147.5 | 148.3 | 134.3 | 0.1 | 80.4 | 139.3 | 141.3 |
| 7 | 145.8 | 157.0 | 187.4 | 138.2 | 145.8 | 133.3 | 0.1 | 83.0 | 117.9 | 119.4 |
| 8 | 144.8 | 157.5 | 182.3 | 135.5 | 144.8 | 132.7 | 0.1 | 84.8 | 110.9 | 112.0 |
| 9 | 143.2 | 152.0 | 177.0 | 124.8 | 143.2 | 123.7 | 0.1 | 88.3 | 104.1 | 104.9 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.456 | 0.461 | 0.842 | 0.632 | 0.456 | 0.411 | 0.927 | 1.232 |
| 2 | 0.457 | 0.480 | 0.824 | 0.642 | 0.457 | 0.437 | 0.981 | 1.196 |
| 3 | 0.457 | 0.480 | 0.806 | 0.624 | 0.457 | 0.435 | 0.976 | 1.168 |
| 4 | 0.460 | 0.473 | 0.754 | 0.564 | 0.460 | 0.423 | 0.940 | 1.044 |
| 5 | 0.453 | 0.456 | 0.679 | 0.486 | 0.453 | 0.398 | 0.896 | 0.811 |
| 6 | 0.445 | 0.461 | 0.610 | 0.435 | 0.445 | 0.396 | 0.906 | 0.610 |
| 7 | 0.437 | 0.464 | 0.561 | 0.408 | 0.437 | 0.394 | 0.914 | 0.561 |
| 8 | 0.434 | 0.465 | 0.546 | 0.400 | 0.434 | 0.392 | 0.917 | 0.546 |
| 9 | 0.429 | 0.449 | 0.530 | 0.368 | 0.429 | 0.365 | 0.864 | 0.530 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 1.8 | -2.9 | 7.2 | 0.422 | 0.817 | 0.095 | 0.095 | 0.047 | 0.047 |
| 2 | 10.00 | 1.8 | -3.1 | 6.3 | 0.386 | 0.903 | 0.050 | 0.050 | 0.026 | 0.026 |
| 3 | 15.00 | 2.1 | -3.2 | 6.8 | 0.399 | 0.909 | 0.047 | 0.047 | 0.024 | 0.024 |
| 4 | 30.00 | 2.4 | -4.6 | 9.2 | 0.441 | 0.897 | 0.054 | 0.054 | 0.029 | 0.029 |
| 5 | 50.00 | 3.6 | -6.7 | 13.8 | 0.494 | 0.880 | 0.064 | 0.064 | 0.035 | 0.035 |
| 6 | 70.00 | 4.8 | -8.6 | 16.2 | 0.519 | 0.910 | 0.052 | 0.052 | 0.029 | 0.029 |
| 7 | 85.00 | 5.8 | -9.1 | 14.8 | 0.514 | 0.928 | 0.043 | 0.043 | 0.023 | 0.023 |
| 8 | 90.00 | 6.2 | -9.0 | 12.6 | 0.512 | 0.931 | 0.041 | 0.041 | 0.022 | 0.022 |
| 9 | 95.00 | 6.8 | -8.6 | 9.5 | 0.559 | 0.845 | 0.096 | 0.096 | 0.050 | 0.050 |

TABLE VII. - Concluded.

(e) Reading number 1771

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 29.6 | 58.4 | 50.3 | 288.8 | 1.062 | 10.11 | 1.182 |
| 2 | 23.868 | 23.876 | 0.0 | 26.0 | 57.3 | 47.5 | 288.6 | 1.058 | 10.14 | 1.192 |
| 3 | 23.086 | 23.114 | 0.0 | 26.0 | 56.5 | 46.1 | 288.3 | 1.056 | 10.14 | 1.186 |
| 4 | 20.731 | 20.828 | 0.0 | 28.7 | 53.5 | 41.9 | 288.0 | 1.051 | 10.13 | 1.165 |
| 5 | 17.607 | 17.780 | 0.0 | 31.4 | 49.5 | 35.2 | 287.9 | 1.044 | 10.13 | 1.142 |
| 6 | 14.531 | 14.732 | 0.0 | 32.8 | 44.6 | 24.4 | 287.9 | 1.039 | 10.14 | 1.131 |
| 7 | 12.294 | 12.446 | 0.0 | 33.1 | 40.1 | 15.6 | 287.9 | 1.034 | 10.13 | 1.116 |
| 8 | 11.565 | 11.684 | 0.0 | 33.8 | 38.4 | 11.8 | 287.8 | 1.033 | 10.13 | 1.110 |
| 9 | 10.843 | 10.922 | 0.0 | 36.7 | 36.8 | 7.4 | 288.0 | 1.032 | 10.10 | 1.100 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 145.4 | 153.4 | 277.5 | 208.7 | 145.4 | 133.4 | 0.1 | 75.9 | 236.5 | 236.4 |
| 2 | 147.1 | 161.5 | 272.1 | 214.9 | 147.1 | 145.2 | 0.1 | 70.7 | 229.1 | 229.1 |
| 3 | 145.8 | 160.8 | 264.3 | 208.4 | 145.8 | 144.5 | 0.1 | 70.6 | 220.5 | 220.8 |
| 4 | 146.3 | 156.8 | 246.1 | 184.8 | 146.3 | 137.5 | 0.1 | 75.4 | 198.0 | 198.9 |
| 5 | 143.6 | 151.5 | 221.3 | 158.4 | 143.6 | 129.4 | 0.1 | 78.9 | 168.5 | 170.1 |
| 6 | 141.3 | 153.1 | 198.3 | 141.2 | 141.3 | 128.7 | 0.1 | 82.9 | 139.2 | 141.1 |
| 7 | 140.0 | 152.8 | 182.9 | 132.9 | 140.0 | 128.0 | 0.1 | 83.5 | 117.8 | 119.3 |
| 8 | 139.7 | 153.3 | 178.3 | 130.2 | 139.7 | 127.5 | 0.1 | 85.2 | 110.8 | 111.9 |
| 9 | 138.2 | 148.8 | 172.7 | 120.2 | 138.2 | 119.2 | 0.1 | 89.0 | 103.6 | 104.4 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.435 | 0.446 | 0.830 | 0.606 | 0.435 | 0.387 | 0.917 | 1.249 |
| 2 | 0.440 | 0.471 | 0.814 | 0.627 | 0.440 | 0.424 | 0.987 | 1.211 |
| 3 | 0.436 | 0.470 | 0.791 | 0.609 | 0.436 | 0.422 | 0.991 | 1.174 |
| 4 | 0.438 | 0.459 | 0.737 | 0.541 | 0.438 | 0.402 | 0.939 | 1.050 |
| 5 | 0.430 | 0.445 | 0.663 | 0.465 | 0.430 | 0.380 | 0.901 | 0.828 |
| 6 | 0.423 | 0.450 | 0.593 | 0.416 | 0.423 | 0.379 | 0.910 | 0.593 |
| 7 | 0.419 | 0.451 | 0.547 | 0.392 | 0.419 | 0.378 | 0.914 | 0.547 |
| 8 | 0.418 | 0.453 | 0.533 | 0.385 | 0.418 | 0.376 | 0.912 | 0.533 |
| 9 | 0.413 | 0.439 | 0.516 | 0.355 | 0.413 | 0.352 | 0.863 | 0.516 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 3.0 | -1.7 | 8.1 | 0.456 | 0.789 | 0.116 | 0.116 | 0.057 | 0.057 |
| 2 | 10.00 | 2.8 | -2.0 | 6.7 | 0.406 | 0.883 | 0.063 | 0.063 | 0.032 | 0.032 |
| 3 | 15.00 | 3.1 | -2.1 | 7.1 | 0.410 | 0.886 | 0.063 | 0.063 | 0.032 | 0.032 |
| 4 | 30.00 | 3.6 | -3.5 | 9.6 | 0.469 | 0.882 | 0.066 | 0.066 | 0.035 | 0.035 |
| 5 | 50.00 | 5.0 | -5.3 | 14.0 | 0.524 | 0.888 | 0.064 | 0.064 | 0.035 | 0.035 |
| 6 | 70.00 | 6.2 | -7.2 | 16.2 | 0.546 | 0.927 | 0.045 | 0.045 | 0.025 | 0.025 |
| 7 | 85.00 | 6.9 | -8.0 | 15.2 | 0.533 | 0.937 | 0.039 | 0.039 | 0.021 | 0.021 |
| 8 | 90.00 | 7.2 | -8.0 | 12.8 | 0.532 | 0.931 | 0.043 | 0.043 | 0.023 | 0.023 |
| 9 | 95.00 | 7.6 | -7.8 | 9.3 | 0.577 | 0.860 | 0.091 | 0.091 | 0.048 | 0.048 |

TABLE VIII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR ROTOR

51B B AT 100 PERCENT DESIGN SPEED

(a) Reading number 1796

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 15.0 | 48.9 | 44.6 | 288.8 | 1.043 | 10.07 | 1.115 |
| 2 | 23.868 | 23.876 | -0.0 | 13.6 | 47.8 | 42.4 | 288.7 | 1.043 | 10.13 | 1.133 |
| 3 | 23.086 | 23.114 | -0.0 | 14.3 | 46.9 | 40.9 | 288.5 | 1.041 | 10.14 | 1.130 |
| 4 | 20.731 | 20.828 | 0. | 16.2 | 43.4 | 35.7 | 288.0 | 1.039 | 10.14 | 1.122 |
| 5 | 17.607 | 17.780 | -0.0 | 19.3 | 39.0 | 28.3 | 287.9 | 1.036 | 10.14 | 1.108 |
| 6 | 14.531 | 14.732 | -0.0 | 22.4 | 34.0 | 17.1 | 287.8 | 1.036 | 10.14 | 1.119 |
| 7 | 12.294 | 12.446 | -0.0 | 23.1 | 30.0 | 10.5 | 287.8 | 1.032 | 10.14 | 1.100 |
| 8 | 11.565 | 11.684 | -0.0 | 22.8 | 28.5 | 9.3 | 287.8 | 1.029 | 10.14 | 1.083 |
| 9 | 10.843 | 10.922 | -0.0 | 24.7 | 27.2 | 6.3 | 287.8 | 1.028 | 10.11 | 1.066 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 206.6 | 195.2 | 314.1 | 264.8 | 206.6 | 188.5 | -0.0 | 50.5 | 236.5 | 236.4 |
| 2 | 208.4 | 204.5 | 310.3 | 269.2 | 208.4 | 198.8 | -0.0 | 48.3 | 229.8 | 229.9 |
| 3 | 208.0 | 204.9 | 304.6 | 262.8 | 208.0 | 198.5 | -0.0 | 50.6 | 222.5 | 222.7 |
| 4 | 211.0 | 206.4 | 290.2 | 244.2 | 211.0 | 198.2 | 0. | 57.6 | 199.3 | 200.3 |
| 5 | 209.4 | 203.8 | 269.3 | 218.6 | 209.4 | 192.4 | -0.0 | 67.2 | 169.3 | 171.0 |
| 6 | 206.9 | 212.6 | 249.6 | 205.6 | 206.9 | 196.5 | -0.0 | 81.2 | 139.6 | 141.5 |
| 7 | 204.8 | 212.8 | 236.5 | 199.1 | 204.8 | 195.7 | -0.0 | 83.6 | 118.4 | 119.8 |
| 8 | 204.2 | 208.2 | 232.4 | 194.4 | 204.2 | 191.9 | -0.0 | 80.8 | 110.9 | 112.1 |
| 9 | 202.6 | 202.0 | 227.8 | 184.7 | 202.6 | 183.6 | -0.0 | 84.4 | 104.0 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.630 | 0.579 | 0.958 | 0.786 | 0.630 | 0.560 | 0.912 | 1.221 |
| 2 | 0.636 | 0.610 | 0.947 | 0.802 | 0.636 | 0.592 | 0.954 | 1.191 |
| 3 | 0.635 | 0.612 | 0.930 | 0.784 | 0.635 | 0.593 | 0.955 | 1.164 |
| 4 | 0.645 | 0.617 | 0.888 | 0.731 | 0.645 | 0.593 | 0.939 | 1.028 |
| 5 | 0.640 | 0.610 | 0.824 | 0.655 | 0.640 | 0.576 | 0.919 | 0.824 |
| 6 | 0.632 | 0.639 | 0.763 | 0.618 | 0.632 | 0.591 | 0.950 | 0.763 |
| 7 | 0.625 | 0.641 | 0.722 | 0.599 | 0.625 | 0.589 | 0.956 | 0.722 |
| 8 | 0.623 | 0.627 | 0.710 | 0.585 | 0.623 | 0.578 | 0.940 | 0.710 |
| 9 | 0.618 | 0.607 | 0.695 | 0.555 | 0.618 | 0.552 | 0.906 | 0.695 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -3.6 | -8.2 | 5.4 | 0.279 | 0.732 | 0.086 | 0.084 | 0.047 | 0.046 |
| 2 | 10.00 | -3.7 | -8.5 | 4.6 | 0.250 | 0.852 | 0.048 | 0.047 | 0.027 | 0.026 |
| 3 | 15.00 | -3.5 | -8.7 | 5.0 | 0.261 | 0.874 | 0.040 | 0.040 | 0.022 | 0.022 |
| 4 | 30.00 | -3.6 | -10.6 | 6.4 | 0.301 | 0.864 | 0.044 | 0.044 | 0.026 | 0.026 |
| 5 | 50.00 | -2.5 | -12.9 | 10.1 | 0.357 | 0.831 | 0.056 | 0.056 | 0.033 | 0.033 |
| 6 | 70.00 | -1.4 | -14.8 | 11.9 | 0.378 | 0.913 | 0.033 | 0.033 | 0.019 | 0.019 |
| 7 | 85.00 | -0.1 | -15.0 | 13.1 | 0.360 | 0.858 | 0.052 | 0.052 | 0.029 | 0.029 |
| 8 | 90.00 | 0.3 | -14.9 | 13.2 | 0.355 | 0.797 | 0.070 | 0.070 | 0.038 | 0.038 |
| 9 | 95.00 | 1.0 | -14.4 | 11.2 | 0.386 | 0.670 | 0.111 | 0.111 | 0.058 | 0.058 |

TABLE VIII. - Continued.

(b) Reading number 1797

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 20.3 | 50.1 | 44.8 | 288.9 | 1.054 | 10.07 | 1.157 |
| 2 | 23.868 | 23.876 | -0.0 | 18.1 | 48.8 | 42.4 | 288.7 | 1.051 | 10.13 | 1.172 |
| 3 | 23.086 | 23.114 | -0.0 | 18.4 | 47.9 | 40.5 | 288.6 | 1.050 | 10.14 | 1.171 |
| 4 | 20.731 | 20.828 | -0.0 | 20.6 | 44.5 | 35.0 | 288.0 | 1.047 | 10.14 | 1.164 |
| 5 | 17.607 | 17.780 | -0.0 | 23.5 | 40.0 | 26.4 | 287.9 | 1.044 | 10.14 | 1.151 |
| 6 | 14.531 | 14.732 | -0.0 | 25.3 | 35.1 | 16.9 | 287.9 | 1.039 | 10.14 | 1.134 |
| 7 | 12.294 | 12.446 | -0.0 | 25.7 | 31.1 | 11.3 | 287.8 | 1.031 | 10.14 | 1.098 |
| 8 | 11.565 | 11.684 | -0.0 | 25.6 | 29.7 | 9.4 | 287.8 | 1.029 | 10.14 | 1.090 |
| 9 | 10.843 | 10.922 | -0.0 | 27.4 | 28.3 | 5.8 | 287.8 | 1.029 | 10.11 | 1.082 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 197.9 | 185.3 | 308.6 | 244.7 | 197.9 | 173.7 | -0.0 | 64.4 | 236.8 | 236.7 |
| 2 | 200.2 | 194.6 | 304.2 | 250.3 | 200.2 | 185.0 | -0.0 | 60.4 | 229.0 | 229.0 |
| 3 | 200.4 | 196.8 | 298.8 | 245.8 | 200.4 | 186.8 | -0.0 | 62.1 | 221.6 | 221.9 |
| 4 | 203.2 | 198.7 | 284.7 | 227.1 | 203.2 | 185.9 | -0.0 | 69.9 | 199.4 | 200.3 |
| 5 | 201.6 | 199.8 | 263.2 | 204.5 | 201.6 | 183.1 | -0.1 | 79.7 | 169.2 | 170.8 |
| 6 | 198.6 | 201.7 | 242.9 | 190.6 | 198.6 | 182.3 | -0.0 | 86.2 | 139.8 | 141.7 |
| 7 | 195.9 | 194.7 | 228.7 | 178.9 | 195.9 | 175.4 | -0.0 | 84.5 | 118.0 | 119.5 |
| 8 | 195.3 | 193.6 | 224.9 | 176.9 | 195.3 | 174.6 | -0.0 | 83.7 | 111.3 | 112.5 |
| 9 | 193.5 | 190.2 | 219.8 | 169.6 | 193.5 | 168.8 | -0.0 | 87.6 | 104.1 | 104.9 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.601 | 0.545 | 0.938 | 0.720 | 0.601 | 0.511 | 0.878 | 1.239 |
| 2 | 0.609 | 0.575 | 0.926 | 0.740 | 0.609 | 0.547 | 0.924 | 1.200 |
| 3 | 0.610 | 0.583 | 0.909 | 0.728 | 0.610 | 0.553 | 0.932 | 1.170 |
| 4 | 0.620 | 0.590 | 0.868 | 0.675 | 0.620 | 0.552 | 0.915 | 1.045 |
| 5 | 0.615 | 0.595 | 0.802 | 0.609 | 0.615 | 0.545 | 0.909 | 0.802 |
| 6 | 0.605 | 0.603 | 0.740 | 0.569 | 0.605 | 0.545 | 0.918 | 0.740 |
| 7 | 0.596 | 0.583 | 0.696 | 0.535 | 0.596 | 0.525 | 0.896 | 0.696 |
| 8 | 0.594 | 0.580 | 0.684 | 0.530 | 0.594 | 0.523 | 0.894 | 0.684 |
| 9 | 0.588 | 0.569 | 0.668 | 0.507 | 0.588 | 0.505 | 0.872 | 0.668 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -2.3 | -7.0 | 5.6 | 0.366 | 0.788 | 0.087 | 0.085 | 0.047 | 0.046 |
| 2 | 10.00 | -2.6 | -7.5 | 4.6 | 0.327 | 0.903 | 0.039 | 0.038 | 0.022 | 0.021 |
| 3 | 15.00 | -2.5 | -7.8 | 4.6 | 0.332 | 0.922 | 0.031 | 0.031 | 0.018 | 0.018 |
| 4 | 30.00 | -2.5 | -9.5 | 5.7 | 0.379 | 0.934 | 0.027 | 0.027 | 0.016 | 0.016 |
| 5 | 50.00 | -1.5 | -11.8 | 8.3 | 0.427 | 0.933 | 0.029 | 0.029 | 0.017 | 0.017 |
| 6 | 70.00 | -0.2 | -13.6 | 11.7 | 0.435 | 0.945 | 0.023 | 0.023 | 0.014 | 0.014 |
| 7 | 85.00 | 0.9 | -14.0 | 13.8 | 0.428 | 0.868 | 0.050 | 0.050 | 0.028 | 0.028 |
| 8 | 90.00 | 1.5 | -13.7 | 13.4 | 0.418 | 0.856 | 0.053 | 0.053 | 0.029 | 0.029 |
| 9 | 95.00 | 2.1 | -13.3 | 10.7 | 0.440 | 0.774 | 0.087 | 0.087 | 0.046 | 0.046 |

TABLE VIII. - Continued.

(c) Reading number 1798

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 21.5 | 52.0 | 45.8 | 288.9 | 1.054 | 10.09 | 1.163 |
| 2 | 23.868 | 23.876 | -0.0 | 20.2 | 50.9 | 43.4 | 288.8 | 1.051 | 10.13 | 1.177 |
| 3 | 23.086 | 23.114 | -0.0 | 19.6 | 50.1 | 42.2 | 288.5 | 1.050 | 10.14 | 1.172 |
| 4 | 20.731 | 20.828 | -0.0 | 21.4 | 46.7 | 37.2 | 287.9 | 1.046 | 10.14 | 1.157 |
| 5 | 17.607 | 17.780 | -0.0 | 24.1 | 42.4 | 30.2 | 287.9 | 1.041 | 10.14 | 1.134 |
| 6 | 14.531 | 14.732 | -0.0 | 26.4 | 37.5 | 20.4 | 287.9 | 1.038 | 10.13 | 1.121 |
| 7 | 12.294 | 12.446 | 0.0 | 27.8 | 33.3 | 11.2 | 287.9 | 1.034 | 10.14 | 1.115 |
| 8 | 11.565 | 11.684 | -0.0 | 28.3 | 31.9 | 8.1 | 287.8 | 1.033 | 10.13 | 1.113 |
| 9 | 10.843 | 10.922 | -0.0 | 30.8 | 30.5 | 4.4 | 287.8 | 1.032 | 10.10 | 1.097 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 184.9 | 178.9 | 300.2 | 238.6 | 184.9 | 166.5 | -0.0 | 65.5 | 236.5 | 236.4 |
| 2 | 186.8 | 186.8 | 296.3 | 241.0 | 186.8 | 175.2 | -0.0 | 64.6 | 230.1 | 230.1 |
| 3 | 186.1 | 187.3 | 289.9 | 238.1 | 186.1 | 176.5 | -0.0 | 62.7 | 222.3 | 222.6 |
| 4 | 187.6 | 186.5 | 273.5 | 218.0 | 187.6 | 173.6 | -0.0 | 68.1 | 199.0 | 199.9 |
| 5 | 185.3 | 181.8 | 250.9 | 191.9 | 185.3 | 165.9 | -0.0 | 74.3 | 169.2 | 170.8 |
| 6 | 182.0 | 182.4 | 229.5 | 174.3 | 182.0 | 163.4 | -0.0 | 81.1 | 139.8 | 141.7 |
| 7 | 179.7 | 186.8 | 215.2 | 168.5 | 179.7 | 165.3 | 0.0 | 87.1 | 118.3 | 119.7 |
| 8 | 179.2 | 188.3 | 211.1 | 167.4 | 179.2 | 165.7 | -0.0 | 89.3 | 111.6 | 112.8 |
| 9 | 177.2 | 181.7 | 205.6 | 156.5 | 177.2 | 156.0 | -0.0 | 93.1 | 104.3 | 105.1 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.559 | 0.525 | 0.908 | 0.701 | 0.559 | 0.489 | 0.901 | 1.260 |
| 2 | 0.566 | 0.551 | 0.897 | 0.711 | 0.566 | 0.517 | 0.938 | 1.230 |
| 3 | 0.564 | 0.553 | 0.878 | 0.703 | 0.564 | 0.521 | 0.948 | 1.199 |
| 4 | 0.569 | 0.552 | 0.830 | 0.645 | 0.569 | 0.514 | 0.926 | 1.069 |
| 5 | 0.562 | 0.539 | 0.761 | 0.569 | 0.562 | 0.492 | 0.895 | 0.808 |
| 6 | 0.551 | 0.542 | 0.695 | 0.518 | 0.551 | 0.485 | 0.898 | 0.695 |
| 7 | 0.544 | 0.557 | 0.651 | 0.502 | 0.544 | 0.493 | 0.920 | 0.651 |
| 8 | 0.542 | 0.562 | 0.639 | 0.499 | 0.542 | 0.494 | 0.925 | 0.639 |
| 9 | 0.536 | 0.541 | 0.622 | 0.466 | 0.536 | 0.465 | 0.880 | 0.622 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -0.4 | -5.1 | 6.6 | 0.371 | 0.810 | 0.082 | 0.080 | 0.044 | 0.043 |
| 2 | 10.00 | -0.5 | -5.4 | 5.6 | 0.351 | 0.927 | 0.031 | 0.030 | 0.017 | 0.016 |
| 3 | 15.00 | -0.3 | -5.6 | 6.2 | 0.340 | 0.921 | 0.033 | 0.033 | 0.018 | 0.018 |
| 4 | 30.00 | -0.2 | -7.3 | 7.9 | 0.382 | 0.927 | 0.031 | 0.031 | 0.018 | 0.018 |
| 5 | 50.00 | 0.9 | -9.5 | 12.0 | 0.435 | 0.902 | 0.042 | 0.042 | 0.024 | 0.024 |
| 6 | 70.00 | 2.2 | -11.3 | 15.2 | 0.459 | 0.882 | 0.054 | 0.054 | 0.031 | 0.031 |
| 7 | 85.00 | 3.2 | -11.7 | 13.7 | 0.447 | 0.925 | 0.035 | 0.035 | 0.019 | 0.019 |
| 8 | 90.00 | 3.7 | -11.5 | 12.0 | 0.440 | 0.935 | 0.030 | 0.030 | 0.017 | 0.017 |
| 9 | 95.00 | 4.3 | -11.1 | 9.3 | 0.479 | 0.825 | 0.083 | 0.083 | 0.044 | 0.044 |

TABLE VIII. - Continued.

(d) Reading number 1800

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 25.2 | 54.1 | 46.5 | 288.9 | 1.060 | 10.10 | 1.179 |
| 2 | 23.868 | 23.876 | -0.0 | 22.5 | 52.9 | 43.8 | 288.7 | 1.057 | 10.14 | 1.194 |
| 3 | 23.086 | 23.114 | -0.0 | 22.2 | 52.0 | 42.4 | 288.4 | 1.056 | 10.14 | 1.193 |
| 4 | 20.731 | 20.828 | -0.0 | 24.5 | 48.9 | 38.0 | 288.0 | 1.050 | 10.13 | 1.170 |
| 5 | 17.607 | 17.780 | -0.0 | 27.1 | 44.7 | 31.0 | 287.9 | 1.044 | 10.14 | 1.144 |
| 6 | 14.531 | 14.732 | -0.0 | 29.0 | 39.8 | 20.8 | 287.9 | 1.039 | 10.14 | 1.132 |
| 7 | 12.294 | 12.446 | -0.0 | 30.6 | 35.6 | 11.3 | 287.9 | 1.035 | 10.13 | 1.119 |
| 8 | 11.565 | 11.684 | -0.0 | 30.5 | 34.0 | 8.3 | 287.8 | 1.034 | 10.13 | 1.117 |
| 9 | 10.843 | 10.922 | -0.0 | 33.3 | 32.6 | 4.4 | 287.9 | 1.033 | 10.10 | 1.101 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 170.9 | 171.2 | 291.7 | 225.1 | 170.9 | 154.9 | -0.0 | 72.9 | 236.4 | 236.3 |
| 2 | 173.3 | 180.5 | 287.3 | 231.1 | 173.3 | 166.7 | -0.0 | 69.2 | 229.1 | 229.2 |
| 3 | 173.7 | 181.8 | 282.2 | 228.0 | 173.7 | 168.3 | -0.0 | 68.8 | 222.4 | 222.6 |
| 4 | 174.4 | 178.2 | 265.1 | 205.7 | 174.4 | 162.1 | -0.0 | 74.0 | 199.6 | 200.6 |
| 5 | 171.4 | 172.9 | 241.2 | 179.6 | 171.4 | 153.9 | -0.0 | 78.8 | 169.6 | 171.3 |
| 6 | 167.8 | 173.5 | 218.5 | 162.3 | 167.8 | 151.8 | -0.0 | 84.2 | 139.9 | 141.8 |
| 7 | 165.1 | 175.7 | 203.1 | 154.2 | 165.1 | 151.2 | -0.0 | 89.4 | 118.2 | 119.7 |
| 8 | 164.8 | 177.2 | 198.8 | 154.2 | 164.8 | 152.6 | -0.0 | 90.0 | 111.2 | 112.3 |
| 9 | 163.0 | 170.7 | 193.4 | 143.0 | 163.0 | 142.6 | -0.0 | 93.8 | 104.0 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.515 | 0.500 | 0.879 | 0.658 | 0.515 | 0.453 | 0.906 | 1.284 |
| 2 | 0.522 | 0.530 | 0.866 | 0.678 | 0.522 | 0.489 | 0.962 | 1.247 |
| 3 | 0.524 | 0.534 | 0.851 | 0.670 | 0.524 | 0.495 | 0.969 | 1.220 |
| 4 | 0.527 | 0.525 | 0.801 | 0.606 | 0.527 | 0.478 | 0.930 | 1.094 |
| 5 | 0.517 | 0.510 | 0.728 | 0.530 | 0.517 | 0.454 | 0.898 | 0.856 |
| 6 | 0.506 | 0.514 | 0.659 | 0.480 | 0.506 | 0.449 | 0.904 | 0.659 |
| 7 | 0.497 | 0.521 | 0.612 | 0.458 | 0.497 | 0.449 | 0.916 | 0.612 |
| 8 | 0.497 | 0.526 | 0.599 | 0.458 | 0.497 | 0.453 | 0.926 | 0.599 |
| 9 | 0.491 | 0.506 | 0.582 | 0.424 | 0.491 | 0.423 | 0.875 | 0.582 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 1.7 | -2.9 | 7.3 | 0.419 | 0.809 | 0.094 | 0.092 | 0.049 | 0.048 |
| 2 | 10.00 | 1.5 | -3.4 | 6.1 | 0.377 | 0.910 | 0.043 | 0.043 | 0.024 | 0.023 |
| 3 | 15.00 | 1.6 | -3.6 | 6.5 | 0.374 | 0.927 | 0.036 | 0.035 | 0.020 | 0.020 |
| 4 | 30.00 | 1.9 | -5.1 | 8.7 | 0.425 | 0.914 | 0.041 | 0.041 | 0.023 | 0.023 |
| 5 | 50.00 | 3.2 | -7.2 | 12.8 | 0.476 | 0.898 | 0.050 | 0.050 | 0.029 | 0.029 |
| 6 | 70.00 | 4.4 | -9.0 | 15.6 | 0.496 | 0.918 | 0.043 | 0.043 | 0.025 | 0.025 |
| 7 | 85.00 | 5.5 | -9.4 | 13.9 | 0.491 | 0.933 | 0.036 | 0.036 | 0.020 | 0.020 |
| 8 | 90.00 | 5.8 | -9.4 | 12.3 | 0.473 | 0.939 | 0.033 | 0.033 | 0.018 | 0.018 |
| 9 | 95.00 | 6.3 | -9.0 | 9.3 | 0.518 | 0.833 | 0.091 | 0.091 | 0.048 | 0.048 |

TABLE VIII. - Continued.

(e) Reading number 1801

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 27.9 | 55.3 | 47.0 | 288.8 | 1.064 | 10.10 | 1.187 |
| 2 | 23.868 | 23.876 | -0.0 | 23.9 | 54.1 | 44.3 | 288.7 | 1.060 | 10.14 | 1.204 |
| 3 | 23.086 | 23.114 | -0.0 | 24.6 | 53.2 | 42.9 | 288.4 | 1.058 | 10.14 | 1.193 |
| 4 | 20.731 | 20.828 | -0.0 | 26.6 | 50.1 | 38.2 | 288.1 | 1.052 | 10.14 | 1.174 |
| 5 | 17.607 | 17.780 | -0.0 | 28.6 | 45.9 | 31.4 | 287.9 | 1.045 | 10.13 | 1.146 |
| 6 | 14.531 | 14.732 | -0.0 | 30.7 | 41.1 | 21.2 | 287.9 | 1.040 | 10.13 | 1.133 |
| 7 | 12.294 | 12.446 | -0.0 | 31.7 | 36.8 | 11.7 | 287.9 | 1.036 | 10.13 | 1.123 |
| 8 | 11.565 | 11.684 | -0.0 | 32.1 | 35.3 | 8.5 | 287.8 | 1.034 | 10.13 | 1.117 |
| 9 | 10.843 | 10.922 | -0.0 | 34.8 | 33.9 | 4.4 | 288.0 | 1.034 | 10.11 | 1.103 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 164.2 | 167.4 | 288.7 | 217.2 | 164.2 | 148.0 | -0.0 | 78.3 | 237.4 | 237.3 |
| 2 | 166.5 | 177.6 | 284.1 | 226.7 | 166.5 | 162.3 | -0.0 | 72.0 | 230.2 | 230.2 |
| 3 | 165.9 | 175.8 | 276.7 | 218.3 | 165.9 | 159.9 | -0.0 | 73.1 | 221.4 | 221.6 |
| 4 | 166.8 | 173.8 | 259.9 | 197.8 | 166.8 | 155.4 | -0.0 | 77.8 | 199.3 | 200.2 |
| 5 | 163.7 | 168.0 | 235.2 | 172.9 | 163.7 | 147.6 | -0.0 | 80.3 | 168.8 | 170.5 |
| 6 | 160.0 | 167.9 | 212.5 | 154.8 | 160.0 | 144.4 | -0.0 | 85.8 | 139.8 | 141.7 |
| 7 | 158.3 | 171.0 | 197.8 | 148.6 | 158.3 | 145.5 | -0.0 | 89.9 | 118.6 | 120.0 |
| 8 | 157.3 | 170.9 | 192.7 | 146.3 | 157.3 | 144.7 | -0.0 | 90.9 | 111.4 | 112.5 |
| 9 | 155.2 | 165.5 | 187.0 | 136.2 | 155.2 | 135.8 | -0.0 | 94.6 | 104.2 | 105.0 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.494 | 0.488 | 0.868 | 0.633 | 0.494 | 0.431 | 0.901 | 1.303 |
| 2 | 0.501 | 0.520 | 0.855 | 0.664 | 0.501 | 0.475 | 0.975 | 1.266 |
| 3 | 0.499 | 0.515 | 0.833 | 0.640 | 0.499 | 0.469 | 0.964 | 1.226 |
| 4 | 0.502 | 0.511 | 0.783 | 0.581 | 0.502 | 0.457 | 0.932 | 1.103 |
| 5 | 0.493 | 0.495 | 0.708 | 0.509 | 0.493 | 0.435 | 0.901 | 0.867 |
| 6 | 0.481 | 0.496 | 0.639 | 0.457 | 0.481 | 0.426 | 0.902 | 0.639 |
| 7 | 0.476 | 0.507 | 0.595 | 0.440 | 0.476 | 0.431 | 0.919 | 0.595 |
| 8 | 0.473 | 0.507 | 0.579 | 0.434 | 0.473 | 0.429 | 0.920 | 0.579 |
| 9 | 0.466 | 0.490 | 0.561 | 0.403 | 0.466 | 0.402 | 0.875 | 0.561 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 2.9 | -1.7 | 7.8 | 0.454 | 0.792 | 0.110 | 0.109 | 0.057 | 0.056 |
| 2 | 10.00 | 2.7 | -2.2 | 6.5 | 0.393 | 0.906 | 0.049 | 0.048 | 0.026 | 0.026 |
| 3 | 15.00 | 2.8 | -2.5 | 6.9 | 0.408 | 0.896 | 0.054 | 0.054 | 0.029 | 0.029 |
| 4 | 30.00 | 3.1 | -3.9 | 8.9 | 0.454 | 0.897 | 0.054 | 0.054 | 0.030 | 0.030 |
| 5 | 50.00 | 4.4 | -6.0 | 13.2 | 0.495 | 0.888 | 0.059 | 0.059 | 0.034 | 0.034 |
| 6 | 70.00 | 5.8 | -7.6 | 16.0 | 0.521 | 0.909 | 0.051 | 0.051 | 0.029 | 0.029 |
| 7 | 85.00 | 6.7 | -8.2 | 14.3 | 0.508 | 0.945 | 0.031 | 0.031 | 0.017 | 0.017 |
| 8 | 90.00 | 7.1 | -8.1 | 12.5 | 0.500 | 0.931 | 0.039 | 0.039 | 0.021 | 0.021 |
| 9 | 95.00 | 7.7 | -7.7 | 9.3 | 0.540 | 0.843 | 0.093 | 0.093 | 0.049 | 0.049 |

TABLE VIII. - Concluded.

(f) Reading number 1807

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 28.5 | 56.0 | 47.0 | 288.9 | 1.067 | 10.10 | 1.194 |
| 2 | 23.868 | 23.876 | -0.0 | 24.7 | 54.7 | 44.3 | 288.8 | 1.062 | 10.14 | 1.206 |
| 3 | 23.086 | 23.114 | -0.0 | 25.0 | 53.7 | 43.1 | 288.4 | 1.059 | 10.14 | 1.198 |
| 4 | 20.731 | 20.828 | -0.0 | 27.4 | 50.6 | 38.5 | 288.0 | 1.054 | 10.13 | 1.176 |
| 5 | 17.607 | 17.780 | -0.0 | 30.1 | 46.6 | 31.2 | 287.9 | 1.047 | 10.14 | 1.150 |
| 6 | 14.531 | 14.732 | -0.0 | 31.7 | 41.8 | 21.2 | 287.8 | 1.041 | 10.13 | 1.134 |
| 7 | 12.294 | 12.446 | -0.0 | 32.3 | 37.4 | 11.9 | 287.9 | 1.036 | 10.14 | 1.121 |
| 8 | 11.565 | 11.684 | -0.0 | 32.8 | 35.8 | 8.6 | 287.9 | 1.034 | 10.13 | 1.115 |
| 9 | 10.843 | 10.922 | -0.0 | 35.5 | 34.4 | 4.4 | 287.9 | 1.034 | 10.10 | 1.103 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 159.8 | 167.2 | 286.2 | 215.2 | 159.8 | 146.8 | -0.1 | 79.9 | 237.3 | 237.2 |
| 2 | 162.4 | 175.9 | 281.1 | 223.2 | 162.4 | 159.8 | -0.1 | 73.5 | 229.3 | 229.4 |
| 3 | 163.4 | 174.9 | 275.9 | 217.3 | 163.4 | 158.6 | -0.1 | 73.9 | 222.2 | 222.5 |
| 4 | 163.7 | 172.0 | 258.0 | 195.0 | 163.7 | 152.7 | -0.1 | 79.0 | 199.4 | 200.3 |
| 5 | 160.2 | 166.9 | 233.3 | 168.9 | 160.2 | 144.4 | -0.1 | 83.7 | 169.6 | 171.2 |
| 6 | 156.5 | 165.4 | 209.8 | 150.9 | 156.5 | 140.7 | -0.1 | 87.0 | 139.8 | 141.7 |
| 7 | 154.3 | 167.4 | 194.1 | 144.7 | 154.3 | 141.6 | -0.1 | 89.4 | 117.7 | 119.1 |
| 8 | 153.9 | 167.6 | 189.8 | 142.6 | 153.9 | 140.9 | -0.1 | 90.7 | 111.0 | 112.1 |
| 9 | 152.2 | 162.9 | 184.4 | 133.0 | 152.2 | 132.6 | -0.1 | 94.6 | 104.1 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.480 | 0.486 | 0.859 | 0.626 | 0.480 | 0.427 | 0.919 | 1.311 |
| 2 | 0.488 | 0.514 | 0.845 | 0.653 | 0.488 | 0.467 | 0.984 | 1.268 |
| 3 | 0.491 | 0.512 | 0.830 | 0.636 | 0.491 | 0.464 | 0.971 | 1.236 |
| 4 | 0.493 | 0.505 | 0.777 | 0.572 | 0.493 | 0.448 | 0.933 | 1.109 |
| 5 | 0.482 | 0.491 | 0.702 | 0.497 | 0.482 | 0.425 | 0.901 | 0.880 |
| 6 | 0.470 | 0.488 | 0.631 | 0.445 | 0.470 | 0.415 | 0.899 | 0.631 |
| 7 | 0.463 | 0.495 | 0.583 | 0.428 | 0.463 | 0.419 | 0.918 | 0.583 |
| 8 | 0.462 | 0.496 | 0.570 | 0.422 | 0.462 | 0.417 | 0.916 | 0.570 |
| 9 | 0.457 | 0.482 | 0.553 | 0.393 | 0.457 | 0.392 | 0.871 | 0.553 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN- | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 3.6 | -1.0 | 7.8 | 0.461 | 0.781 | 0.123 | 0.121 | 0.064 | 0.063 |
| 2 | 10.00 | 3.3 | -1.6 | 6.5 | 0.403 | 0.893 | 0.058 | 0.057 | 0.031 | 0.031 |
| 3 | 15.00 | 3.3 | -2.0 | 7.2 | 0.412 | 0.904 | 0.051 | 0.051 | 0.028 | 0.028 |
| 4 | 30.00 | 3.7 | -3.4 | 9.1 | 0.464 | 0.884 | 0.062 | 0.062 | 0.035 | 0.035 |
| 5 | 50.00 | 5.1 | -5.2 | 13.0 | 0.518 | 0.865 | 0.076 | 0.076 | 0.044 | 0.044 |
| 6 | 70.00 | 6.4 | -7.0 | 16.0 | 0.538 | 0.902 | 0.057 | 0.057 | 0.033 | 0.033 |
| 7 | 85.00 | 7.2 | -7.7 | 14.4 | 0.517 | 0.926 | 0.043 | 0.043 | 0.024 | 0.024 |
| 8 | 90.00 | 7.6 | -7.6 | 12.6 | 0.512 | 0.917 | 0.049 | 0.049 | 0.026 | 0.026 |
| 9 | 95.00 | 8.2 | -7.2 | 9.3 | 0.551 | 0.839 | 0.098 | 0.098 | 0.051 | 0.051 |

TABLE IX. - BLADE-ELEMENT DATA AT BLADE EDGES FOR ROTOR 51B C

AT 100 PERCENT DESIGN SPEED

(a) Reading number 1830

| RP | RADIUS | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 16.1 | 52.4 | 50.0 | 288.8 | 1.038 | 10.09 | 1.105 |
| 2 | 23.868 | 23.876 | 0.0 | 14.3 | 51.3 | 47.8 | 288.8 | 1.036 | 10.13 | 1.118 |
| 3 | 23.086 | 23.114 | 0.0 | 14.4 | 50.2 | 46.2 | 288.7 | 1.035 | 10.13 | 1.118 |
| 4 | 20.731 | 20.828 | 0.0 | 16.5 | 46.8 | 40.5 | 287.9 | 1.035 | 10.13 | 1.121 |
| 5 | 17.607 | 17.780 | 0.0 | 20.1 | 42.3 | 31.9 | 287.9 | 1.035 | 10.14 | 1.121 |
| 6 | 14.531 | 14.732 | 0.0 | 22.3 | 37.2 | 22.1 | 287.9 | 1.033 | 10.14 | 1.113 |
| 7 | 12.294 | 12.446 | 0.0 | 22.9 | 32.9 | 15.9 | 287.8 | 1.027 | 10.14 | 1.088 |
| 8 | 11.565 | 11.684 | 0.0 | 22.4 | 31.3 | 14.9 | 287.9 | 1.023 | 10.14 | 1.074 |
| 9 | 10.843 | 10.922 | 0.0 | 23.7 | 30.1 | 12.8 | 287.8 | 1.023 | 10.11 | 1.059 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 182.5 | 166.6 | 299.2 | 249.1 | 182.5 | 160.1 | 0.0 | 46.2 | 237.2 | 237.1 |
| 2 | 183.6 | 174.4 | 293.8 | 251.6 | 183.6 | 169.0 | 0.0 | 43.0 | 229.4 | 229.4 |
| 3 | 184.2 | 176.0 | 288.0 | 246.5 | 184.2 | 170.5 | 0.0 | 43.7 | 221.4 | 221.7 |
| 4 | 186.2 | 180.6 | 272.2 | 227.8 | 186.2 | 173.2 | 0.0 | 51.4 | 198.5 | 199.4 |
| 5 | 185.3 | 183.5 | 250.6 | 203.2 | 185.3 | 172.4 | 0.0 | 63.0 | 168.8 | 170.5 |
| 6 | 183.7 | 187.1 | 230.6 | 186.9 | 183.7 | 173.1 | 0.0 | 70.9 | 139.4 | 141.3 |
| 7 | 181.8 | 182.8 | 216.5 | 175.0 | 181.8 | 168.4 | 0.0 | 71.2 | 117.6 | 119.0 |
| 8 | 181.4 | 178.3 | 212.4 | 170.6 | 181.4 | 164.9 | 0.0 | 67.9 | 110.5 | 111.6 |
| 9 | 179.2 | 171.4 | 207.1 | 160.9 | 179.2 | 156.9 | 0.0 | 69.0 | 103.8 | 104.6 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.552 | 0.491 | 0.905 | 0.735 | 0.552 | 0.472 | 0.877 | 1.067 |
| 2 | 0.555 | 0.516 | 0.889 | 0.745 | 0.555 | 0.500 | 0.920 | 1.029 |
| 3 | 0.557 | 0.522 | 0.872 | 0.730 | 0.557 | 0.505 | 0.926 | 0.994 |
| 4 | 0.565 | 0.537 | 0.825 | 0.677 | 0.565 | 0.515 | 0.930 | 0.828 |
| 5 | 0.562 | 0.546 | 0.760 | 0.604 | 0.562 | 0.513 | 0.930 | 0.760 |
| 6 | 0.556 | 0.558 | 0.699 | 0.557 | 0.556 | 0.516 | 0.943 | 0.699 |
| 7 | 0.551 | 0.546 | 0.656 | 0.523 | 0.551 | 0.503 | 0.926 | 0.656 |
| 8 | 0.549 | 0.533 | 0.643 | 0.510 | 0.549 | 0.493 | 0.909 | 0.643 |
| 9 | 0.542 | 0.511 | 0.627 | 0.480 | 0.542 | 0.468 | 0.876 | 0.627 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -6.0 | -10.7 | 4.8 | 0.285 | 0.753 | 0.077 | 0.077 | 0.038 | 0.038 |
| 2 | 10.00 | -6.1 | -11.0 | 4.0 | 0.254 | 0.892 | 0.033 | 0.033 | 0.017 | 0.017 |
| 3 | 15.00 | -6.2 | -11.4 | 4.3 | 0.257 | 0.920 | 0.024 | 0.024 | 0.012 | 0.012 |
| 4 | 30.00 | -6.1 | -13.2 | 5.2 | 0.298 | 0.940 | 0.020 | 0.020 | 0.011 | 0.011 |
| 5 | 50.00 | -5.2 | -15.5 | 7.7 | 0.359 | 0.951 | 0.018 | 0.018 | 0.010 | 0.010 |
| 6 | 70.00 | -4.2 | -17.6 | 10.6 | 0.380 | 0.946 | 0.022 | 0.022 | 0.012 | 0.012 |
| 7 | 85.00 | -3.2 | -18.1 | 12.4 | 0.379 | 0.919 | 0.029 | 0.029 | 0.016 | 0.016 |
| 8 | 90.00 | -2.9 | -18.1 | 12.9 | 0.373 | 0.898 | 0.033 | 0.033 | 0.018 | 0.018 |
| 9 | 95.00 | -2.1 | -17.5 | 11.7 | 0.400 | 0.707 | 0.100 | 0.100 | 0.052 | 0.052 |

TABLE IX. - Continued.

(b) Reading number 1829

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 19.9 | 54.6 | 50.7 | 288.7 | 1.046 | 10.10 | 1.141 |
| 2 | 23.868 | 23.876 | 0.0 | 18.1 | 53.4 | 48.2 | 288.7 | 1.043 | 10.13 | 1.151 |
| 3 | 23.086 | 23.114 | 0.0 | 18.0 | 52.4 | 46.9 | 288.5 | 1.042 | 10.14 | 1.150 |
| 4 | 20.731 | 20.828 | 0.0 | 20.5 | 49.2 | 41.3 | 288.1 | 1.042 | 10.13 | 1.147 |
| 5 | 17.607 | 17.780 | 0.0 | 23.7 | 44.7 | 32.9 | 288.0 | 1.038 | 10.14 | 1.136 |
| 6 | 14.531 | 14.732 | 0.0 | 25.9 | 39.7 | 23.3 | 287.9 | 1.035 | 10.14 | 1.121 |
| 7 | 12.294 | 12.446 | 0.0 | 26.3 | 35.4 | 17.0 | 287.8 | 1.029 | 10.14 | 1.095 |
| 8 | 11.565 | 11.684 | 0.0 | 26.0 | 33.8 | 15.2 | 287.9 | 1.026 | 10.14 | 1.086 |
| 9 | 10.843 | 10.922 | 0.0 | 28.4 | 32.4 | 11.5 | 287.8 | 1.026 | 10.11 | 1.077 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 168.0 | 158.9 | 290.2 | 235.9 | 168.0 | 149.4 | 0.0 | 54.0 | 236.6 | 236.5 |
| 2 | 170.2 | 166.8 | 285.2 | 237.7 | 170.2 | 158.5 | 0.0 | 51.8 | 228.9 | 229.0 |
| 3 | 170.6 | 167.8 | 279.9 | 233.4 | 170.6 | 159.6 | 0.0 | 51.9 | 221.9 | 222.2 |
| 4 | 171.8 | 170.6 | 263.0 | 212.5 | 171.8 | 159.7 | 0.0 | 59.9 | 199.1 | 200.1 |
| 5 | 170.6 | 171.3 | 240.0 | 186.9 | 170.6 | 156.9 | 0.0 | 68.9 | 168.8 | 170.4 |
| 6 | 167.9 | 171.8 | 218.3 | 168.1 | 167.9 | 154.5 | 0.0 | 75.1 | 139.6 | 141.5 |
| 7 | 166.2 | 166.6 | 203.8 | 156.2 | 166.2 | 149.4 | 0.0 | 73.7 | 118.0 | 119.5 |
| 8 | 166.1 | 164.7 | 199.9 | 153.3 | 166.1 | 148.0 | 0.0 | 72.2 | 111.2 | 112.3 |
| 9 | 163.9 | 160.0 | 194.1 | 143.5 | 163.9 | 140.7 | 0.0 | 76.2 | 104.0 | 104.7 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.506 | 0.466 | 0.874 | 0.692 | 0.506 | 0.438 | 0.890 | 1.106 |
| 2 | 0.513 | 0.491 | 0.859 | 0.700 | 0.513 | 0.466 | 0.931 | 1.066 |
| 3 | 0.514 | 0.495 | 0.844 | 0.688 | 0.514 | 0.470 | 0.936 | 1.039 |
| 4 | 0.518 | 0.504 | 0.794 | 0.627 | 0.518 | 0.471 | 0.930 | 0.913 |
| 5 | 0.515 | 0.507 | 0.724 | 0.553 | 0.515 | 0.464 | 0.919 | 0.724 |
| 6 | 0.506 | 0.509 | 0.658 | 0.498 | 0.506 | 0.458 | 0.920 | 0.658 |
| 7 | 0.501 | 0.495 | 0.614 | 0.464 | 0.501 | 0.444 | 0.899 | 0.614 |
| 8 | 0.500 | 0.489 | 0.602 | 0.455 | 0.500 | 0.440 | 0.891 | 0.602 |
| 9 | 0.494 | 0.475 | 0.585 | 0.426 | 0.494 | 0.417 | 0.858 | 0.585 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -3.8 | -8.5 | 5.5 | 0.329 | 0.842 | 0.061 | 0.061 | 0.030 | 0.030 |
| 2 | 10.00 | -4.1 | -9.0 | 4.4 | 0.304 | 0.946 | 0.020 | 0.020 | 0.010 | 0.010 |
| 3 | 15.00 | -4.0 | -9.2 | 4.9 | 0.304 | 0.963 | 0.014 | 0.014 | 0.007 | 0.007 |
| 4 | 30.00 | -3.7 | -10.8 | 6.0 | 0.355 | 0.962 | 0.016 | 0.016 | 0.008 | 0.008 |
| 5 | 50.00 | -2.8 | -13.2 | 8.7 | 0.414 | 0.969 | 0.014 | 0.014 | 0.008 | 0.008 |
| 6 | 70.00 | -1.6 | -15.1 | 11.7 | 0.443 | 0.957 | 0.020 | 0.020 | 0.011 | 0.011 |
| 7 | 85.00 | -0.8 | -15.7 | 13.6 | 0.439 | 0.914 | 0.037 | 0.037 | 0.020 | 0.020 |
| 8 | 90.00 | -0.4 | -15.6 | 13.2 | 0.432 | 0.909 | 0.038 | 0.038 | 0.020 | 0.020 |
| 9 | 95.00 | 0.2 | -15.2 | 10.4 | 0.469 | 0.820 | 0.077 | 0.077 | 0.040 | 0.040 |

TABLE IX. - Continued.

(c) Reading number 1828

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 21.2 | 56.5 | 51.1 | 289.0 | 1.048 | 10.10 | 1.152 |
| 2 | 23.868 | 23.876 | 0.0 | 19.7 | 55.4 | 49.1 | 288.9 | 1.046 | 10.13 | 1.157 |
| 3 | 23.086 | 23.114 | 0.0 | 19.7 | 54.5 | 47.8 | 288.2 | 1.044 | 10.14 | 1.153 |
| 4 | 20.731 | 20.828 | 0.0 | 22.2 | 51.3 | 43.3 | 288.0 | 1.040 | 10.14 | 1.139 |
| 5 | 17.607 | 17.780 | -0.0 | 25.1 | 47.1 | 36.2 | 288.0 | 1.036 | 10.14 | 1.124 |
| 6 | 14.531 | 14.732 | 0.0 | 27.3 | 42.0 | 26.0 | 287.9 | 1.034 | 10.14 | 1.115 |
| 7 | 12.294 | 12.446 | 0.0 | 28.3 | 37.5 | 18.0 | 287.8 | 1.029 | 10.13 | 1.097 |
| 8 | 11.565 | 11.684 | 0.0 | 28.7 | 36.0 | 15.0 | 287.9 | 1.027 | 10.13 | 1.094 |
| 9 | 10.843 | 10.922 | 0.0 | 31.5 | 34.7 | 11.1 | 288.0 | 1.028 | 10.11 | 1.084 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 156.3 | 155.7 | 283.5 | 231.3 | 156.3 | 145.2 | 0.0 | 56.3 | 236.5 | 236.4 |
| 2 | 157.9 | 160.8 | 278.4 | 231.5 | 157.9 | 151.4 | 0.0 | 54.3 | 229.3 | 229.3 |
| 3 | 158.0 | 160.9 | 272.0 | 225.7 | 158.0 | 151.4 | 0.0 | 54.3 | 221.4 | 221.6 |
| 4 | 158.5 | 159.1 | 253.6 | 202.5 | 158.5 | 147.3 | 0.0 | 60.0 | 198.0 | 198.9 |
| 5 | 156.7 | 156.4 | 230.1 | 175.6 | 156.7 | 141.6 | -0.0 | 66.3 | 168.4 | 170.1 |
| 6 | 154.7 | 158.4 | 208.2 | 156.5 | 154.7 | 140.7 | 0.0 | 72.7 | 139.3 | 141.3 |
| 7 | 153.2 | 156.4 | 193.0 | 144.8 | 153.2 | 137.7 | 0.0 | 74.2 | 117.5 | 119.0 |
| 8 | 152.3 | 156.4 | 188.3 | 142.1 | 152.3 | 137.2 | 0.0 | 75.1 | 110.7 | 111.9 |
| 9 | 150.3 | 151.8 | 182.8 | 131.9 | 150.3 | 129.5 | 0.0 | 79.3 | 104.0 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.469 | 0.456 | 0.850 | 0.677 | 0.469 | 0.425 | 0.929 | 1.135 |
| 2 | 0.474 | 0.472 | 0.835 | 0.679 | 0.474 | 0.444 | 0.959 | 1.101 |
| 3 | 0.475 | 0.473 | 0.817 | 0.663 | 0.475 | 0.445 | 0.959 | 1.069 |
| 4 | 0.476 | 0.468 | 0.762 | 0.596 | 0.476 | 0.434 | 0.929 | 0.943 |
| 5 | 0.471 | 0.461 | 0.691 | 0.518 | 0.471 | 0.418 | 0.904 | 0.691 |
| 6 | 0.464 | 0.468 | 0.625 | 0.463 | 0.464 | 0.416 | 0.910 | 0.625 |
| 7 | 0.460 | 0.463 | 0.580 | 0.429 | 0.460 | 0.408 | 0.899 | 0.580 |
| 8 | 0.457 | 0.463 | 0.565 | 0.421 | 0.457 | 0.407 | 0.901 | 0.565 |
| 9 | 0.451 | 0.449 | 0.548 | 0.390 | 0.451 | 0.383 | 0.861 | 0.548 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -1.9 | -6.5 | 5.9 | 0.335 | 0.862 | 0.058 | 0.058 | 0.028 | 0.028 |
| 2 | 10.00 | -2.0 | -6.9 | 5.4 | 0.315 | 0.927 | 0.030 | 0.030 | 0.015 | 0.015 |
| 3 | 15.00 | -1.9 | -7.2 | 5.9 | 0.319 | 0.936 | 0.027 | 0.027 | 0.013 | 0.013 |
| 4 | 30.00 | -1.6 | -8.7 | 8.0 | 0.371 | 0.938 | 0.026 | 0.026 | 0.014 | 0.014 |
| 5 | 50.00 | -0.4 | -10.8 | 12.0 | 0.431 | 0.931 | 0.031 | 0.031 | 0.017 | 0.017 |
| 6 | 70.00 | 0.6 | -12.8 | 14.5 | 0.464 | 0.933 | 0.033 | 0.033 | 0.018 | 0.018 |
| 7 | 85.00 | 1.4 | -13.5 | 14.6 | 0.469 | 0.944 | 0.027 | 0.027 | 0.014 | 0.014 |
| 8 | 90.00 | 1.8 | -13.4 | 13.0 | 0.465 | 0.946 | 0.026 | 0.026 | 0.014 | 0.014 |
| 9 | 95.00 | 2.5 | -12.9 | 10.0 | 0.508 | 0.821 | 0.093 | 0.093 | 0.048 | 0.048 |

TABLE IX. - Continued.

(d) Reading number 1827

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | 0.0 | 24.2 | 58.4 | 51.9 | 288.9 | 1.053 | 10.10 | 1.164 |
| 2 | 23.868 | 23.876 | 0.0 | 21.8 | 57.2 | 49.9 | 288.7 | 1.050 | 10.13 | 1.168 |
| 3 | 23.086 | 23.114 | 0.0 | 22.1 | 56.3 | 48.5 | 288.5 | 1.048 | 10.14 | 1.165 |
| 4 | 20.731 | 20.828 | 0.0 | 24.7 | 53.2 | 43.8 | 288.1 | 1.045 | 10.13 | 1.153 |
| 5 | 17.607 | 17.780 | 0.0 | 27.4 | 49.1 | 38.1 | 287.9 | 1.039 | 10.14 | 1.126 |
| 6 | 14.531 | 14.732 | 0.0 | 30.0 | 44.1 | 27.2 | 287.7 | 1.035 | 10.14 | 1.118 |
| 7 | 12.294 | 12.446 | 0.0 | 30.7 | 39.6 | 18.2 | 287.9 | 1.031 | 10.14 | 1.106 |
| 8 | 11.565 | 11.684 | 0.0 | 31.3 | 38.0 | 14.9 | 287.8 | 1.029 | 10.13 | 1.100 |
| 9 | 10.843 | 10.922 | 0.0 | 34.0 | 36.5 | 11.2 | 287.9 | 1.029 | 10.11 | 1.088 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 146.0 | 150.8 | 278.4 | 222.6 | 146.0 | 137.5 | 0.0 | 61.9 | 237.1 | 237.0 |
| 2 | 147.9 | 155.7 | 272.9 | 224.4 | 147.9 | 144.6 | 0.0 | 57.9 | 229.4 | 229.5 |
| 3 | 148.1 | 156.1 | 266.9 | 218.3 | 148.1 | 144.6 | 0.0 | 58.9 | 222.1 | 222.4 |
| 4 | 149.2 | 155.4 | 249.1 | 195.6 | 149.2 | 141.1 | 0.0 | 65.0 | 199.5 | 200.4 |
| 5 | 146.8 | 147.8 | 224.1 | 166.8 | 146.8 | 131.2 | 0.0 | 68.0 | 169.3 | 171.0 |
| 6 | 143.8 | 149.6 | 200.3 | 145.7 | 143.8 | 129.6 | 0.0 | 74.8 | 139.6 | 141.5 |
| 7 | 142.2 | 150.5 | 184.7 | 136.3 | 142.2 | 129.5 | 0.0 | 76.8 | 117.8 | 119.3 |
| 8 | 142.0 | 150.3 | 180.2 | 133.0 | 142.0 | 128.5 | 0.0 | 78.0 | 111.0 | 112.1 |
| 9 | 140.2 | 144.3 | 174.4 | 121.9 | 140.2 | 119.6 | 0.0 | 80.7 | 103.7 | 104.5 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.437 | 0.439 | 0.832 | 0.649 | 0.437 | 0.401 | 0.942 | 1.166 |
| 2 | 0.443 | 0.455 | 0.817 | 0.656 | 0.443 | 0.423 | 0.978 | 1.128 |
| 3 | 0.444 | 0.457 | 0.799 | 0.639 | 0.444 | 0.423 | 0.976 | 1.098 |
| 4 | 0.447 | 0.456 | 0.747 | 0.574 | 0.447 | 0.414 | 0.946 | 0.976 |
| 5 | 0.440 | 0.434 | 0.671 | 0.490 | 0.440 | 0.386 | 0.894 | 0.739 |
| 6 | 0.431 | 0.441 | 0.600 | 0.429 | 0.431 | 0.382 | 0.901 | 0.600 |
| 7 | 0.426 | 0.444 | 0.553 | 0.402 | 0.426 | 0.382 | 0.910 | 0.553 |
| 8 | 0.425 | 0.444 | 0.540 | 0.393 | 0.425 | 0.380 | 0.905 | 0.540 |
| 9 | 0.419 | 0.426 | 0.522 | 0.360 | 0.419 | 0.353 | 0.853 | 0.522 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -0.0 | -4.7 | 6.7 | 0.370 | 0.836 | 0.078 | 0.078 | 0.037 | 0.037 |
| 2 | 10.00 | -0.3 | -5.1 | 6.1 | 0.338 | 0.918 | 0.038 | 0.038 | 0.018 | 0.018 |
| 3 | 15.00 | -0.1 | -5.4 | 6.5 | 0.347 | 0.924 | 0.035 | 0.035 | 0.017 | 0.017 |
| 4 | 30.00 | 0.3 | -6.8 | 8.5 | 0.402 | 0.912 | 0.043 | 0.043 | 0.022 | 0.022 |
| 5 | 50.00 | 1.6 | -8.8 | 13.9 | 0.460 | 0.892 | 0.054 | 0.054 | 0.028 | 0.028 |
| 6 | 70.00 | 2.8 | -10.6 | 15.7 | 0.504 | 0.916 | 0.047 | 0.047 | 0.026 | 0.026 |
| 7 | 85.00 | 3.5 | -11.4 | 14.7 | 0.499 | 0.937 | 0.036 | 0.036 | 0.019 | 0.019 |
| 8 | 90.00 | 3.8 | -11.4 | 12.9 | 0.500 | 0.940 | 0.033 | 0.033 | 0.018 | 0.018 |
| 9 | 95.00 | 4.3 | -11.1 | 10.1 | 0.547 | 0.841 | 0.093 | 0.093 | 0.048 | 0.048 |

TABLE IX. - Continued.

(e) Reading number 1824

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.648 | 24.638 | -0.0 | 28.8 | 60.2 | 52.7 | 288.7 | 1.060 | 10.11 | 1.176 |
| 2 | 23.868 | 23.876 | -0.0 | 25.3 | 59.1 | 50.2 | 288.5 | 1.055 | 10.13 | 1.180 |
| 3 | 23.086 | 23.114 | -0.0 | 25.6 | 58.3 | 48.8 | 288.3 | 1.054 | 10.14 | 1.179 |
| 4 | 20.731 | 20.828 | -0.0 | 28.3 | 55.4 | 44.8 | 288.0 | 1.048 | 10.14 | 1.158 |
| 5 | 17.607 | 17.780 | -0.0 | 31.3 | 51.5 | 39.1 | 288.0 | 1.041 | 10.13 | 1.134 |
| 6 | 14.531 | 14.732 | -0.0 | 33.4 | 46.7 | 28.1 | 287.9 | 1.037 | 10.13 | 1.124 |
| 7 | 12.294 | 12.446 | -0.0 | 34.0 | 42.3 | 18.6 | 287.9 | 1.032 | 10.13 | 1.111 |
| 8 | 11.565 | 11.684 | -0.0 | 34.8 | 40.6 | 14.9 | 287.9 | 1.031 | 10.13 | 1.105 |
| 9 | 10.843 | 10.922 | -0.0 | 38.0 | 39.1 | 10.6 | 287.9 | 1.031 | 10.11 | 1.095 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 135.8 | 145.2 | 273.3 | 210.0 | 135.8 | 127.2 | -0.0 | 70.0 | 237.2 | 237.1 |
| 2 | 137.1 | 151.4 | 266.8 | 213.7 | 137.1 | 136.8 | -0.0 | 64.8 | 228.9 | 229.0 |
| 3 | 137.2 | 152.4 | 261.4 | 208.5 | 137.2 | 137.4 | -0.0 | 65.9 | 222.4 | 222.7 |
| 4 | 137.4 | 148.4 | 241.9 | 184.0 | 137.4 | 130.6 | -0.0 | 70.5 | 199.1 | 200.0 |
| 5 | 134.1 | 140.5 | 215.6 | 154.6 | 134.1 | 120.0 | -0.0 | 73.1 | 168.8 | 170.5 |
| 6 | 131.6 | 142.0 | 191.8 | 134.3 | 131.6 | 118.5 | -0.0 | 78.2 | 139.5 | 141.4 |
| 7 | 129.9 | 142.4 | 175.5 | 124.5 | 129.9 | 118.0 | -0.0 | 79.7 | 118.0 | 119.5 |
| 8 | 129.6 | 142.2 | 170.7 | 120.9 | 129.6 | 116.8 | -0.0 | 81.1 | 111.0 | 112.1 |
| 9 | 128.2 | 137.4 | 165.2 | 110.2 | 128.2 | 108.3 | -0.0 | 84.6 | 104.0 | 104.8 |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.405 | 0.421 | 0.815 | 0.609 | 0.405 | 0.369 | 0.937 | 1.194 |
| 2 | 0.409 | 0.441 | 0.797 | 0.623 | 0.409 | 0.399 | 0.998 | 1.152 |
| 3 | 0.410 | 0.445 | 0.781 | 0.608 | 0.410 | 0.401 | 1.001 | 1.127 |
| 4 | 0.411 | 0.434 | 0.723 | 0.538 | 0.411 | 0.382 | 0.951 | 1.002 |
| 5 | 0.400 | 0.412 | 0.644 | 0.453 | 0.400 | 0.352 | 0.895 | 0.780 |
| 6 | 0.393 | 0.417 | 0.573 | 0.394 | 0.393 | 0.348 | 0.901 | 0.573 |
| 7 | 0.388 | 0.419 | 0.524 | 0.366 | 0.388 | 0.347 | 0.908 | 0.524 |
| 8 | 0.387 | 0.419 | 0.509 | 0.356 | 0.387 | 0.344 | 0.901 | 0.509 |
| 9 | 0.383 | 0.404 | 0.493 | 0.324 | 0.383 | 0.319 | 0.844 | 0.493 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|------|--------|-------|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 1.8 | -2.9 | 7.5 | 0.427 | 0.789 | 0.116 | 0.116 | 0.054 | 0.054 |
| 2 | 10.00 | 1.6 | -3.2 | 6.4 | 0.382 | 0.882 | 0.062 | 0.062 | 0.030 | 0.030 |
| 3 | 15.00 | 1.9 | -3.3 | 6.8 | 0.390 | 0.892 | 0.058 | 0.058 | 0.028 | 0.028 |
| 4 | 30.00 | 2.5 | -4.6 | 9.5 | 0.449 | 0.886 | 0.062 | 0.062 | 0.032 | 0.032 |
| 5 | 50.00 | 4.1 | -6.3 | 14.9 | 0.511 | 0.893 | 0.060 | 0.060 | 0.031 | 0.031 |
| 6 | 70.00 | 5.3 | -8.1 | 16.5 | 0.552 | 0.913 | 0.054 | 0.054 | 0.030 | 0.030 |
| 7 | 85.00 | 6.1 | -8.8 | 15.2 | 0.549 | 0.938 | 0.040 | 0.040 | 0.021 | 0.021 |
| 8 | 90.00 | 6.4 | -8.8 | 12.9 | 0.553 | 0.918 | 0.054 | 0.054 | 0.028 | 0.028 |
| 9 | 95.00 | 6.9 | -8.5 | 9.5 | 0.605 | 0.847 | 0.105 | 0.105 | 0.054 | 0.054 |

TABLE IX. - Concluded.

(f) Reading number 1841

| RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|--------|--------|-----------|------|-----------|------|------------|-------|-------------|-------|
| IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 24.648 | 24.638 | 0.0 | 32.5 | 61.5 | 53.6 | 288.5 | 1.063 | 10.12 | 1.178 |
| 23.868 | 23.876 | 0.0 | 28.3 | 60.3 | 51.0 | 288.4 | 1.058 | 10.13 | 1.184 |
| 23.086 | 23.114 | 0.0 | 28.0 | 59.3 | 49.2 | 288.3 | 1.056 | 10.14 | 1.181 |
| 20.731 | 20.828 | 0.0 | 30.4 | 56.6 | 45.1 | 288.1 | 1.051 | 10.13 | 1.165 |
| 17.607 | 17.780 | 0.0 | 33.1 | 52.7 | 39.2 | 288.0 | 1.043 | 10.13 | 1.141 |
| 14.531 | 14.732 | 0.0 | 34.7 | 47.9 | 28.2 | 288.0 | 1.038 | 10.13 | 1.131 |
| 12.294 | 12.446 | 0.0 | 35.5 | 43.3 | 19.3 | 288.0 | 1.032 | 10.13 | 1.112 |
| 11.565 | 11.684 | 0.0 | 36.6 | 41.7 | 15.5 | 288.0 | 1.031 | 10.13 | 1.106 |
| 10.843 | 10.922 | 0.0 | 40.1 | 40.3 | 10.5 | 288.1 | 1.031 | 10.11 | 1.097 |

| ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-------|
| IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 128.8 | 140.8 | 269.5 | 200.1 | 128.8 | 118.8 | 0.0 | 75.7 | 236.8 | 236.7 |
| 130.5 | 147.0 | 263.8 | 205.6 | 130.5 | 129.5 | 0.0 | 69.6 | 229.2 | 229.3 |
| 131.4 | 148.6 | 257.5 | 200.8 | 131.4 | 131.2 | 0.0 | 69.8 | 221.5 | 221.8 |
| 131.4 | 145.8 | 238.5 | 178.1 | 131.4 | 125.7 | 0.0 | 73.8 | 199.0 | 199.9 |
| 128.8 | 138.8 | 212.6 | 150.1 | 128.8 | 116.3 | 0.0 | 75.9 | 169.2 | 170.9 |
| 126.4 | 140.4 | 188.4 | 131.0 | 126.4 | 115.5 | 0.0 | 79.9 | 139.8 | 141.7 |
| 124.8 | 137.6 | 171.6 | 118.7 | 124.8 | 112.0 | 0.0 | 80.0 | 117.8 | 119.2 |
| 124.5 | 137.0 | 166.8 | 114.2 | 124.5 | 110.1 | 0.0 | 81.6 | 111.0 | 112.2 |
| 122.8 | 133.5 | 161.0 | 103.8 | 122.8 | 102.1 | 0.0 | 86.0 | 104.1 | 104.9 |

| ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 0.384 | 0.408 | 0.803 | 0.579 | 0.384 | 0.344 | 0.922 | 1.210 |
| 0.389 | 0.427 | 0.786 | 0.598 | 0.389 | 0.376 | 0.992 | 1.171 |
| 0.392 | 0.433 | 0.768 | 0.585 | 0.392 | 0.382 | 0.999 | 1.136 |
| 0.392 | 0.425 | 0.712 | 0.520 | 0.392 | 0.367 | 0.956 | 1.015 |
| 0.384 | 0.406 | 0.634 | 0.439 | 0.384 | 0.340 | 0.903 | 0.797 |
| 0.377 | 0.412 | 0.562 | 0.384 | 0.377 | 0.339 | 0.914 | 0.562 |
| 0.372 | 0.405 | 0.511 | 0.349 | 0.372 | 0.329 | 0.897 | 0.511 |
| 0.371 | 0.403 | 0.497 | 0.336 | 0.371 | 0.324 | 0.884 | 0.497 |
| 0.366 | 0.392 | 0.480 | 0.305 | 0.366 | 0.300 | 0.831 | 0.480 |

| PERCENT | | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|---------|------|-----------|------|-------|--------|-----|------------|-------|------------|-------|
| SPAN | MEAN | SS | | | | | TOT | PROF | TOT | PROF |
| 5.00 | 3.0 | -1.6 | 8.4 | 0.472 | 0.759 | | 0.142 | 0.142 | 0.064 | 0.064 |
| 10.00 | 2.9 | -2.0 | 7.2 | 0.420 | 0.850 | | 0.085 | 0.085 | 0.041 | 0.041 |
| 15.00 | 2.9 | -2.3 | 7.2 | 0.422 | 0.871 | | 0.074 | 0.074 | 0.036 | 0.036 |
| 30.00 | 3.6 | -3.4 | 9.8 | 0.476 | 0.878 | | 0.071 | 0.071 | 0.036 | 0.036 |
| 50.00 | 5.2 | -5.1 | 15.1 | 0.534 | 0.900 | | 0.060 | 0.060 | 0.031 | 0.031 |
| 70.00 | 6.5 | -6.9 | 16.6 | 0.567 | 0.952 | | 0.032 | 0.032 | 0.017 | 0.017 |
| 85.00 | 7.2 | -7.7 | 15.8 | 0.574 | 0.969 | | 0.020 | 0.020 | 0.011 | 0.011 |
| 90.00 | 7.5 | -7.7 | 13.5 | 0.584 | 0.958 | | 0.028 | 0.028 | 0.015 | 0.015 |
| 95.00 | 8.1 | -7.3 | 9.3 | 0.638 | 0.881 | | 0.085 | 0.085 | 0.044 | 0.044 |

TABLE X. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 51

WITH STAGE 51B A-51 AT 100 PERCENT DESIGN SPEED

(a) Reading number 1766

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 17.1 | 1.3 | 17.1 | 1.3 | 301.7 | 0.997 | 11.31 | 0.979 |
| 2 | 23.861 | 23.806 | 14.9 | 1.1 | 14.9 | 1.1 | 300.9 | 0.998 | 11.55 | 0.978 |
| 3 | 23.127 | 23.167 | 15.4 | 0.7 | 15.4 | 0.7 | 300.4 | 0.997 | 11.55 | 0.993 |
| 4 | 20.917 | 20.996 | 17.5 | 0.2 | 17.5 | 0.2 | 299.8 | 0.995 | 11.53 | 0.993 |
| 5 | 17.955 | 18.080 | 20.8 | 0.8 | 20.8 | 0.8 | 299.2 | 0.996 | 11.50 | 0.996 |
| 6 | 14.945 | 15.110 | 23.9 | 1.7 | 23.9 | 1.7 | 298.5 | 0.997 | 11.43 | 0.997 |
| 7 | 12.647 | 12.786 | 24.9 | 2.5 | 24.9 | 2.5 | 296.4 | 0.999 | 11.11 | 0.996 |
| 8 | 11.869 | 11.966 | 24.9 | 3.1 | 24.9 | 3.1 | 295.6 | 1.001 | 10.95 | 0.989 |
| 9 | 11.087 | 11.125 | 26.5 | 4.2 | 26.5 | 4.2 | 295.4 | 1.001 | 10.80 | 0.974 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 185.4 | 165.9 | 185.4 | 165.9 | 177.2 | 165.8 | 54.7 | 3.6 | 0. | 0. |
| 2 | 196.2 | 174.1 | 196.2 | 174.1 | 189.6 | 174.0 | 50.6 | 3.4 | 0. | 0. |
| 3 | 197.0 | 176.8 | 197.0 | 176.8 | 189.9 | 176.8 | 52.3 | 2.1 | 0. | 0. |
| 4 | 197.8 | 180.0 | 197.8 | 180.0 | 189.6 | 180.0 | 59.4 | 0.7 | 0. | 0. |
| 5 | 196.5 | 181.8 | 196.5 | 181.8 | 183.7 | 181.8 | 69.8 | 2.7 | 0. | 0. |
| 6 | 194.6 | 182.0 | 194.6 | 182.0 | 177.9 | 181.9 | 78.9 | 5.6 | 0. | 0. |
| 7 | 185.2 | 170.7 | 185.2 | 170.7 | 168.0 | 170.5 | 78.0 | 7.4 | 0. | 0. |
| 8 | 179.8 | 161.0 | 179.8 | 161.0 | 163.0 | 160.8 | 75.8 | 8.6 | 0. | 0. |
| 9 | 174.2 | 145.7 | 174.2 | 145.7 | 155.9 | 145.3 | 77.7 | 10.8 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS VEL R MACH NO | |
|----|-------------|-------|-------------|-------|---------------|-------|--------------------------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | | |
| 1 | 0.548 | 0.489 | 0.548 | 0.488 | 0.524 | 0.488 | 0.936 | 0.548 |
| 2 | 0.583 | 0.514 | 0.583 | 0.514 | 0.563 | 0.514 | 0.918 | 0.503 |
| 3 | 0.586 | 0.523 | 0.586 | 0.523 | 0.565 | 0.523 | 0.931 | 0.503 |
| 4 | 0.589 | 0.534 | 0.589 | 0.534 | 0.562 | 0.534 | 0.954 | 0.509 |
| 5 | 0.586 | 0.541 | 0.586 | 0.541 | 0.548 | 0.541 | 0.989 | 0.506 |
| 6 | 0.581 | 0.542 | 0.581 | 0.542 | 0.531 | 0.541 | 1.022 | 0.531 |
| 7 | 0.553 | 0.507 | 0.553 | 0.507 | 0.502 | 0.507 | 1.015 | 0.553 |
| 8 | 0.536 | 0.478 | 0.536 | 0.478 | 0.486 | 0.477 | 0.986 | 0.536 |
| 9 | 0.519 | 0.430 | 0.519 | 0.430 | 0.464 | 0.429 | 0.932 | 0.519 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 2.8 | -6.4 | 5.3 | 0.240 | 0. | 0.112 | 0.112 | 0.055 | 0.055 |
| 2 | 10.00 | 0.5 | -8.7 | 5.1 | 0.227 | 0. | 0.105 | 0.105 | 0.050 | 0.050 |
| 3 | 15.00 | 0.8 | -8.4 | 4.7 | 0.220 | 0. | 0.060 | 0.060 | 0.028 | 0.028 |
| 4 | 30.00 | 2.0 | -7.2 | 4.2 | 0.213 | 0. | 0.034 | 0.034 | 0.014 | 0.014 |
| 5 | 50.00 | 3.4 | -5.8 | 5.0 | 0.197 | 0. | 0.021 | 0.021 | 0.008 | 0.008 |
| 6 | 70.00 | 4.1 | -5.1 | 6.0 | 0.177 | 0. | 0.016 | 0.016 | 0.005 | 0.005 |
| 7 | 85.00 | 3.3 | -5.8 | 6.7 | 0.174 | 0. | 0.021 | 0.021 | 0.005 | 0.005 |
| 8 | 90.00 | 3.0 | -6.1 | 7.2 | 0.193 | 0. | 0.061 | 0.061 | 0.014 | 0.014 |
| 9 | 95.00 | 4.3 | -4.8 | 8.2 | 0.248 | 0. | 0.155 | 0.155 | 0.034 | 0.034 |

TABLE X. - Continued.

(b) Reading number 1767

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 19.7 | 1.6 | 19.7 | 1.6 | 303.9 | 0.995 | 11.58 | 0.982 |
| 2 | 23.861 | 23.886 | 17.6 | 1.5 | 17.6 | 1.5 | 302.8 | 0.997 | 11.82 | 0.977 |
| 3 | 23.127 | 23.167 | 17.8 | 1.1 | 17.8 | 1.1 | 302.2 | 0.997 | 11.82 | 0.986 |
| 4 | 20.917 | 20.996 | 20.1 | 0.8 | 20.1 | 0.8 | 301.2 | 0.996 | 11.78 | 0.991 |
| 5 | 17.955 | 18.080 | 23.2 | 1.1 | 23.2 | 1.1 | 300.1 | 0.996 | 11.65 | 0.996 |
| 6 | 14.945 | 15.110 | 25.9 | 1.9 | 25.9 | 1.9 | 298.9 | 0.997 | 11.47 | 0.998 |
| 7 | 12.647 | 12.786 | 26.6 | 2.2 | 26.6 | 2.2 | 296.5 | 1.000 | 11.10 | 0.999 |
| 8 | 11.869 | 11.966 | 26.4 | 3.0 | 26.4 | 3.0 | 295.9 | 1.001 | 11.01 | 0.989 |
| 9 | 11.087 | 11.125 | 29.1 | 4.5 | 29.1 | 4.5 | 296.1 | 1.000 | 10.88 | 0.976 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 179.8 | 161.7 | 179.8 | 161.7 | 169.2 | 161.6 | 60.7 | 4.6 | 0. | 0. |
| 2 | 190.6 | 168.4 | 190.6 | 168.4 | 181.7 | 168.4 | 57.5 | 4.4 | 0. | 0. |
| 3 | 191.7 | 171.2 | 191.7 | 171.2 | 182.5 | 171.2 | 58.5 | 3.2 | 0. | 0. |
| 4 | 192.7 | 173.8 | 192.7 | 173.8 | 181.0 | 173.8 | 66.2 | 2.3 | 0. | 0. |
| 5 | 189.8 | 173.2 | 189.8 | 173.2 | 174.4 | 173.2 | 74.9 | 3.4 | 0. | 0. |
| 6 | 185.3 | 169.2 | 185.3 | 169.2 | 166.7 | 169.1 | 81.0 | 5.7 | 0. | 0. |
| 7 | 173.4 | 155.3 | 173.4 | 155.3 | 155.1 | 155.2 | 77.6 | 6.0 | 0. | 0. |
| 8 | 170.6 | 145.8 | 170.6 | 145.8 | 152.9 | 145.6 | 75.8 | 7.7 | 0. | 0. |
| 9 | 166.0 | 131.1 | 166.0 | 131.1 | 145.1 | 130.7 | 80.7 | 10.2 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.529 | 0.474 | 0.529 | 0.474 | 0.498 | 0.474 | 0.935 | 0.529 |
| 2 | 0.563 | 0.495 | 0.563 | 0.495 | 0.537 | 0.495 | 0.927 | 0.563 |
| 3 | 0.568 | 0.504 | 0.568 | 0.504 | 0.540 | 0.504 | 0.938 | 0.563 |
| 4 | 0.572 | 0.514 | 0.572 | 0.514 | 0.537 | 0.514 | 0.960 | 0.572 |
| 5 | 0.564 | 0.513 | 0.564 | 0.513 | 0.518 | 0.513 | 0.993 | 0.564 |
| 6 | 0.551 | 0.501 | 0.551 | 0.501 | 0.495 | 0.501 | 1.015 | 0.551 |
| 7 | 0.516 | 0.459 | 0.516 | 0.459 | 0.461 | 0.459 | 1.001 | 0.516 |
| 8 | 0.507 | 0.430 | 0.507 | 0.430 | 0.455 | 0.430 | 0.952 | 0.507 |
| 9 | 0.493 | 0.386 | 0.493 | 0.386 | 0.431 | 0.385 | 0.901 | 0.493 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 5.4 | -3.8 | 5.7 | 0.253 | 0. | 0.106 | 0.106 | 0.052 | 0.052 |
| 2 | 10.00 | 3.1 | -6.1 | 5.5 | 0.248 | 0. | 0.117 | 0.117 | 0.055 | 0.055 |
| 3 | 15.00 | 3.2 | -6.1 | 5.1 | 0.239 | 0. | 0.072 | 0.072 | 0.033 | 0.033 |
| 4 | 30.00 | 4.6 | -4.6 | 4.8 | 0.236 | 0. | 0.043 | 0.043 | 0.018 | 0.018 |
| 5 | 50.00 | 5.8 | -3.3 | 5.2 | 0.222 | 0. | 0.020 | 0.020 | 0.007 | 0.007 |
| 6 | 70.00 | 6.1 | -3.1 | 6.2 | 0.207 | 0. | 0.010 | 0.010 | 0.003 | 0.003 |
| 7 | 85.00 | 5.0 | -4.1 | 6.4 | 0.208 | 0. | 0.003 | 0.003 | 0.001 | 0.001 |
| 8 | 90.00 | 4.4 | -4.7 | 7.1 | 0.240 | 0. | 0.067 | 0.067 | 0.016 | 0.016 |
| 9 | 95.00 | 6.9 | -2.2 | 8.5 | 0.304 | 0. | 0.157 | 0.157 | 0.034 | 0.034 |

TABLE X. - Continued.

(c) Reading number 1768

| RP | RADI I | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 20.7 | 2.0 | 20.7 | 2.0 | 303.6 | 0.997 | 11.69 | 0.977 |
| 2 | 23.861 | 23.886 | 18.8 | 2.1 | 18.8 | 2.1 | 302.8 | 0.998 | 11.83 | 0.979 |
| 3 | 23.127 | 23.167 | 18.8 | 1.6 | 18.8 | 1.6 | 301.9 | 0.998 | 11.78 | 0.986 |
| 4 | 20.917 | 20.996 | 20.7 | 0.6 | 20.7 | 0.6 | 300.7 | 0.996 | 11.63 | 0.993 |
| 5 | 17.955 | 18.080 | 23.9 | 0.9 | 23.9 | 0.9 | 299.0 | 0.998 | 11.42 | 0.999 |
| 6 | 14.945 | 15.110 | 26.8 | 1.6 | 26.8 | 1.6 | 298.2 | 0.998 | 11.31 | 1.002 |
| 7 | 12.647 | 12.786 | 28.8 | 2.3 | 28.8 | 2.3 | 297.1 | 0.998 | 11.22 | 0.992 |
| 8 | 11.869 | 11.966 | 29.3 | 3.7 | 29.3 | 3.7 | 296.7 | 0.999 | 11.18 | 0.978 |
| 9 | 11.087 | 11.125 | 31.9 | 5.3 | 31.9 | 5.3 | 296.6 | 1.000 | 11.03 | 0.973 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 175.5 | 153.7 | 175.5 | 153.7 | 164.1 | 153.6 | 62.1 | 5.3 | 0. | 0. |
| 2 | 182.3 | 159.7 | 182.3 | 159.7 | 172.5 | 159.6 | 58.9 | 5.7 | 0. | 0. |
| 3 | 181.6 | 160.6 | 181.6 | 160.6 | 171.9 | 160.5 | 58.6 | 4.5 | 0. | 0. |
| 4 | 178.2 | 159.0 | 178.2 | 159.0 | 166.7 | 159.0 | 63.0 | 1.7 | 0. | 0. |
| 5 | 169.9 | 154.6 | 169.9 | 154.6 | 155.3 | 154.5 | 68.9 | 2.6 | 0. | 0. |
| 6 | 166.3 | 151.9 | 166.3 | 151.9 | 148.4 | 151.9 | 75.1 | 4.4 | 0. | 0. |
| 7 | 165.3 | 143.3 | 165.3 | 143.3 | 144.9 | 143.1 | 79.6 | 5.8 | 0. | 0. |
| 8 | 165.0 | 133.6 | 165.0 | 133.6 | 143.9 | 133.3 | 80.7 | 8.7 | 0. | 0. |
| 9 | 159.7 | 121.2 | 159.7 | 121.2 | 135.5 | 120.7 | 84.5 | 11.2 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.516 | 0.449 | 0.516 | 0.449 | 0.482 | 0.449 | 0.936 | 0.516 |
| 2 | 0.538 | 0.468 | 0.538 | 0.468 | 0.509 | 0.468 | 0.925 | 0.533 |
| 3 | 0.536 | 0.472 | 0.536 | 0.472 | 0.508 | 0.471 | 0.934 | 0.536 |
| 4 | 0.527 | 0.468 | 0.527 | 0.468 | 0.493 | 0.468 | 0.954 | 0.527 |
| 5 | 0.502 | 0.456 | 0.502 | 0.456 | 0.459 | 0.455 | 0.995 | 0.502 |
| 6 | 0.492 | 0.448 | 0.492 | 0.448 | 0.439 | 0.448 | 1.023 | 0.492 |
| 7 | 0.490 | 0.422 | 0.490 | 0.422 | 0.429 | 0.422 | 0.988 | 0.490 |
| 8 | 0.489 | 0.393 | 0.489 | 0.393 | 0.427 | 0.392 | 0.926 | 0.489 |
| 9 | 0.473 | 0.355 | 0.473 | 0.355 | 0.401 | 0.354 | 0.890 | 0.473 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 6.4 | -2.8 | 6.1 | 0.282 | 0. | 0.137 | 0.137 | 0.067 | 0.067 |
| 2 | 10.00 | 4.4 | -4.8 | 6.1 | 0.262 | 0. | 0.116 | 0.116 | 0.055 | 0.055 |
| 3 | 15.00 | 4.2 | -5.0 | 5.6 | 0.253 | 0. | 0.077 | 0.077 | 0.035 | 0.035 |
| 4 | 30.00 | 5.2 | -4.0 | 4.6 | 0.250 | 0. | 0.039 | 0.039 | 0.016 | 0.016 |
| 5 | 50.00 | 6.5 | -2.7 | 5.1 | 0.230 | 0. | 0.003 | 0.003 | 0.001 | 0.001 |
| 6 | 70.00 | 7.0 | -2.2 | 5.9 | 0.213 | 0. | -0.012 | -0.012 | -0.004 | -0.004 |
| 7 | 85.00 | 7.2 | -1.9 | 6.5 | 0.246 | 0. | 0.055 | 0.055 | 0.014 | 0.014 |
| 8 | 90.00 | 7.3 | -1.8 | 7.8 | 0.293 | 0. | 0.143 | 0.143 | 0.034 | 0.034 |
| 9 | 95.00 | 9.7 | 0.6 | 9.3 | 0.342 | 0. | 0.190 | 0.190 | 0.042 | 0.042 |

TABLE X. - Continued.

(d) Reading number 1769

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 25.8 | 3.5 | 25.8 | 3.5 | 305.9 | 0.998 | 11.92 | 0.975 |
| 2 | 23.861 | 23.886 | 23.4 | 3.4 | 23.4 | 3.4 | 304.8 | 0.999 | 12.04 | 0.975 |
| 3 | 23.127 | 23.167 | 24.0 | 2.7 | 24.0 | 2.7 | 304.0 | 0.999 | 11.99 | 0.982 |
| 4 | 20.917 | 20.996 | 25.8 | 1.4 | 25.8 | 1.4 | 302.3 | 0.996 | 11.80 | 0.994 |
| 5 | 17.955 | 18.080 | 28.6 | 1.4 | 28.6 | 1.4 | 300.2 | 0.998 | 11.52 | 1.000 |
| 6 | 14.945 | 15.110 | 30.9 | 2.0 | 30.9 | 2.0 | 298.9 | 0.998 | 11.43 | 0.995 |
| 7 | 12.647 | 12.786 | 32.6 | 3.2 | 32.6 | 3.2 | 297.6 | 0.998 | 11.29 | 0.987 |
| 8 | 11.869 | 11.966 | 33.4 | 4.6 | 33.4 | 4.6 | 297.2 | 0.999 | 11.25 | 0.976 |
| 9 | 11.087 | 11.125 | 36.6 | 5.8 | 36.6 | 5.8 | 297.2 | 1.000 | 11.11 | 0.977 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|-----|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 164.3 | 142.3 | 164.3 | 142.3 | 147.9 | 142.0 | 71.6 | 8.7 | 0. | 0. |
| 2 | 170.8 | 146.6 | 170.8 | 146.6 | 156.7 | 146.4 | 67.8 | 8.7 | 0. | 0. |
| 3 | 170.3 | 147.4 | 170.3 | 147.4 | 155.5 | 147.3 | 69.3 | 7.0 | 0. | 0. |
| 4 | 165.8 | 145.9 | 165.8 | 145.9 | 149.3 | 145.9 | 72.3 | 3.5 | 0. | 0. |
| 5 | 156.4 | 137.9 | 156.4 | 137.9 | 137.3 | 137.9 | 74.8 | 3.3 | 0. | 0. |
| 6 | 154.1 | 131.4 | 154.1 | 131.4 | 132.2 | 131.3 | 79.2 | 4.6 | 0. | 0. |
| 7 | 151.6 | 119.2 | 151.6 | 119.2 | 127.8 | 119.0 | 81.6 | 6.7 | 0. | 0. |
| 8 | 151.4 | 107.9 | 151.4 | 107.9 | 126.4 | 107.5 | 83.4 | 8.7 | 0. | 0. |
| 9 | 146.1 | 97.3 | 146.1 | 97.3 | 117.3 | 96.8 | 87.0 | 9.8 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.479 | 0.413 | 0.479 | 0.413 | 0.431 | 0.412 | 0.950 | 0.479 |
| 2 | 0.500 | 0.427 | 0.500 | 0.427 | 0.459 | 0.426 | 0.934 | 0.500 |
| 3 | 0.499 | 0.430 | 0.499 | 0.430 | 0.456 | 0.429 | 0.947 | 0.499 |
| 4 | 0.487 | 0.427 | 0.487 | 0.427 | 0.438 | 0.427 | 0.977 | 0.487 |
| 5 | 0.460 | 0.404 | 0.460 | 0.404 | 0.404 | 0.404 | 1.004 | 0.460 |
| 6 | 0.454 | 0.385 | 0.454 | 0.385 | 0.389 | 0.385 | 0.993 | 0.454 |
| 7 | 0.447 | 0.349 | 0.447 | 0.349 | 0.377 | 0.349 | 0.931 | 0.447 |
| 8 | 0.447 | 0.316 | 0.447 | 0.316 | 0.373 | 0.314 | 0.851 | 0.447 |
| 9 | 0.430 | 0.284 | 0.430 | 0.284 | 0.346 | 0.282 | 0.825 | 0.498 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 11.5 | 2.3 | 7.6 | 0.321 | 0. | 0.174 | 0.174 | 0.065 | 0.065 |
| 2 | 10.00 | 9.0 | -0.2 | 7.4 | 0.305 | 0. | 0.161 | 0.161 | 0.076 | 0.076 |
| 3 | 15.00 | 9.4 | 0.2 | 6.7 | 0.302 | 0. | 0.112 | 0.112 | 0.051 | 0.051 |
| 4 | 30.00 | 10.3 | 1.1 | 5.4 | 0.292 | 0. | 0.040 | 0.040 | 0.017 | 0.017 |
| 5 | 50.00 | 11.2 | 2.0 | 5.5 | 0.281 | 0. | -0.003 | -0.003 | -0.001 | -0.001 |
| 6 | 70.00 | 11.1 | 2.0 | 6.2 | 0.291 | 0. | 0.035 | 0.035 | 0.010 | 0.010 |
| 7 | 85.00 | 11.0 | 1.9 | 7.4 | 0.338 | 0. | 0.102 | 0.102 | 0.026 | 0.026 |
| 8 | 90.00 | 11.5 | 2.4 | 8.7 | 0.404 | 0. | 0.184 | 0.184 | 0.043 | 0.043 |
| 9 | 95.00 | 14.4 | 5.2 | 9.8 | 0.450 | 0. | 0.197 | 0.197 | 0.043 | 0.043 |

TABLE X. - Concluded.

(e) Reading number 1771

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 28.6 | 4.5 | 28.6 | 4.5 | 306.7 | 1.000 | 11.94 | 0.976 |
| 2 | 23.861 | 23.866 | 25.0 | 4.0 | 25.0 | 4.0 | 305.4 | 1.001 | 12.08 | 0.973 |
| 3 | 23.127 | 23.167 | 25.1 | 3.1 | 25.1 | 3.1 | 304.6 | 0.999 | 12.03 | 0.979 |
| 4 | 20.917 | 20.996 | 27.8 | 1.6 | 27.8 | 1.6 | 302.6 | 0.997 | 11.81 | 0.995 |
| 5 | 17.955 | 18.080 | 30.8 | 1.5 | 30.8 | 1.5 | 300.5 | 0.998 | 11.58 | 0.998 |
| 6 | 14.945 | 15.110 | 32.8 | 2.3 | 32.8 | 2.3 | 299.1 | 0.998 | 11.47 | 0.993 |
| 7 | 12.647 | 12.786 | 33.8 | 3.5 | 33.8 | 3.5 | 297.7 | 0.998 | 11.31 | 0.985 |
| 8 | 11.869 | 11.966 | 34.6 | 4.7 | 34.6 | 4.7 | 297.2 | 0.999 | 11.25 | 0.977 |
| 9 | 11.087 | 11.125 | 37.8 | 5.8 | 37.8 | 5.8 | 297.2 | 1.000 | 11.11 | 0.977 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 158.9 | 139.5 | 158.9 | 139.5 | 139.5 | 138.1 | 76.0 | 10.8 | 0. | 0. |
| 2 | 167.6 | 142.2 | 167.6 | 142.2 | 152.0 | 141.9 | 70.7 | 10.0 | 0. | 0. |
| 3 | 166.6 | 142.7 | 166.6 | 142.7 | 151.0 | 142.4 | 70.6 | 7.7 | 0. | 0. |
| 4 | 160.8 | 141.4 | 160.8 | 141.4 | 142.2 | 141.4 | 75.1 | 3.9 | 0. | 0. |
| 5 | 152.7 | 132.5 | 152.7 | 132.5 | 131.2 | 132.4 | 78.1 | 3.6 | 0. | 0. |
| 6 | 150.7 | 124.3 | 150.7 | 124.3 | 126.7 | 124.2 | 81.7 | 4.9 | 0. | 0. |
| 7 | 147.8 | 110.8 | 147.8 | 110.8 | 122.8 | 110.6 | 82.2 | 6.7 | 0. | 0. |
| 8 | 147.6 | 101.9 | 147.6 | 101.9 | 121.5 | 101.5 | 85.9 | 8.4 | 0. | 0. |
| 9 | 143.1 | 92.3 | 143.1 | 92.3 | 113.1 | 91.8 | 87.6 | 9.3 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.462 | 0.401 | 0.462 | 0.401 | 0.406 | 0.400 | 0.939 | 0.538 |
| 2 | 0.490 | 0.413 | 0.490 | 0.413 | 0.444 | 0.412 | 0.934 | 0.490 |
| 3 | 0.488 | 0.415 | 0.488 | 0.415 | 0.442 | 0.414 | 0.944 | 0.408 |
| 4 | 0.471 | 0.413 | 0.471 | 0.413 | 0.417 | 0.413 | 0.994 | 0.409 |
| 5 | 0.448 | 0.387 | 0.448 | 0.387 | 0.385 | 0.387 | 1.009 | 0.506 |
| 6 | 0.443 | 0.364 | 0.443 | 0.364 | 0.372 | 0.363 | 0.980 | 0.493 |
| 7 | 0.435 | 0.324 | 0.435 | 0.324 | 0.362 | 0.323 | 0.901 | 0.469 |
| 8 | 0.435 | 0.298 | 0.435 | 0.298 | 0.358 | 0.297 | 0.836 | 0.475 |
| 9 | 0.421 | 0.269 | 0.421 | 0.269 | 0.333 | 0.268 | 0.812 | 0.508 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-----|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 14.3 | 5.1 | 8.5 | 0.329 | 0. | 0.173 | 0.173 | 0.084 | 0.084 |
| 2 | 10.00 | 10.5 | 1.3 | 8.1 | 0.323 | 0. | 0.179 | 0.179 | 0.085 | 0.085 |
| 3 | 15.00 | 10.4 | 1.2 | 7.1 | 0.317 | 0. | 0.137 | 0.137 | 0.063 | 0.063 |
| 4 | 30.00 | 12.3 | 3.1 | 5.6 | 0.304 | 0. | 0.034 | 0.034 | 0.014 | 0.014 |
| 5 | 50.00 | 13.4 | 4.2 | 5.7 | 0.306 | 0. | 0.017 | 0.017 | 0.006 | 0.006 |
| 6 | 70.00 | 13.0 | 3.8 | 6.5 | 0.326 | 0. | 0.059 | 0.059 | 0.017 | 0.017 |
| 7 | 85.00 | 12.2 | 3.1 | 7.7 | 0.378 | 0. | 0.121 | 0.121 | 0.031 | 0.031 |
| 8 | 90.00 | 12.7 | 3.6 | 8.8 | 0.430 | 0. | 0.186 | 0.186 | 0.044 | 0.044 |
| 9 | 95.00 | 15.6 | 6.4 | 9.8 | 0.475 | 0. | 0.196 | 0.196 | 0.043 | 0.043 |

TABLE XI. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 51

WITH STAGE 51B B-51 AT 100 PERCENT DESIGN SPEED

(a) Reading number 1796

| RP | RADIO | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 14.2 | 1.0 | 14.2 | 1.0 | 301.3 | 0.995 | 11.23 | 0.967 |
| 2 | 23.861 | 23.886 | 12.9 | 0.8 | 12.9 | 0.8 | 301.0 | 0.996 | 11.47 | 0.973 |
| 3 | 23.127 | 23.167 | 13.5 | 0.5 | 13.5 | 0.5 | 300.2 | 0.997 | 11.45 | 0.983 |
| 4 | 20.917 | 20.996 | 15.5 | 0.2 | 15.5 | 0.2 | 299.2 | 0.995 | 11.38 | 0.987 |
| 5 | 17.955 | 18.080 | 18.8 | 0.6 | 18.8 | 0.6 | 298.2 | 0.998 | 11.23 | 1.002 |
| 6 | 14.945 | 15.110 | 22.6 | 1.3 | 22.6 | 1.3 | 298.1 | 0.997 | 11.35 | 0.990 |
| 7 | 12.647 | 12.786 | 23.9 | 2.3 | 23.9 | 2.3 | 297.0 | 0.997 | 11.15 | 0.990 |
| 8 | 11.869 | 11.966 | 23.8 | 3.4 | 23.8 | 3.4 | 296.1 | 0.999 | 10.98 | 0.987 |
| 9 | 11.087 | 11.125 | 25.8 | 5.3 | 25.8 | 5.3 | 295.8 | 0.999 | 10.77 | 0.967 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 206.0 | 179.2 | 206.0 | 179.2 | 199.7 | 179.2 | 50.5 | 3.0 | 0. | 0. |
| 2 | 216.3 | 189.3 | 216.3 | 189.3 | 210.9 | 189.2 | 48.3 | 2.7 | 0. | 0. |
| 3 | 216.1 | 191.4 | 216.1 | 191.4 | 210.1 | 191.4 | 50.5 | 1.6 | 0. | 0. |
| 4 | 215.1 | 192.4 | 215.1 | 192.4 | 207.3 | 192.4 | 57.4 | 0.5 | 0. | 0. |
| 5 | 206.9 | 194.2 | 206.9 | 194.2 | 195.9 | 194.2 | 66.6 | 2.0 | 0. | 0. |
| 6 | 208.5 | 195.7 | 208.5 | 195.7 | 192.5 | 195.6 | 80.0 | 4.3 | 0. | 0. |
| 7 | 202.9 | 191.5 | 202.9 | 191.5 | 185.5 | 191.4 | 82.2 | 7.6 | 0. | 0. |
| 8 | 197.4 | 183.8 | 197.4 | 183.8 | 180.6 | 183.5 | 79.6 | 10.9 | 0. | 0. |
| 9 | 191.1 | 166.1 | 191.1 | 166.1 | 172.0 | 165.4 | 83.2 | 15.3 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.614 | 0.530 | 0.614 | 0.530 | 0.595 | 0.530 | 0.897 | 0.614 |
| 2 | 0.648 | 0.562 | 0.648 | 0.562 | 0.631 | 0.562 | 0.897 | 0.648 |
| 3 | 0.648 | 0.570 | 0.648 | 0.570 | 0.630 | 0.570 | 0.911 | 0.648 |
| 4 | 0.646 | 0.574 | 0.646 | 0.574 | 0.622 | 0.574 | 0.928 | 0.646 |
| 5 | 0.620 | 0.580 | 0.620 | 0.580 | 0.587 | 0.580 | 0.991 | 0.620 |
| 6 | 0.625 | 0.585 | 0.625 | 0.585 | 0.578 | 0.585 | 1.016 | 0.625 |
| 7 | 0.609 | 0.573 | 0.609 | 0.573 | 0.557 | 0.573 | 1.032 | 0.609 |
| 8 | 0.592 | 0.549 | 0.592 | 0.549 | 0.542 | 0.548 | 1.016 | 0.592 |
| 9 | 0.572 | 0.494 | 0.572 | 0.494 | 0.515 | 0.492 | 0.962 | 0.572 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | -0.1 | -9.3 | 5.0 | 0.243 | 0. | 0.145 | 0.145 | 0.071 | 0.071 |
| 2 | 10.00 | -1.5 | -10.7 | 4.8 | 0.225 | 0. | 0.110 | 0.110 | 0.052 | 0.052 |
| 3 | 15.00 | -1.1 | -10.3 | 4.5 | 0.218 | 0. | 0.068 | 0.068 | 0.031 | 0.031 |
| 4 | 30.00 | -0.0 | -9.2 | 4.2 | 0.215 | 0. | 0.052 | 0.052 | 0.022 | 0.022 |
| 5 | 50.00 | 1.4 | -7.8 | 4.7 | 0.173 | 0. | -0.010 | -0.010 | -0.003 | -0.003 |
| 6 | 70.00 | 2.7 | -6.4 | 5.5 | 0.169 | 0. | 0.042 | 0.042 | 0.013 | 0.013 |
| 7 | 85.00 | 2.3 | -6.8 | 6.5 | 0.148 | 0. | 0.045 | 0.045 | 0.011 | 0.011 |
| 8 | 90.00 | 1.8 | -7.3 | 7.5 | 0.150 | 0. | 0.063 | 0.063 | 0.015 | 0.015 |
| 9 | 95.00 | 3.6 | -5.5 | 9.3 | 0.209 | 0. | 0.164 | 0.164 | 0.036 | 0.036 |

TABLE XI. - Continued.

(b) Reading number 1797

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 19.4 | 1.6 | 19.4 | 1.6 | 304.5 | 0.995 | 11.66 | 0.972 |
| 2 | 23.861 | 23.886 | 17.2 | 1.5 | 17.2 | 1.5 | 303.5 | 0.995 | 11.88 | 0.973 |
| 3 | 23.127 | 23.167 | 17.5 | 1.1 | 17.5 | 1.1 | 303.0 | 0.996 | 11.87 | 0.984 |
| 4 | 20.917 | 20.996 | 19.8 | 0.8 | 19.8 | 0.8 | 301.7 | 0.996 | 11.80 | 0.990 |
| 5 | 17.955 | 18.080 | 23.0 | 1.2 | 23.0 | 1.2 | 300.5 | 0.996 | 11.67 | 0.997 |
| 6 | 14.945 | 15.110 | 25.4 | 1.9 | 25.4 | 1.9 | 299.0 | 0.998 | 11.50 | 1.000 |
| 7 | 12.647 | 12.786 | 26.5 | 2.2 | 26.5 | 2.2 | 296.7 | 1.001 | 11.13 | 1.001 |
| 8 | 11.869 | 11.966 | 26.5 | 3.0 | 26.5 | 3.0 | 296.1 | 1.000 | 11.05 | 0.986 |
| 9 | 11.087 | 11.125 | 28.5 | 4.1 | 28.5 | 4.1 | 296.3 | 1.000 | 10.94 | 0.968 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 194.2 | 169.6 | 194.2 | 169.6 | 183.2 | 169.5 | 64.5 | 4.6 | 0. | 0. |
| 2 | 204.4 | 177.8 | 204.4 | 177.8 | 195.3 | 177.8 | 60.4 | 4.7 | 0. | 0. |
| 3 | 206.4 | 181.7 | 206.4 | 181.7 | 196.8 | 181.7 | 62.1 | 3.6 | 0. | 0. |
| 4 | 206.0 | 184.3 | 206.0 | 184.3 | 193.9 | 184.3 | 69.6 | 2.5 | 0. | 0. |
| 5 | 202.3 | 184.7 | 202.3 | 184.7 | 186.3 | 184.7 | 79.0 | 3.8 | 0. | 0. |
| 6 | 198.0 | 182.0 | 198.0 | 182.0 | 178.9 | 181.9 | 85.0 | 6.2 | 0. | 0. |
| 7 | 186.6 | 169.1 | 186.6 | 169.1 | 167.1 | 169.0 | 83.2 | 6.4 | 0. | 0. |
| 8 | 184.5 | 158.8 | 184.5 | 158.8 | 165.1 | 158.6 | 82.4 | 8.2 | 0. | 0. |
| 9 | 180.7 | 143.8 | 180.7 | 143.8 | 158.8 | 143.4 | 86.3 | 10.2 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.573 | 0.498 | 0.573 | 0.498 | 0.541 | 0.498 | 0.926 | 0.573 |
| 2 | 0.607 | 0.524 | 0.607 | 0.524 | 0.579 | 0.524 | 0.910 | 0.607 |
| 3 | 0.613 | 0.537 | 0.613 | 0.537 | 0.585 | 0.537 | 0.923 | 0.613 |
| 4 | 0.613 | 0.546 | 0.613 | 0.546 | 0.577 | 0.546 | 0.951 | 0.613 |
| 5 | 0.603 | 0.548 | 0.603 | 0.548 | 0.555 | 0.548 | 0.991 | 0.603 |
| 6 | 0.591 | 0.541 | 0.591 | 0.541 | 0.534 | 0.540 | 1.017 | 0.591 |
| 7 | 0.557 | 0.502 | 0.557 | 0.502 | 0.499 | 0.501 | 1.012 | 0.557 |
| 8 | 0.551 | 0.470 | 0.551 | 0.470 | 0.493 | 0.470 | 0.961 | 0.551 |
| 9 | 0.539 | 0.424 | 0.539 | 0.424 | 0.473 | 0.423 | 0.903 | 0.539 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 5.1 | -4.1 | 5.6 | 0.277 | 0. | 0.143 | 0.143 | 0.070 | 0.070 |
| 2 | 10.00 | 2.7 | -6.5 | 5.5 | 0.259 | 0. | 0.121 | 0.121 | 0.057 | 0.057 |
| 3 | 15.00 | 2.9 | -6.3 | 5.1 | 0.250 | 0. | 0.072 | 0.072 | 0.033 | 0.033 |
| 4 | 30.00 | 4.2 | -4.9 | 4.8 | 0.241 | 0. | 0.044 | 0.044 | 0.018 | 0.018 |
| 5 | 50.00 | 5.6 | -3.6 | 5.3 | 0.219 | 0. | 0.013 | 0.013 | 0.004 | 0.004 |
| 6 | 70.00 | 5.6 | -3.6 | 6.2 | 0.199 | 0. | -0.001 | -0.001 | -0.000 | -0.000 |
| 7 | 85.00 | 4.9 | -4.3 | 6.4 | 0.197 | 0. | -0.005 | -0.005 | -0.001 | -0.001 |
| 8 | 90.00 | 4.6 | -4.5 | 7.1 | 0.234 | 0. | 0.073 | 0.073 | 0.017 | 0.017 |
| 9 | 95.00 | 6.3 | -2.8 | 8.0 | 0.297 | 0. | 0.177 | 0.177 | 0.039 | 0.039 |

TABLE XI. - Continued.

(c) Reading number 1798

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 20.5 | 1.9 | 20.5 | 1.9 | 304.6 | 0.996 | 11.74 | 0.975 |
| 2 | 23.861 | 23.886 | 19.3 | 2.0 | 19.3 | 2.0 | 303.6 | 0.998 | 11.92 | 0.977 |
| 3 | 23.127 | 23.167 | 18.7 | 1.5 | 18.7 | 1.5 | 303.0 | 0.997 | 11.88 | 0.985 |
| 4 | 20.917 | 20.996 | 20.6 | 0.6 | 20.6 | 0.6 | 301.2 | 0.996 | 11.73 | 0.991 |
| 5 | 17.955 | 18.080 | 23.6 | 0.8 | 23.6 | 0.8 | 299.6 | 0.997 | 11.50 | 0.999 |
| 6 | 14.945 | 15.110 | 26.5 | 1.4 | 26.5 | 1.4 | 298.7 | 0.998 | 11.36 | 1.002 |
| 7 | 12.647 | 12.786 | 28.5 | 2.0 | 28.5 | 2.0 | 297.7 | 0.998 | 11.30 | 0.990 |
| 8 | 11.869 | 11.966 | 29.2 | 3.4 | 29.2 | 3.4 | 297.4 | 0.998 | 11.28 | 0.974 |
| 9 | 11.087 | 11.125 | 31.9 | 4.8 | 31.9 | 4.8 | 297.1 | 0.999 | 11.07 | 0.970 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 187.1 | 163.3 | 187.1 | 163.3 | 175.2 | 163.2 | 65.6 | 5.5 | 0. | 0. |
| 2 | 195.5 | 170.6 | 195.5 | 170.6 | 184.5 | 170.5 | 64.7 | 5.9 | 0. | 0. |
| 3 | 195.8 | 171.9 | 195.8 | 171.9 | 185.5 | 171.9 | 62.7 | 4.5 | 0. | 0. |
| 4 | 192.9 | 170.6 | 192.9 | 170.6 | 180.5 | 170.6 | 67.8 | 1.9 | 0. | 0. |
| 5 | 184.0 | 166.7 | 184.0 | 166.7 | 168.6 | 166.6 | 73.6 | 2.4 | 0. | 0. |
| 6 | 179.3 | 164.0 | 179.3 | 164.0 | 160.5 | 164.0 | 79.9 | 4.0 | 0. | 0. |
| 7 | 179.5 | 156.5 | 179.5 | 156.5 | 157.7 | 156.4 | 85.7 | 5.5 | 0. | 0. |
| 8 | 179.9 | 146.7 | 179.9 | 146.7 | 157.0 | 146.4 | 87.9 | 8.8 | 0. | 0. |
| 9 | 173.4 | 134.0 | 173.4 | 134.0 | 147.1 | 133.5 | 91.7 | 11.3 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.551 | 0.478 | 0.551 | 0.478 | 0.516 | 0.478 | 0.932 | 0.551 |
| 2 | 0.578 | 0.501 | 0.578 | 0.501 | 0.546 | 0.501 | 0.924 | 0.578 |
| 3 | 0.580 | 0.506 | 0.580 | 0.506 | 0.549 | 0.506 | 0.926 | 0.580 |
| 4 | 0.572 | 0.504 | 0.572 | 0.504 | 0.536 | 0.504 | 0.945 | 0.572 |
| 5 | 0.546 | 0.492 | 0.546 | 0.492 | 0.500 | 0.492 | 0.988 | 0.546 |
| 6 | 0.532 | 0.485 | 0.532 | 0.485 | 0.476 | 0.485 | 1.022 | 0.532 |
| 7 | 0.534 | 0.462 | 0.534 | 0.462 | 0.469 | 0.462 | 0.991 | 0.534 |
| 8 | 0.535 | 0.433 | 0.535 | 0.433 | 0.467 | 0.432 | 0.933 | 0.535 |
| 9 | 0.515 | 0.394 | 0.515 | 0.394 | 0.437 | 0.393 | 0.907 | 0.515 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 6.2 | -3.0 | 6.0 | 0.284 | 0. | 0.135 | 0.135 | 0.066 | 0.066 |
| 2 | 10.00 | 4.9 | -4.3 | 6.0 | 0.270 | 0. | 0.116 | 0.116 | 0.055 | 0.055 |
| 3 | 15.00 | 4.0 | -5.2 | 5.5 | 0.258 | 0. | 0.075 | 0.075 | 0.035 | 0.035 |
| 4 | 30.00 | 5.1 | -4.1 | 4.6 | 0.257 | 0. | 0.047 | 0.047 | 0.019 | 0.019 |
| 5 | 50.00 | 6.2 | -3.0 | 4.9 | 0.232 | 0. | 0.008 | 0.008 | 0.003 | 0.003 |
| 6 | 70.00 | 6.6 | -2.5 | 5.6 | 0.211 | 0. | -0.014 | -0.014 | -0.004 | -0.004 |
| 7 | 85.00 | 6.9 | -2.2 | 6.2 | 0.240 | 0. | 0.056 | 0.056 | 0.014 | 0.014 |
| 8 | 90.00 | 7.3 | -1.8 | 7.5 | 0.288 | 0. | 0.149 | 0.149 | 0.035 | 0.035 |
| 9 | 95.00 | 9.7 | 0.6 | 8.8 | 0.329 | 0. | 0.183 | 0.183 | 0.040 | 0.040 |

TABLE XI. - Continued.

(d) Reading number 1800

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 24.2 | 2.3 | 24.2 | 2.3 | 306.1 | 0.998 | 11.91 | 0.976 |
| 2 | 23.861 | 23.886 | 21.6 | 2.6 | 21.6 | 2.6 | 305.2 | 0.998 | 12.10 | 0.973 |
| 3 | 23.127 | 23.167 | 21.3 | 2.1 | 21.3 | 2.1 | 304.5 | 0.997 | 12.09 | 0.979 |
| 4 | 20.917 | 20.996 | 23.7 | 1.0 | 23.7 | 1.0 | 302.4 | 0.996 | 11.86 | 0.992 |
| 5 | 17.955 | 18.080 | 26.5 | 1.1 | 26.5 | 1.1 | 300.5 | 0.997 | 11.59 | 0.997 |
| 6 | 14.945 | 15.110 | 29.1 | 1.7 | 29.1 | 1.7 | 299.1 | 0.998 | 11.47 | 0.994 |
| 7 | 12.647 | 12.786 | 31.3 | 2.5 | 31.3 | 2.5 | 298.0 | 0.998 | 11.35 | 0.989 |
| 8 | 11.869 | 11.966 | 31.4 | 3.9 | 31.4 | 3.9 | 297.7 | 0.998 | 11.32 | 0.974 |
| 9 | 11.087 | 11.125 | 34.4 | 5.2 | 34.4 | 5.2 | 297.5 | 0.999 | 11.12 | 0.973 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 178.3 | 155.1 | 178.3 | 155.1 | 162.6 | 155.0 | 73.1 | 6.2 | 0. | 0. |
| 2 | 188.4 | 161.2 | 188.4 | 161.2 | 175.2 | 161.1 | 69.2 | 7.4 | 0. | 0. |
| 3 | 189.4 | 163.0 | 189.4 | 163.0 | 176.5 | 162.9 | 68.8 | 5.9 | 0. | 0. |
| 4 | 183.7 | 161.0 | 183.7 | 161.0 | 168.3 | 161.0 | 73.7 | 2.8 | 0. | 0. |
| 5 | 174.7 | 153.5 | 174.7 | 153.5 | 156.3 | 153.5 | 78.0 | 2.9 | 0. | 0. |
| 6 | 170.7 | 148.1 | 170.7 | 148.1 | 149.2 | 148.1 | 83.0 | 4.4 | 0. | 0. |
| 7 | 169.3 | 140.4 | 169.3 | 140.4 | 144.6 | 140.2 | 87.9 | 6.1 | 0. | 0. |
| 8 | 169.9 | 129.7 | 169.9 | 129.7 | 144.9 | 129.4 | 88.6 | 8.8 | 0. | 0. |
| 9 | 163.4 | 117.7 | 163.4 | 117.7 | 134.8 | 117.2 | 92.4 | 10.7 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.522 | 0.452 | 0.522 | 0.452 | 0.476 | 0.451 | 0.953 | 0.522 |
| 2 | 0.554 | 0.471 | 0.554 | 0.471 | 0.515 | 0.471 | 0.919 | 0.554 |
| 3 | 0.558 | 0.477 | 0.558 | 0.477 | 0.520 | 0.477 | 0.923 | 0.558 |
| 4 | 0.542 | 0.473 | 0.542 | 0.473 | 0.497 | 0.473 | 0.957 | 0.542 |
| 5 | 0.516 | 0.451 | 0.516 | 0.451 | 0.462 | 0.451 | 0.982 | 0.516 |
| 6 | 0.505 | 0.436 | 0.505 | 0.436 | 0.441 | 0.436 | 0.992 | 0.505 |
| 7 | 0.501 | 0.413 | 0.501 | 0.413 | 0.428 | 0.412 | 0.970 | 0.501 |
| 8 | 0.503 | 0.381 | 0.503 | 0.381 | 0.429 | 0.380 | 0.893 | 0.503 |
| 9 | 0.484 | 0.344 | 0.484 | 0.344 | 0.399 | 0.343 | 0.869 | 0.504 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 9.9 | 0.7 | 6.4 | 0.313 | 0. | 0.141 | 0.141 | 0.069 | 0.069 |
| 2 | 10.00 | 7.1 | -2.1 | 6.7 | 0.299 | 0. | 0.142 | 0.142 | 0.067 | 0.067 |
| 3 | 15.00 | 6.7 | -2.6 | 6.1 | 0.292 | 0. | 0.110 | 0.110 | 0.050 | 0.050 |
| 4 | 30.00 | 8.1 | -1.0 | 5.0 | 0.284 | 0. | 0.043 | 0.043 | 0.018 | 0.018 |
| 5 | 50.00 | 9.1 | -0.0 | 5.2 | 0.274 | 0. | 0.020 | 0.020 | 0.007 | 0.007 |
| 6 | 70.00 | 9.2 | 0.1 | 5.9 | 0.269 | 0. | 0.035 | 0.035 | 0.010 | 0.010 |
| 7 | 85.00 | 9.7 | 0.6 | 6.7 | 0.292 | 0. | 0.070 | 0.070 | 0.018 | 0.018 |
| 8 | 90.00 | 9.5 | 0.4 | 8.0 | 0.347 | 0. | 0.164 | 0.164 | 0.039 | 0.039 |
| 9 | 95.00 | 12.2 | 3.1 | 9.2 | 0.390 | 0. | 0.181 | 0.181 | 0.040 | 0.040 |

TABLE XI. - Continued.

(e) Reading number 1801

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 26.8 | 3.1 | 26.8 | 3.1 | 307.1 | 0.998 | 12.00 | 0.975 |
| 2 | 23.861 | 23.886 | 22.9 | 3.3 | 22.9 | 3.3 | 306.1 | 0.999 | 12.21 | 0.969 |
| 3 | 23.127 | 23.167 | 23.6 | 2.8 | 23.6 | 2.8 | 305.0 | 0.999 | 12.09 | 0.982 |
| 4 | 20.917 | 20.996 | 25.7 | 1.3 | 25.7 | 1.3 | 303.1 | 0.996 | 11.90 | 0.992 |
| 5 | 17.955 | 18.080 | 28.0 | 1.2 | 28.0 | 1.2 | 300.8 | 0.998 | 11.61 | 0.998 |
| 6 | 14.945 | 15.110 | 30.8 | 1.8 | 30.8 | 1.8 | 299.4 | 0.998 | 11.48 | 0.995 |
| 7 | 12.647 | 12.786 | 32.4 | 2.7 | 32.4 | 2.7 | 298.2 | 0.998 | 11.38 | 0.985 |
| 8 | 11.869 | 11.966 | 33.0 | 4.1 | 33.0 | 4.1 | 297.7 | 0.998 | 11.31 | 0.976 |
| 9 | 11.087 | 11.125 | 35.9 | 5.5 | 35.9 | 5.5 | 297.7 | 1.000 | 11.15 | 0.973 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 173.9 | 151.7 | 173.9 | 151.7 | 155.2 | 151.5 | 78.4 | 8.2 | 0. | 0. |
| 2 | 185.0 | 157.0 | 185.0 | 157.0 | 170.4 | 156.7 | 72.1 | 9.1 | 0. | 0. |
| 3 | 182.7 | 157.6 | 182.7 | 157.6 | 167.4 | 157.5 | 73.0 | 7.6 | 0. | 0. |
| 4 | 178.8 | 155.8 | 178.8 | 155.8 | 161.1 | 155.7 | 77.5 | 3.4 | 0. | 0. |
| 5 | 169.6 | 147.4 | 169.6 | 147.4 | 149.8 | 147.4 | 79.6 | 3.0 | 0. | 0. |
| 6 | 165.3 | 140.6 | 165.3 | 140.6 | 142.0 | 140.5 | 84.5 | 4.3 | 0. | 0. |
| 7 | 165.0 | 130.3 | 165.0 | 130.3 | 139.3 | 130.1 | 88.5 | 6.1 | 0. | 0. |
| 8 | 164.1 | 120.2 | 164.1 | 120.2 | 137.6 | 119.9 | 89.5 | 8.5 | 0. | 0. |
| 9 | 158.7 | 107.9 | 158.7 | 107.9 | 128.5 | 107.4 | 93.2 | 10.3 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.508 | 0.440 | 0.508 | 0.440 | 0.453 | 0.440 | 0.976 | 0.547 |
| 2 | 0.543 | 0.457 | 0.543 | 0.457 | 0.500 | 0.456 | 0.920 | 0.543 |
| 3 | 0.537 | 0.460 | 0.537 | 0.460 | 0.492 | 0.459 | 0.940 | 0.537 |
| 4 | 0.526 | 0.456 | 0.526 | 0.456 | 0.474 | 0.456 | 0.967 | 0.526 |
| 5 | 0.500 | 0.432 | 0.500 | 0.432 | 0.441 | 0.432 | 0.984 | 0.500 |
| 6 | 0.488 | 0.413 | 0.488 | 0.413 | 0.419 | 0.412 | 0.989 | 0.488 |
| 7 | 0.488 | 0.382 | 0.488 | 0.382 | 0.412 | 0.382 | 0.934 | 0.488 |
| 8 | 0.486 | 0.352 | 0.486 | 0.352 | 0.407 | 0.351 | 0.872 | 0.486 |
| 9 | 0.469 | 0.315 | 0.469 | 0.315 | 0.380 | 0.314 | 0.836 | 0.529 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 12.5 | 3.3 | 7.2 | 0.325 | 0. | 0.152 | 0.152 | 0.074 | 0.074 |
| 2 | 10.00 | 8.5 | -0.7 | 7.4 | 0.313 | 0. | 0.169 | 0.169 | 0.080 | 0.080 |
| 3 | 15.00 | 8.9 | -0.3 | 6.8 | 0.301 | 0. | 0.099 | 0.099 | 0.046 | 0.046 |
| 4 | 30.00 | 10.2 | 1.0 | 5.3 | 0.301 | 0. | 0.047 | 0.047 | 0.019 | 0.019 |
| 5 | 50.00 | 10.6 | 1.4 | 5.3 | 0.291 | 0. | 0.015 | 0.015 | 0.005 | 0.005 |
| 6 | 70.00 | 10.9 | 1.8 | 6.0 | 0.293 | 0. | 0.033 | 0.033 | 0.010 | 0.010 |
| 7 | 85.00 | 10.8 | 1.7 | 6.9 | 0.336 | 0. | 0.102 | 0.102 | 0.026 | 0.026 |
| 8 | 90.00 | 11.1 | 2.0 | 8.2 | 0.384 | 0. | 0.163 | 0.163 | 0.039 | 0.039 |
| 9 | 95.00 | 13.7 | 4.6 | 9.5 | 0.435 | 0. | 0.194 | 0.194 | 0.042 | 0.042 |

TABLE XI. - Concluded.

(f) Reading number 1807

| RP | RADIO | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 27.5 | 3.6 | 27.5 | 3.6 | 308.2 | 0.999 | 12.06 | 0.974 |
| 2 | 23.861 | 23.886 | 23.7 | 3.8 | 23.7 | 3.8 | 306.6 | 1.000 | 12.23 | 0.969 |
| 3 | 23.127 | 23.167 | 24.0 | 3.0 | 24.0 | 3.0 | 305.3 | 1.000 | 12.15 | 0.979 |
| 4 | 20.917 | 20.996 | 26.4 | 1.4 | 26.4 | 1.4 | 303.5 | 0.996 | 11.92 | 0.992 |
| 5 | 17.955 | 18.080 | 29.5 | 1.4 | 29.5 | 1.4 | 301.5 | 0.996 | 11.66 | 0.996 |
| 6 | 14.945 | 15.110 | 31.8 | 1.9 | 31.8 | 1.9 | 299.5 | 0.998 | 11.49 | 0.996 |
| 7 | 12.647 | 12.786 | 33.0 | 2.8 | 33.0 | 2.8 | 298.2 | 0.998 | 11.36 | 0.985 |
| 8 | 11.869 | 11.966 | 33.7 | 4.3 | 33.7 | 4.3 | 297.8 | 0.999 | 11.29 | 0.977 |
| 9 | 11.087 | 11.125 | 36.6 | 5.7 | 36.6 | 5.7 | 297.6 | 1.000 | 11.14 | 0.975 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 173.5 | 150.1 | 173.5 | 150.1 | 154.0 | 149.9 | 80.0 | 9.4 | 0. | 0. |
| 2 | 183.1 | 154.4 | 183.1 | 154.4 | 167.7 | 154.1 | 73.6 | 10.1 | 0. | 0. |
| 3 | 181.7 | 155.2 | 181.7 | 155.2 | 166.0 | 155.0 | 73.9 | 8.1 | 0. | 0. |
| 4 | 176.8 | 153.3 | 176.8 | 153.3 | 158.3 | 153.3 | 78.7 | 3.7 | 0. | 0. |
| 5 | 168.3 | 144.6 | 168.3 | 144.6 | 146.5 | 144.6 | 82.8 | 3.5 | 0. | 0. |
| 6 | 162.8 | 137.3 | 162.8 | 137.3 | 138.4 | 137.2 | 85.8 | 4.5 | 0. | 0. |
| 7 | 161.6 | 125.4 | 161.6 | 125.4 | 135.6 | 125.3 | 87.9 | 6.1 | 0. | 0. |
| 8 | 161.1 | 116.1 | 161.1 | 116.1 | 134.1 | 115.8 | 89.3 | 8.7 | 0. | 0. |
| 9 | 156.3 | 104.3 | 156.3 | 104.3 | 125.5 | 103.8 | 93.2 | 10.3 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.506 | 0.435 | 0.506 | 0.435 | 0.449 | 0.434 | 0.973 | 0.563 |
| 2 | 0.537 | 0.449 | 0.537 | 0.449 | 0.491 | 0.448 | 0.919 | 0.537 |
| 3 | 0.533 | 0.452 | 0.533 | 0.452 | 0.487 | 0.452 | 0.934 | 0.533 |
| 4 | 0.520 | 0.449 | 0.520 | 0.449 | 0.465 | 0.448 | 0.968 | 0.520 |
| 5 | 0.495 | 0.424 | 0.495 | 0.424 | 0.431 | 0.424 | 0.987 | 0.526 |
| 6 | 0.480 | 0.402 | 0.480 | 0.402 | 0.408 | 0.402 | 0.991 | 0.513 |
| 7 | 0.477 | 0.368 | 0.477 | 0.368 | 0.401 | 0.367 | 0.924 | 0.484 |
| 8 | 0.476 | 0.340 | 0.476 | 0.340 | 0.396 | 0.339 | 0.864 | 0.489 |
| 9 | 0.462 | 0.304 | 0.462 | 0.304 | 0.371 | 0.303 | 0.827 | 0.534 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-----|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 13.2 | 4.0 | 7.7 | 0.333 | 0. | 0.163 | 0.163 | 0.079 | 0.079 |
| 2 | 10.00 | 9.2 | 0.0 | 7.8 | 0.321 | 0. | 0.172 | 0.172 | 0.081 | 0.081 |
| 3 | 15.00 | 9.4 | 0.1 | 7.0 | 0.312 | 0. | 0.122 | 0.122 | 0.056 | 0.056 |
| 4 | 30.00 | 10.9 | 1.7 | 5.4 | 0.309 | 0. | 0.047 | 0.047 | 0.019 | 0.019 |
| 5 | 50.00 | 12.1 | 2.9 | 5.5 | 0.309 | 0. | 0.024 | 0.024 | 0.009 | 0.009 |
| 6 | 70.00 | 11.9 | 2.8 | 6.1 | 0.305 | 0. | 0.028 | 0.028 | 0.008 | 0.008 |
| 7 | 85.00 | 11.4 | 2.3 | 7.0 | 0.351 | 0. | 0.101 | 0.101 | 0.025 | 0.025 |
| 8 | 90.00 | 11.7 | 2.6 | 8.4 | 0.397 | 0. | 0.160 | 0.160 | 0.038 | 0.038 |
| 9 | 95.00 | 14.4 | 5.3 | 9.7 | 0.449 | 0. | 0.185 | 0.185 | 0.041 | 0.041 |

TABLE XII. - BLADE-ELEMENT DATA AT BLADE EDGES FOR STATOR 51

WITH STAGE 51B C-51 AT 100 PERCENT DESIGN SPEED

(a) Reading number 1830

| RP | RADIO | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 15.4 | 1.0 | 15.4 | 1.0 | 300.0 | 0.995 | 11.15 | 0.979 |
| 2 | 23.861 | 23.886 | 13.6 | 0.9 | 13.6 | 0.9 | 299.3 | 0.997 | 11.32 | 0.983 |
| 3 | 23.127 | 23.167 | 13.7 | 0.3 | 13.7 | 0.3 | 298.8 | 0.999 | 11.33 | 0.990 |
| 4 | 20.917 | 20.996 | 15.9 | 0.1 | 15.9 | 0.1 | 298.0 | 0.997 | 11.36 | 0.993 |
| 5 | 17.955 | 18.080 | 19.6 | 0.5 | 19.6 | 0.5 | 297.9 | 0.996 | 11.36 | 0.994 |
| 6 | 14.945 | 15.110 | 22.3 | 1.4 | 22.3 | 1.4 | 297.3 | 0.998 | 11.28 | 0.999 |
| 7 | 12.647 | 12.786 | 23.6 | 2.0 | 23.6 | 2.0 | 295.5 | 0.999 | 11.03 | 0.995 |
| 8 | 11.869 | 11.966 | 23.1 | 2.5 | 23.1 | 2.5 | 294.5 | 1.001 | 10.89 | 0.990 |
| 9 | 11.087 | 11.125 | 24.7 | 3.8 | 24.7 | 3.8 | 294.5 | 1.001 | 10.71 | 0.981 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|-----|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 174.5 | 156.0 | 174.5 | 156.0 | 168.3 | 155.9 | 46.3 | 2.7 | 0. | 0. |
| 2 | 182.8 | 164.0 | 182.8 | 164.0 | 177.7 | 164.0 | 43.0 | 2.7 | 0. | 0. |
| 3 | 184.3 | 167.3 | 184.3 | 167.3 | 179.0 | 167.3 | 43.7 | 1.0 | 0. | 0. |
| 4 | 187.2 | 171.4 | 187.2 | 171.4 | 180.1 | 171.4 | 51.1 | 0.4 | 0. | 0. |
| 5 | 186.0 | 174.6 | 186.0 | 174.6 | 175.3 | 174.6 | 62.4 | 1.5 | 0. | 0. |
| 6 | 183.8 | 175.4 | 183.8 | 175.4 | 170.0 | 175.4 | 69.9 | 4.3 | 0. | 0. |
| 7 | 175.3 | 164.2 | 175.3 | 164.2 | 160.7 | 164.1 | 70.1 | 5.7 | 0. | 0. |
| 8 | 169.9 | 155.4 | 169.9 | 155.4 | 156.2 | 155.3 | 66.8 | 6.8 | 0. | 0. |
| 9 | 162.9 | 141.3 | 162.9 | 141.3 | 148.0 | 141.0 | 67.9 | 9.4 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.516 | 0.460 | 0.516 | 0.460 | 0.497 | 0.460 | 0.927 | 0.516 |
| 2 | 0.542 | 0.485 | 0.542 | 0.485 | 0.527 | 0.485 | 0.923 | 0.542 |
| 3 | 0.547 | 0.495 | 0.547 | 0.495 | 0.532 | 0.495 | 0.935 | 0.547 |
| 4 | 0.558 | 0.509 | 0.558 | 0.509 | 0.536 | 0.509 | 0.952 | 0.558 |
| 5 | 0.554 | 0.519 | 0.554 | 0.519 | 0.522 | 0.519 | 0.996 | 0.554 |
| 6 | 0.547 | 0.522 | 0.547 | 0.522 | 0.506 | 0.522 | 1.032 | 0.547 |
| 7 | 0.522 | 0.488 | 0.522 | 0.488 | 0.479 | 0.488 | 1.021 | 0.522 |
| 8 | 0.506 | 0.461 | 0.506 | 0.461 | 0.466 | 0.461 | 0.994 | 0.506 |
| 9 | 0.484 | 0.418 | 0.484 | 0.418 | 0.440 | 0.417 | 0.952 | 0.484 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 1.1 | -8.1 | 5.0 | 0.228 | 0. | 0.125 | 0.125 | 0.061 | 0.061 |
| 2 | 10.00 | -0.8 | -10.0 | 5.0 | 0.207 | 0. | 0.096 | 0.096 | 0.045 | 0.045 |
| 3 | 15.00 | -0.9 | -10.1 | 4.3 | 0.198 | 0. | 0.052 | 0.052 | 0.024 | 0.024 |
| 4 | 30.00 | 0.3 | -8.8 | 4.1 | 0.197 | 0. | 0.035 | 0.035 | 0.014 | 0.014 |
| 5 | 50.00 | 2.2 | -7.0 | 4.6 | 0.178 | 0. | 0.030 | 0.030 | 0.011 | 0.011 |
| 6 | 70.00 | 2.5 | -6.6 | 5.6 | 0.151 | 0. | 0.005 | 0.005 | 0.002 | 0.002 |
| 7 | 85.00 | 2.0 | -7.1 | 6.2 | 0.156 | 0. | 0.030 | 0.030 | 0.008 | 0.008 |
| 8 | 90.00 | 1.2 | -7.9 | 6.6 | 0.169 | 0. | 0.064 | 0.064 | 0.015 | 0.015 |
| 9 | 95.00 | 2.5 | -6.7 | 7.8 | 0.212 | 0. | 0.131 | 0.131 | 0.029 | 0.029 |

TABLE XII. - Continued.

(b) Reading number 1829

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 19.0 | 1.6 | 19.0 | 1.6 | 301.9 | 0.997 | 11.53 | 0.981 |
| 2 | 23.861 | 23.886 | 17.3 | 1.6 | 17.3 | 1.6 | 301.2 | 0.998 | 11.66 | 0.983 |
| 3 | 23.127 | 23.167 | 17.2 | 1.1 | 17.2 | 1.1 | 300.7 | 0.998 | 11.66 | 0.990 |
| 4 | 20.917 | 20.996 | 19.8 | 0.7 | 19.8 | 0.7 | 300.1 | 0.997 | 11.63 | 0.993 |
| 5 | 17.955 | 18.080 | 23.2 | 1.2 | 23.2 | 1.2 | 299.0 | 0.998 | 11.51 | 0.997 |
| 6 | 14.945 | 15.110 | 26.0 | 1.8 | 26.0 | 1.8 | 297.8 | 0.999 | 11.36 | 0.999 |
| 7 | 12.647 | 12.786 | 26.9 | 2.3 | 26.9 | 2.3 | 296.0 | 1.000 | 11.10 | 0.996 |
| 8 | 11.869 | 11.966 | 26.8 | 2.8 | 26.8 | 2.8 | 295.5 | 1.000 | 11.01 | 0.987 |
| 9 | 11.087 | 11.125 | 29.4 | 4.3 | 29.4 | 4.3 | 295.4 | 1.000 | 10.89 | 0.979 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|-----|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 165.8 | 148.6 | 165.8 | 148.6 | 156.8 | 148.5 | 54.1 | 4.2 | 0. | 0. |
| 2 | 174.2 | 155.8 | 174.2 | 155.8 | 166.3 | 155.7 | 51.9 | 4.4 | 0. | 0. |
| 3 | 175.0 | 158.0 | 175.0 | 158.0 | 167.2 | 158.0 | 51.8 | 3.1 | 0. | 0. |
| 4 | 176.1 | 159.7 | 176.1 | 159.7 | 165.7 | 159.7 | 59.6 | 2.0 | 0. | 0. |
| 5 | 173.3 | 158.3 | 173.3 | 158.3 | 159.3 | 158.2 | 68.2 | 3.3 | 0. | 0. |
| 6 | 169.0 | 154.8 | 169.0 | 154.8 | 151.9 | 154.7 | 74.1 | 4.8 | 0. | 0. |
| 7 | 160.3 | 140.7 | 160.3 | 140.7 | 143.0 | 140.6 | 72.5 | 5.7 | 0. | 0. |
| 8 | 157.6 | 131.9 | 157.6 | 131.9 | 140.7 | 131.8 | 71.1 | 6.5 | 0. | 0. |
| 9 | 152.8 | 119.3 | 152.8 | 119.3 | 133.1 | 119.0 | 75.1 | 8.9 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.487 | 0.435 | 0.487 | 0.435 | 0.461 | 0.435 | 0.947 | 0.487 |
| 2 | 0.514 | 0.458 | 0.514 | 0.458 | 0.490 | 0.457 | 0.937 | 0.514 |
| 3 | 0.517 | 0.465 | 0.517 | 0.465 | 0.494 | 0.465 | 0.945 | 0.517 |
| 4 | 0.521 | 0.471 | 0.521 | 0.471 | 0.490 | 0.471 | 0.964 | 0.521 |
| 5 | 0.513 | 0.467 | 0.513 | 0.467 | 0.472 | 0.467 | 0.993 | 0.513 |
| 6 | 0.501 | 0.457 | 0.501 | 0.457 | 0.450 | 0.457 | 1.019 | 0.501 |
| 7 | 0.475 | 0.415 | 0.475 | 0.415 | 0.424 | 0.415 | 0.984 | 0.475 |
| 8 | 0.467 | 0.389 | 0.467 | 0.389 | 0.417 | 0.388 | 0.937 | 0.467 |
| 9 | 0.452 | 0.351 | 0.452 | 0.351 | 0.394 | 0.350 | 0.894 | 0.452 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 4.7 | -4.5 | 5.7 | 0.251 | 0. | 0.126 | 0.126 | 0.062 | 0.062 |
| 2 | 10.00 | 2.9 | -6.3 | 5.6 | 0.235 | 0. | 0.101 | 0.101 | 0.048 | 0.048 |
| 3 | 15.00 | 2.6 | -6.6 | 5.1 | 0.225 | 0. | 0.057 | 0.057 | 0.026 | 0.026 |
| 4 | 30.00 | 4.3 | -4.9 | 4.7 | 0.229 | 0. | 0.042 | 0.042 | 0.018 | 0.018 |
| 5 | 50.00 | 5.8 | -3.4 | 5.3 | 0.220 | 0. | 0.021 | 0.021 | 0.008 | 0.008 |
| 6 | 70.00 | 6.1 | -3.0 | 6.0 | 0.205 | 0. | 0.004 | 0.004 | 0.001 | 0.001 |
| 7 | 85.00 | 5.3 | -3.8 | 6.5 | 0.227 | 0. | 0.031 | 0.031 | 0.008 | 0.008 |
| 8 | 90.00 | 4.9 | -4.2 | 6.9 | 0.259 | 0. | 0.093 | 0.093 | 0.022 | 0.022 |
| 9 | 95.00 | 7.2 | -1.9 | 8.3 | 0.314 | 0. | 0.163 | 0.163 | 0.036 | 0.036 |

TABLE XII. - Continued.

(c) Reading number 1828

| RP | RADIO | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 20.3 | 2.0 | 20.3 | 2.0 | 302.8 | 0.998 | 11.63 | 0.979 |
| 2 | 23.861 | 23.886 | 18.9 | 2.2 | 18.9 | 2.2 | 302.2 | 0.999 | 11.72 | 0.984 |
| 3 | 23.127 | 23.167 | 18.9 | 1.6 | 18.9 | 1.6 | 300.9 | 0.999 | 11.69 | 0.991 |
| 4 | 20.917 | 20.996 | 21.4 | 0.6 | 21.4 | 0.6 | 299.6 | 0.998 | 11.54 | 0.997 |
| 5 | 17.955 | 18.080 | 24.6 | 0.8 | 24.6 | 0.8 | 298.4 | 0.999 | 11.39 | 1.001 |
| 6 | 14.945 | 15.110 | 27.4 | 1.7 | 27.4 | 1.7 | 297.6 | 0.999 | 11.30 | 1.000 |
| 7 | 12.647 | 12.786 | 29.0 | 2.2 | 29.0 | 2.2 | 296.0 | 1.000 | 11.12 | 0.995 |
| 8 | 11.869 | 11.966 | 29.5 | 3.5 | 29.5 | 3.5 | 295.8 | 1.000 | 11.08 | 0.985 |
| 9 | 11.087 | 11.125 | 32.5 | 5.3 | 32.5 | 5.3 | 296.1 | 1.000 | 10.96 | 0.980 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 162.3 | 142.9 | 162.3 | 142.9 | 152.2 | 142.8 | 56.4 | 4.9 | 0. | 0. |
| 2 | 167.7 | 148.8 | 167.7 | 148.8 | 158.6 | 148.7 | 54.3 | 5.8 | 0. | 0. |
| 3 | 167.4 | 150.0 | 167.4 | 150.0 | 158.4 | 150.0 | 54.3 | 4.1 | 0. | 0. |
| 4 | 163.9 | 148.7 | 163.9 | 148.7 | 152.6 | 148.7 | 59.7 | 1.7 | 0. | 0. |
| 5 | 158.0 | 144.6 | 158.0 | 144.6 | 143.7 | 144.6 | 65.7 | 2.1 | 0. | 0. |
| 6 | 155.9 | 140.5 | 155.9 | 140.5 | 138.5 | 140.4 | 71.6 | 4.1 | 0. | 0. |
| 7 | 150.8 | 129.9 | 150.8 | 129.9 | 132.0 | 129.8 | 73.1 | 5.0 | 0. | 0. |
| 8 | 150.1 | 120.6 | 150.1 | 120.6 | 130.7 | 120.3 | 73.9 | 7.3 | 0. | 0. |
| 9 | 145.4 | 109.4 | 145.4 | 109.4 | 122.7 | 109.0 | 78.1 | 10.1 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.476 | 0.417 | 0.476 | 0.417 | 0.446 | 0.417 | 0.938 | 0.476 |
| 2 | 0.493 | 0.435 | 0.493 | 0.435 | 0.466 | 0.435 | 0.938 | 0.493 |
| 3 | 0.493 | 0.440 | 0.493 | 0.440 | 0.466 | 0.440 | 0.947 | 0.493 |
| 4 | 0.483 | 0.437 | 0.483 | 0.437 | 0.450 | 0.437 | 0.974 | 0.483 |
| 5 | 0.466 | 0.425 | 0.466 | 0.425 | 0.424 | 0.425 | 1.006 | 0.466 |
| 6 | 0.460 | 0.413 | 0.460 | 0.413 | 0.409 | 0.413 | 1.014 | 0.460 |
| 7 | 0.446 | 0.382 | 0.446 | 0.382 | 0.390 | 0.382 | 0.984 | 0.446 |
| 8 | 0.444 | 0.354 | 0.444 | 0.354 | 0.386 | 0.353 | 0.921 | 0.444 |
| 9 | 0.429 | 0.320 | 0.429 | 0.320 | 0.362 | 0.319 | 0.888 | 0.429 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 6.0 | -3.2 | 6.0 | 0.275 | 0. | 0.146 | 0.146 | 0.071 | 0.071 |
| 2 | 10.00 | 4.5 | -4.8 | 6.2 | 0.249 | 0. | 0.104 | 0.104 | 0.049 | 0.049 |
| 3 | 15.00 | 4.3 | -4.9 | 5.6 | 0.242 | 0. | 0.062 | 0.062 | 0.028 | 0.028 |
| 4 | 30.00 | 5.9 | -3.3 | 4.6 | 0.240 | 0. | 0.023 | 0.023 | 0.009 | 0.009 |
| 5 | 50.00 | 7.2 | -2.0 | 5.0 | 0.228 | 0. | -0.008 | -0.008 | -0.003 | -0.003 |
| 6 | 70.00 | 7.5 | -1.6 | 5.9 | 0.227 | 0. | -0.001 | -0.001 | -0.000 | -0.000 |
| 7 | 85.00 | 7.4 | -1.7 | 6.4 | 0.252 | 0. | 0.036 | 0.036 | 0.009 | 0.009 |
| 8 | 90.00 | 7.5 | -1.6 | 7.6 | 0.301 | 0. | 0.119 | 0.119 | 0.028 | 0.028 |
| 9 | 95.00 | 10.3 | 1.2 | 9.3 | 0.350 | 0. | 0.166 | 0.166 | 0.037 | 0.037 |

TABLE XII. - Continued.

(d) Reading number 1824

| RP | RADIO | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 27.8 | 4.4 | 27.8 | 4.4 | 306.0 | 0.998 | 11.89 | 0.977 |
| 2 | 23.861 | 23.886 | 24.4 | 3.9 | 24.4 | 3.9 | 304.3 | 1.000 | 11.95 | 0.979 |
| 3 | 23.127 | 23.167 | 24.7 | 3.1 | 24.7 | 3.1 | 303.9 | 0.998 | 11.95 | 0.982 |
| 4 | 20.917 | 20.996 | 27.5 | 1.5 | 27.5 | 1.5 | 302.0 | 0.997 | 11.74 | 0.993 |
| 5 | 17.955 | 18.080 | 30.7 | 1.5 | 30.7 | 1.5 | 299.8 | 0.999 | 11.49 | 1.000 |
| 6 | 14.945 | 15.110 | 33.4 | 2.2 | 33.4 | 2.2 | 298.5 | 0.999 | 11.38 | 0.995 |
| 7 | 12.647 | 12.786 | 34.7 | 3.7 | 34.7 | 3.7 | 297.3 | 0.999 | 11.26 | 0.984 |
| 8 | 11.869 | 11.966 | 35.6 | 5.0 | 35.6 | 5.0 | 297.0 | 0.999 | 11.20 | 0.978 |
| 9 | 11.087 | 11.125 | 39.0 | 5.8 | 39.0 | 5.8 | 296.8 | 1.000 | 11.07 | 0.980 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 150.4 | 132.3 | 150.4 | 132.3 | 133.0 | 131.9 | 70.2 | 10.2 | 0. | 0. |
| 2 | 157.0 | 136.2 | 157.0 | 136.2 | 143.0 | 135.9 | 64.8 | 9.3 | 0. | 0. |
| 3 | 157.8 | 137.1 | 157.8 | 137.1 | 143.4 | 136.9 | 65.8 | 7.4 | 0. | 0. |
| 4 | 152.2 | 134.1 | 152.2 | 134.1 | 135.0 | 134.1 | 70.2 | 3.5 | 0. | 0. |
| 5 | 141.6 | 125.0 | 141.6 | 125.0 | 121.7 | 125.0 | 72.4 | 3.3 | 0. | 0. |
| 6 | 139.9 | 116.0 | 139.9 | 116.0 | 116.7 | 115.9 | 77.1 | 4.5 | 0. | 0. |
| 7 | 137.8 | 100.7 | 137.8 | 100.7 | 113.3 | 100.5 | 78.5 | 6.4 | 0. | 0. |
| 8 | 137.1 | 91.3 | 137.1 | 91.3 | 111.5 | 91.0 | 79.8 | 7.9 | 0. | 0. |
| 9 | 132.4 | 82.5 | 132.4 | 82.5 | 102.9 | 82.1 | 83.3 | 8.4 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.437 | 0.383 | 0.437 | 0.383 | 0.386 | 0.382 | 0.992 | 0.494 |
| 2 | 0.458 | 0.396 | 0.458 | 0.396 | 0.418 | 0.395 | 0.950 | 0.458 |
| 3 | 0.461 | 0.399 | 0.461 | 0.399 | 0.419 | 0.398 | 0.955 | 0.461 |
| 4 | 0.445 | 0.391 | 0.445 | 0.391 | 0.395 | 0.391 | 0.993 | 0.460 |
| 5 | 0.415 | 0.365 | 0.415 | 0.365 | 0.357 | 0.365 | 1.027 | 0.468 |
| 6 | 0.411 | 0.339 | 0.411 | 0.339 | 0.343 | 0.339 | 0.993 | 0.473 |
| 7 | 0.405 | 0.294 | 0.405 | 0.294 | 0.333 | 0.294 | 0.887 | 0.455 |
| 8 | 0.403 | 0.266 | 0.403 | 0.266 | 0.328 | 0.265 | 0.816 | 0.459 |
| 9 | 0.389 | 0.240 | 0.389 | 0.240 | 0.302 | 0.239 | 0.798 | 0.488 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-----|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 13.5 | 4.3 | 8.5 | 0.315 | 0. | 0.187 | 0.187 | 0.091 | 0.091 |
| 2 | 10.00 | 9.9 | 0.7 | 7.9 | 0.300 | 0. | 0.160 | 0.160 | 0.076 | 0.076 |
| 3 | 15.00 | 10.0 | 0.8 | 7.1 | 0.301 | 0. | 0.131 | 0.131 | 0.060 | 0.060 |
| 4 | 30.00 | 11.9 | 2.8 | 5.5 | 0.301 | 0. | 0.051 | 0.051 | 0.021 | 0.021 |
| 5 | 50.00 | 13.3 | 4.2 | 5.6 | 0.291 | 0. | 0.001 | 0.001 | 0.000 | 0.000 |
| 6 | 70.00 | 13.6 | 4.5 | 6.4 | 0.324 | 0. | 0.048 | 0.048 | 0.014 | 0.014 |
| 7 | 85.00 | 13.1 | 4.0 | 7.9 | 0.400 | 0. | 0.145 | 0.145 | 0.037 | 0.037 |
| 8 | 90.00 | 13.7 | 4.5 | 9.1 | 0.457 | 0. | 0.205 | 0.205 | 0.048 | 0.048 |
| 9 | 95.00 | 16.8 | 7.7 | 9.8 | 0.501 | 0. | 0.201 | 0.201 | 0.044 | 0.044 |

TABLE XII. - Continued.

(e) Reading number 1827

| RP | RADII | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 23.3 | 2.5 | 23.3 | 2.5 | 304.3 | 0.998 | 11.76 | 0.978 |
| 2 | 23.861 | 23.886 | 20.9 | 2.8 | 20.9 | 2.8 | 303.0 | 1.000 | 11.84 | 0.982 |
| 3 | 23.127 | 23.167 | 21.3 | 2.1 | 21.3 | 2.1 | 302.4 | 0.999 | 11.81 | 0.986 |
| 4 | 20.917 | 20.996 | 23.9 | 0.9 | 23.9 | 0.9 | 301.2 | 0.997 | 11.68 | 0.991 |
| 5 | 17.955 | 18.080 | 26.8 | 1.1 | 26.8 | 1.1 | 299.1 | 0.999 | 11.42 | 1.001 |
| 6 | 14.945 | 15.110 | 30.0 | 1.9 | 30.0 | 1.9 | 297.9 | 0.999 | 11.34 | 0.997 |
| 7 | 12.647 | 12.786 | 31.3 | 2.8 | 31.3 | 2.8 | 296.9 | 0.999 | 11.21 | 0.990 |
| 8 | 11.869 | 11.966 | 32.1 | 4.2 | 32.1 | 4.2 | 296.3 | 0.999 | 11.15 | 0.981 |
| 9 | 11.087 | 11.125 | 35.0 | 5.6 | 35.0 | 5.6 | 296.3 | 1.000 | 11.01 | 0.981 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|-----|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 156.8 | 137.1 | 156.8 | 137.1 | 144.0 | 136.9 | 62.0 | 6.1 | 0. | 0. |
| 2 | 162.0 | 142.1 | 162.0 | 142.1 | 151.3 | 142.0 | 57.9 | 6.8 | 0. | 0. |
| 3 | 162.1 | 143.2 | 162.1 | 143.2 | 151.1 | 143.1 | 58.8 | 5.3 | 0. | 0. |
| 4 | 159.8 | 140.7 | 159.8 | 140.7 | 146.1 | 140.7 | 64.8 | 2.3 | 0. | 0. |
| 5 | 149.1 | 134.1 | 149.1 | 134.1 | 133.1 | 134.1 | 67.3 | 2.7 | 0. | 0. |
| 6 | 147.3 | 128.7 | 147.3 | 128.7 | 127.5 | 128.6 | 73.7 | 4.3 | 0. | 0. |
| 7 | 145.4 | 117.7 | 145.4 | 117.7 | 124.2 | 117.5 | 75.6 | 5.8 | 0. | 0. |
| 8 | 144.5 | 107.9 | 144.5 | 107.9 | 122.5 | 107.6 | 76.8 | 7.9 | 0. | 0. |
| 9 | 138.5 | 97.5 | 138.5 | 97.5 | 113.4 | 97.0 | 79.5 | 9.5 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.458 | 0.398 | 0.458 | 0.398 | 0.420 | 0.398 | 0.951 | 0.458 |
| 2 | 0.475 | 0.414 | 0.475 | 0.414 | 0.443 | 0.414 | 0.938 | 0.475 |
| 3 | 0.476 | 0.418 | 0.476 | 0.418 | 0.443 | 0.418 | 0.947 | 0.476 |
| 4 | 0.469 | 0.412 | 0.469 | 0.412 | 0.429 | 0.412 | 0.963 | 0.469 |
| 5 | 0.438 | 0.393 | 0.438 | 0.393 | 0.391 | 0.393 | 1.008 | 0.438 |
| 6 | 0.434 | 0.378 | 0.434 | 0.378 | 0.376 | 0.377 | 1.009 | 0.434 |
| 7 | 0.429 | 0.345 | 0.429 | 0.345 | 0.366 | 0.345 | 0.946 | 0.429 |
| 8 | 0.426 | 0.316 | 0.426 | 0.316 | 0.361 | 0.315 | 0.879 | 0.426 |
| 9 | 0.408 | 0.285 | 0.408 | 0.285 | 0.334 | 0.283 | 0.855 | 0.441 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|------|-----|--------|-----|------------|--------|------------|--------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 9.0 | -0.2 | 6.6 | 0.300 | 0. | 0.163 | 0.163 | 0.079 | 0.079 |
| 2 | 10.00 | 6.5 | -2.7 | 6.8 | 0.272 | 0. | 0.128 | 0.128 | 0.060 | 0.060 |
| 3 | 15.00 | 6.6 | -2.6 | 6.1 | 0.269 | 0. | 0.095 | 0.095 | 0.043 | 0.043 |
| 4 | 30.00 | 8.4 | -0.8 | 4.9 | 0.282 | 0. | 0.063 | 0.063 | 0.026 | 0.026 |
| 5 | 50.00 | 9.4 | 0.3 | 5.2 | 0.255 | 0. | -0.010 | -0.010 | -0.003 | -0.003 |
| 6 | 70.00 | 10.2 | 1.1 | 6.1 | 0.266 | 0. | 0.026 | 0.026 | 0.008 | 0.008 |
| 7 | 85.00 | 9.7 | 0.6 | 7.0 | 0.311 | 0. | 0.084 | 0.084 | 0.021 | 0.021 |
| 8 | 90.00 | 10.1 | 1.0 | 8.3 | 0.366 | 0. | 0.162 | 0.162 | 0.038 | 0.038 |
| 9 | 95.00 | 12.8 | 3.7 | 9.6 | 0.407 | 0. | 0.177 | 0.177 | 0.039 | 0.039 |

TABLE XII. - Concluded.

(f) Reading number 1841

| RP | RADI | | ABS BETAM | | REL BETAM | | TOTAL TEMP | | TOTAL PRESS | |
|----|--------|--------|-----------|-----|-----------|-----|------------|-------|-------------|-------|
| | IN | OUT | IN | OUT | IN | OUT | IN | RATIO | IN | RATIO |
| 1 | 24.595 | 24.608 | 31.4 | 5.5 | 31.4 | 5.5 | 306.7 | 1.000 | 11.91 | 0.976 |
| 2 | 23.861 | 23.886 | 27.3 | 5.2 | 27.3 | 5.2 | 305.2 | 1.002 | 12.00 | 0.976 |
| 3 | 23.127 | 23.167 | 27.0 | 4.0 | 27.0 | 4.0 | 304.4 | 1.000 | 11.98 | 0.980 |
| 4 | 20.917 | 20.996 | 29.5 | 2.2 | 29.5 | 2.2 | 302.7 | 0.996 | 11.80 | 0.992 |
| 5 | 17.955 | 18.080 | 32.5 | 1.7 | 32.5 | 1.7 | 300.3 | 0.998 | 11.56 | 0.998 |
| 6 | 14.945 | 15.110 | 34.7 | 2.7 | 34.7 | 2.7 | 298.8 | 0.998 | 11.46 | 0.989 |
| 7 | 12.647 | 12.786 | 36.2 | 4.2 | 36.2 | 4.2 | 297.2 | 0.999 | 11.27 | 0.985 |
| 8 | 11.869 | 11.966 | 37.4 | 5.3 | 37.4 | 5.3 | 296.8 | 1.000 | 11.21 | 0.980 |
| 9 | 11.087 | 11.125 | 41.1 | 5.6 | 41.1 | 5.6 | 296.9 | 1.001 | 11.10 | 0.981 |

| RP | ABS VEL | | REL VEL | | MERID VEL | | TANG VEL | | WHEEL SPEED | |
|----|---------|-------|---------|-------|-----------|-------|----------|------|-------------|-----|
| | IN | OUT | IN | OUT | IN | OUT | IN | OUT | IN | OUT |
| 1 | 145.4 | 126.7 | 145.4 | 126.7 | 124.0 | 126.1 | 75.8 | 12.2 | 0. | 0. |
| 2 | 152.1 | 130.5 | 152.1 | 130.5 | 135.2 | 130.0 | 69.7 | 11.9 | 0. | 0. |
| 3 | 153.6 | 131.3 | 153.6 | 131.3 | 136.8 | 131.0 | 69.8 | 9.1 | 0. | 0. |
| 4 | 149.3 | 130.0 | 149.3 | 130.0 | 129.9 | 129.9 | 73.5 | 5.0 | 0. | 0. |
| 5 | 139.8 | 121.2 | 139.8 | 121.2 | 117.9 | 121.2 | 75.1 | 3.6 | 0. | 0. |
| 6 | 138.3 | 109.4 | 138.3 | 109.4 | 113.7 | 109.3 | 78.7 | 5.1 | 0. | 0. |
| 7 | 133.3 | 94.3 | 133.3 | 94.3 | 107.6 | 94.0 | 78.8 | 7.0 | 0. | 0. |
| 8 | 132.3 | 84.6 | 132.3 | 84.6 | 105.1 | 84.2 | 80.3 | 7.8 | 0. | 0. |
| 9 | 128.8 | 76.0 | 128.8 | 76.0 | 97.0 | 75.6 | 84.7 | 7.4 | 0. | 0. |

| RP | ABS MACH NO | | REL MACH NO | | MERID MACH NO | | MERID PEAK SS | |
|----|-------------|-------|-------------|-------|---------------|-------|---------------|---------|
| | IN | OUT | IN | OUT | IN | OUT | VEL R | MACH NO |
| 1 | 0.421 | 0.366 | 0.421 | 0.366 | 0.360 | 0.364 | 1.016 | 0.538 |
| 2 | 0.443 | 0.378 | 0.443 | 0.378 | 0.394 | 0.376 | 0.961 | 0.483 |
| 3 | 0.448 | 0.381 | 0.448 | 0.381 | 0.399 | 0.380 | 0.957 | 0.476 |
| 4 | 0.436 | 0.379 | 0.436 | 0.379 | 0.380 | 0.379 | 1.000 | 0.500 |
| 5 | 0.409 | 0.354 | 0.409 | 0.354 | 0.345 | 0.354 | 1.028 | 0.493 |
| 6 | 0.406 | 0.319 | 0.406 | 0.319 | 0.334 | 0.319 | 0.961 | 0.489 |
| 7 | 0.392 | 0.275 | 0.392 | 0.275 | 0.316 | 0.274 | 0.874 | 0.466 |
| 8 | 0.389 | 0.246 | 0.389 | 0.246 | 0.309 | 0.245 | 0.801 | 0.472 |
| 9 | 0.378 | 0.221 | 0.378 | 0.221 | 0.285 | 0.220 | 0.779 | 0.504 |

| RP | PERCENT | INCIDENCE | | DEV | D-FACT | EFF | LOSS COEFF | | LOSS PARAM | |
|----|---------|-----------|-----|-----|--------|-----|------------|-------|------------|-------|
| | SPAN | MEAN | SS | | | | TOT | PROF | TOT | PROF |
| 1 | 5.00 | 17.1 | 7.9 | 9.6 | 0.342 | 0. | 0.209 | 0.209 | 0.102 | 0.102 |
| 2 | 10.00 | 12.8 | 3.6 | 9.3 | 0.322 | 0. | 0.191 | 0.191 | 0.090 | 0.090 |
| 3 | 15.00 | 12.4 | 3.2 | 8.0 | 0.327 | 0. | 0.156 | 0.156 | 0.072 | 0.072 |
| 4 | 30.00 | 14.0 | 4.8 | 6.2 | 0.320 | 0. | 0.066 | 0.066 | 0.027 | 0.027 |
| 5 | 50.00 | 15.1 | 5.9 | 5.8 | 0.315 | 0. | 0.018 | 0.018 | 0.006 | 0.006 |
| 6 | 70.00 | 14.8 | 5.7 | 6.9 | 0.367 | 0. | 0.098 | 0.098 | 0.029 | 0.029 |
| 7 | 85.00 | 14.6 | 5.5 | 8.4 | 0.428 | 0. | 0.150 | 0.150 | 0.038 | 0.038 |
| 8 | 90.00 | 15.4 | 6.3 | 9.4 | 0.490 | 0. | 0.197 | 0.197 | 0.046 | 0.046 |
| 9 | 95.00 | 18.9 | 9.8 | 9.6 | 0.542 | 0. | 0.198 | 0.198 | 0.043 | 0.043 |

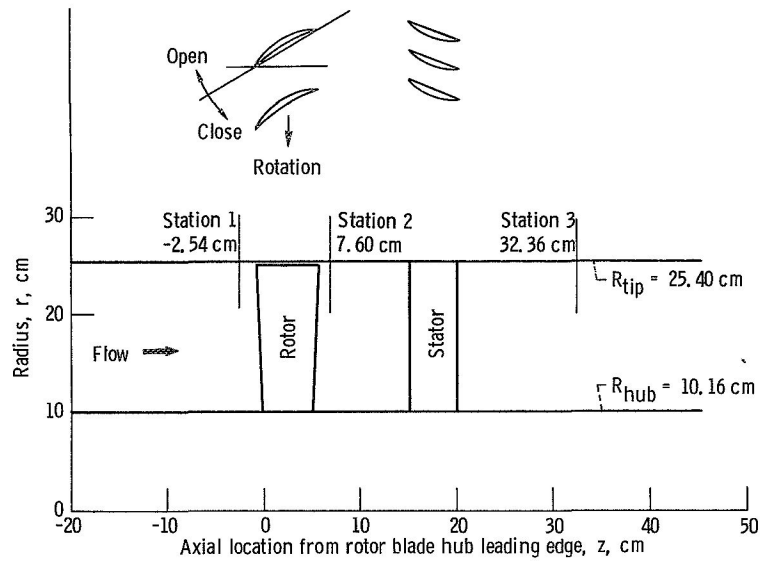


Figure 1. - Compressor flow path.

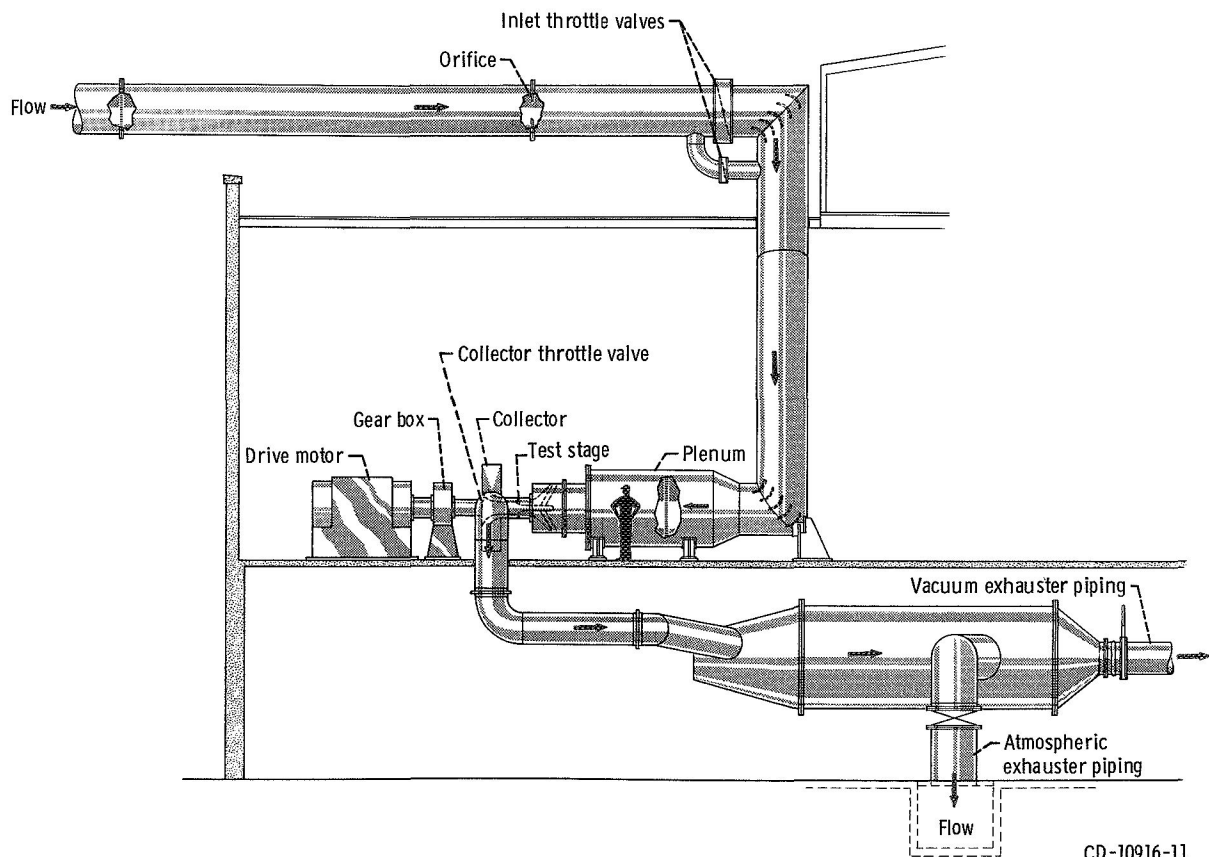


Figure 2. - Single-stage compressor facility.

CD-10916-11

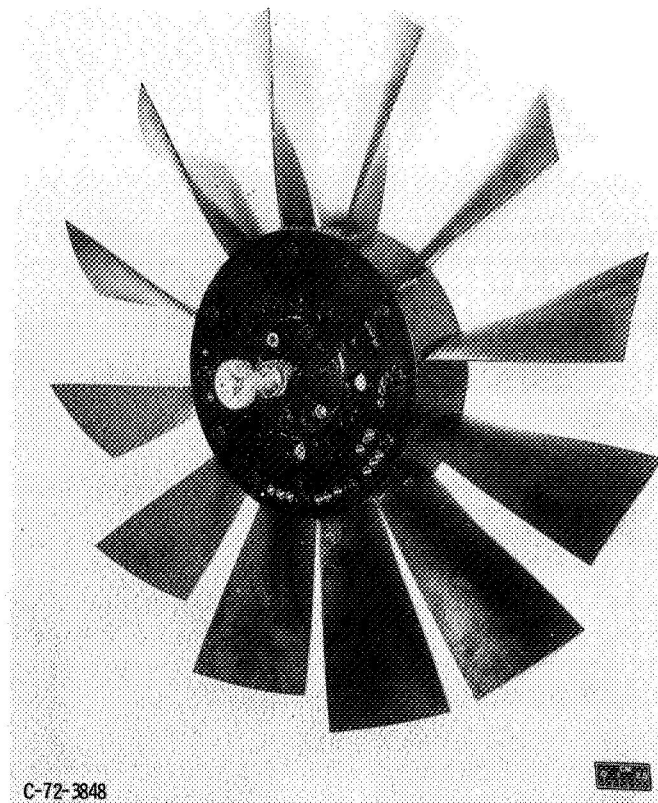


Figure 3. - Rotor 51B A.

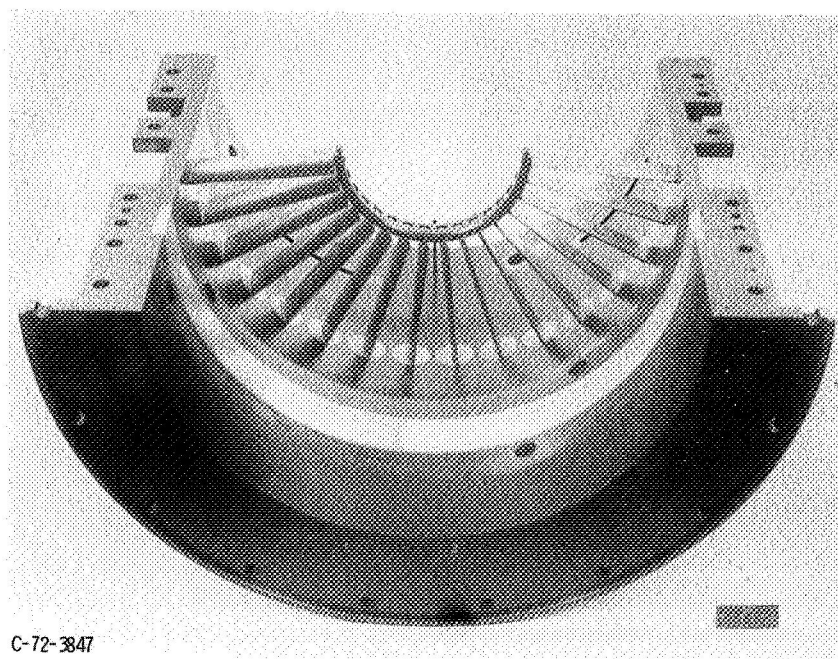
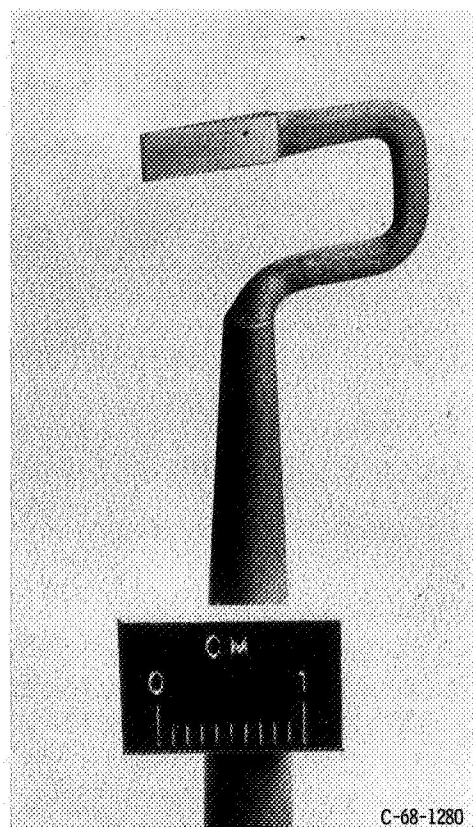


Figure 4. - Stator 51.



(a) Combination total pressure, total temperature, and flow angle probe.



(b) Static-pressure probe; 8° C-shaped wedge.

Figure 5. - Survey probes.

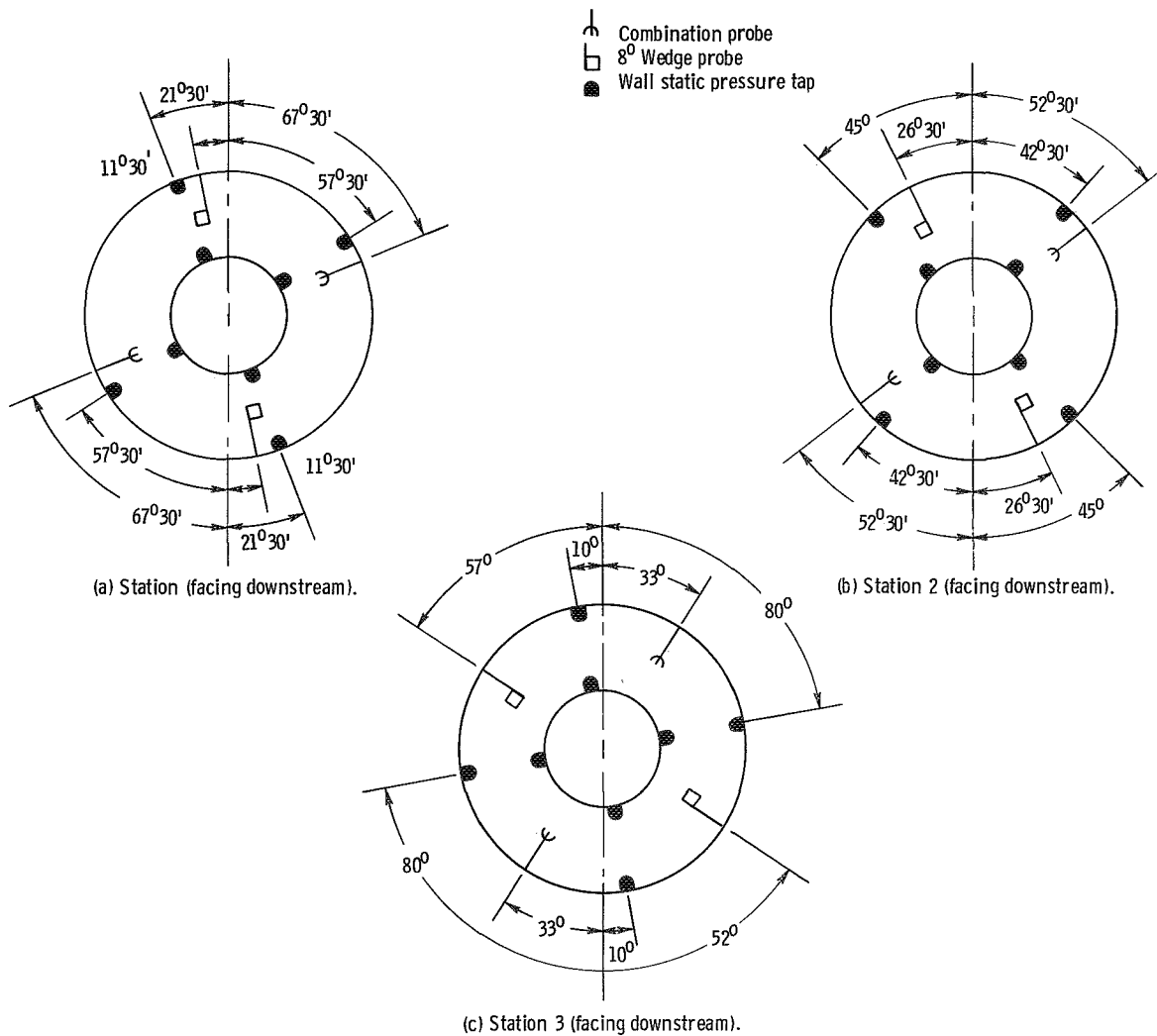
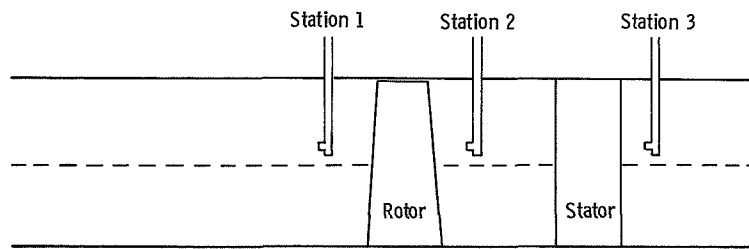


Figure 6. - Circumferential location of instrumentation.

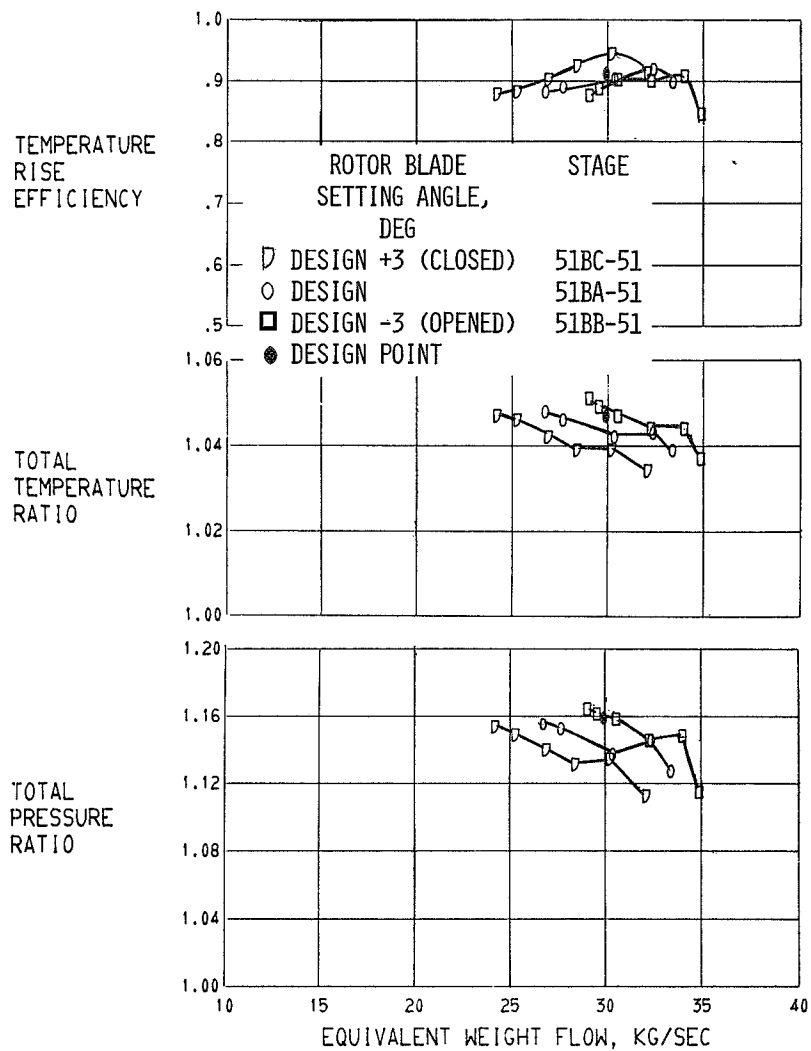


FIGURE 7. - OVERALL PERFORMANCE FOR ROTOR 51B FOR THREE ROTOR BLADE SETTING ANGLES AT 100 PERCENT DESIGN SPEED.

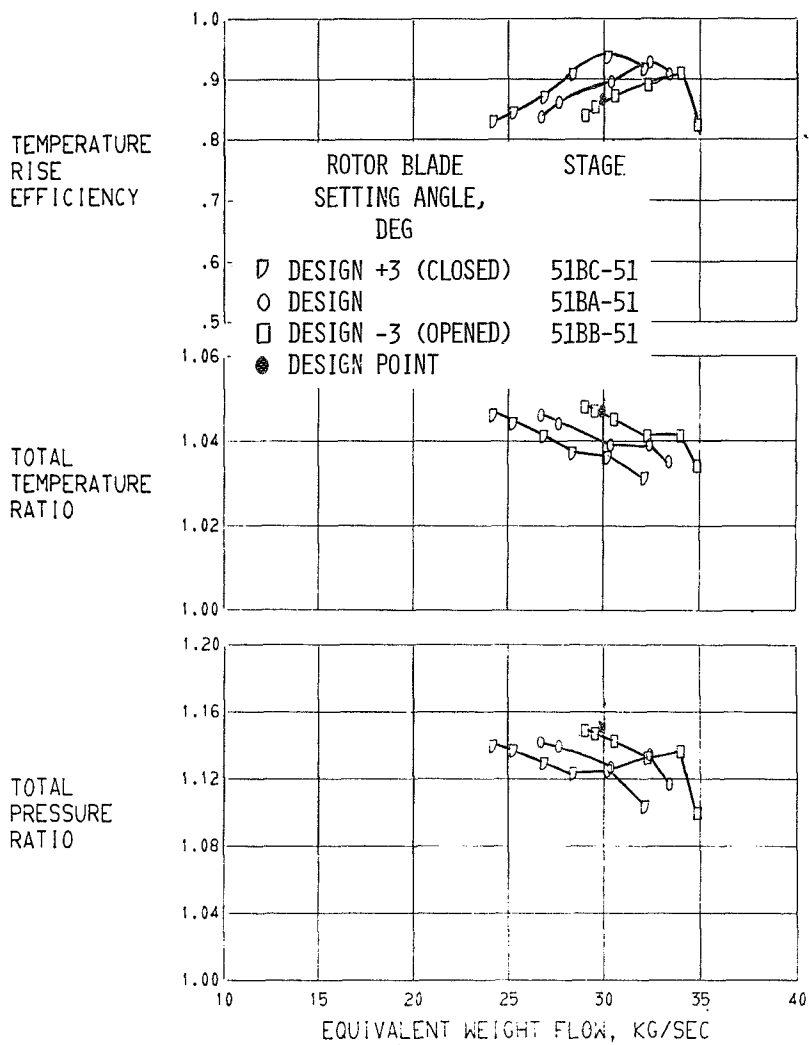
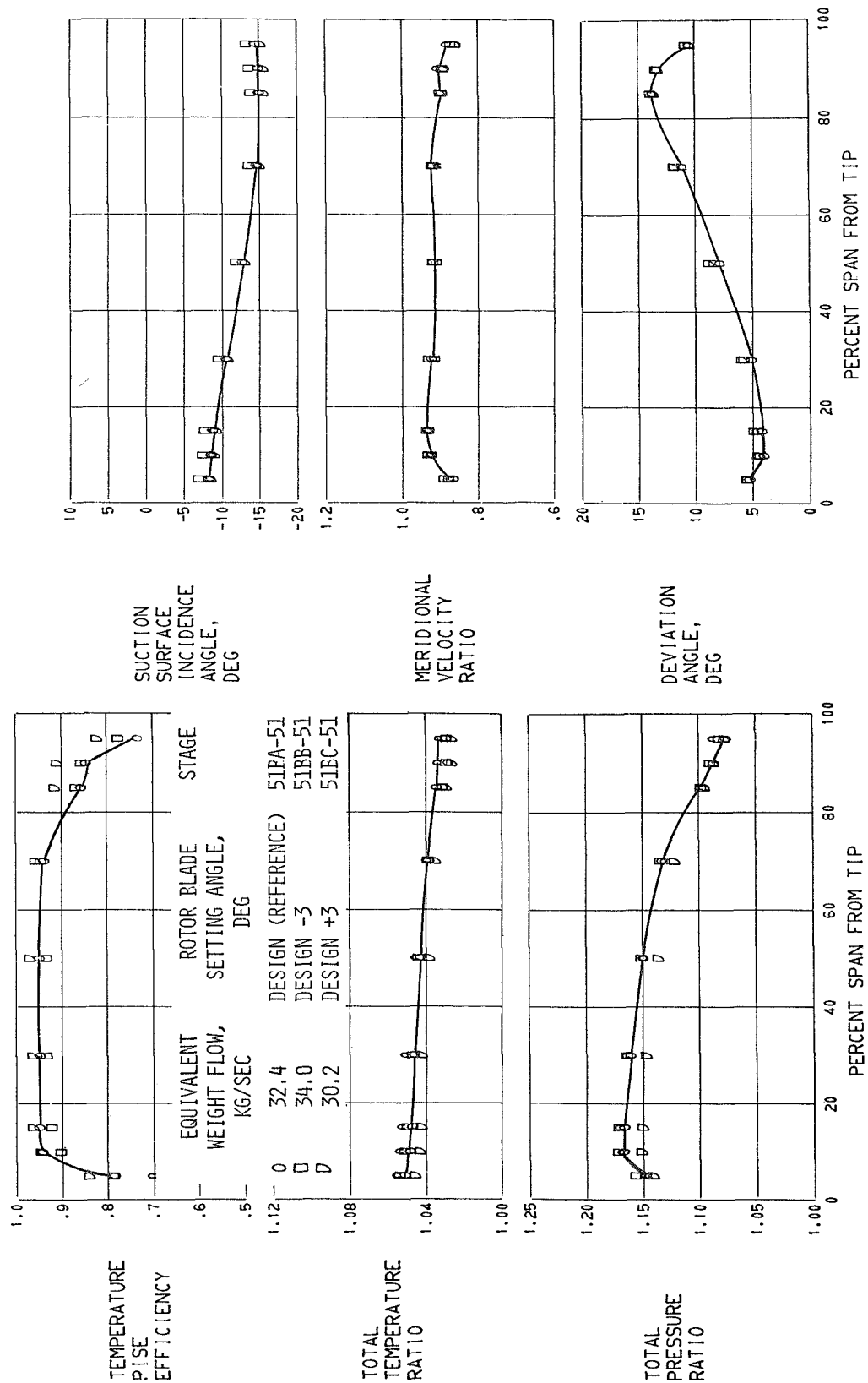


FIGURE 8. - OVERALL PERFORMANCE FOR STAGE 51B-51 FOR THREE ROTOR BLADE SETTING ANGLES AT 100 PER-CENT DESIGN SPEED.



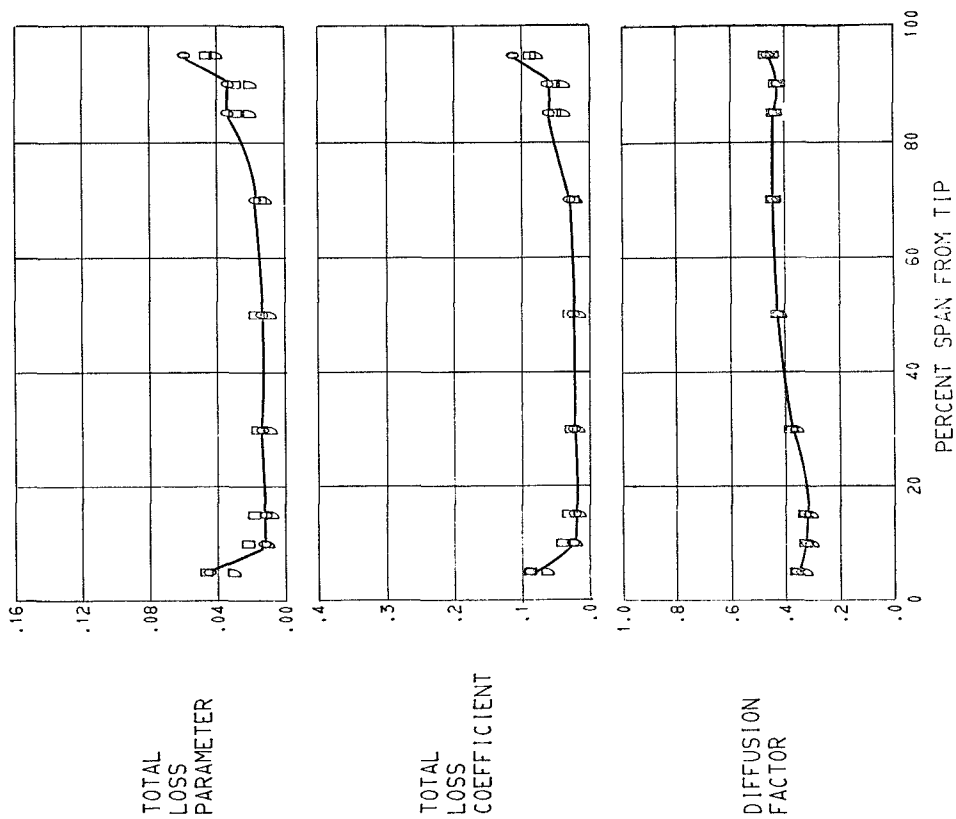


FIGURE 9. - RADIAL DISTRIBUTION OF PERFORMANCE FOR ROTOR 51B AT PEAK EFFICIENCY FOR THREE ROTOR BLADE SETTING ANGLES AT 100 PERCENT DESIGN SPEED.

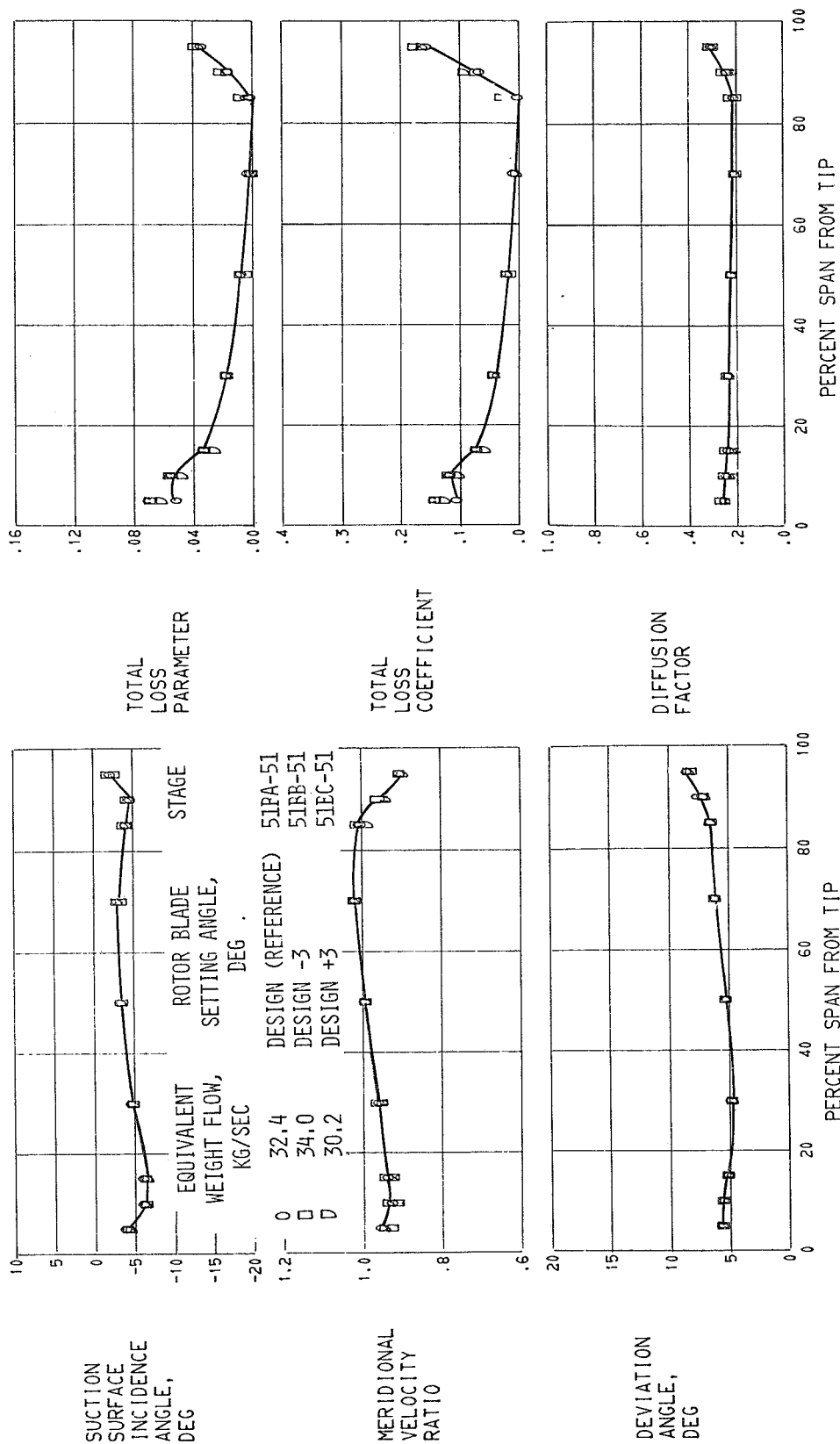
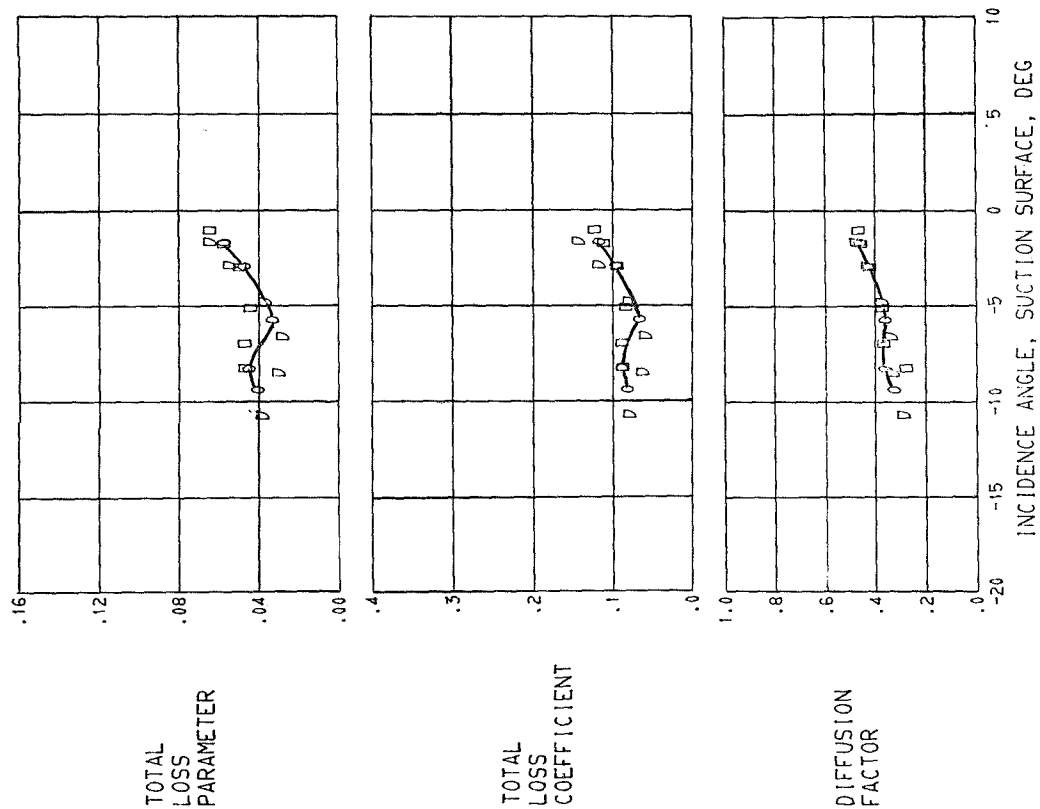
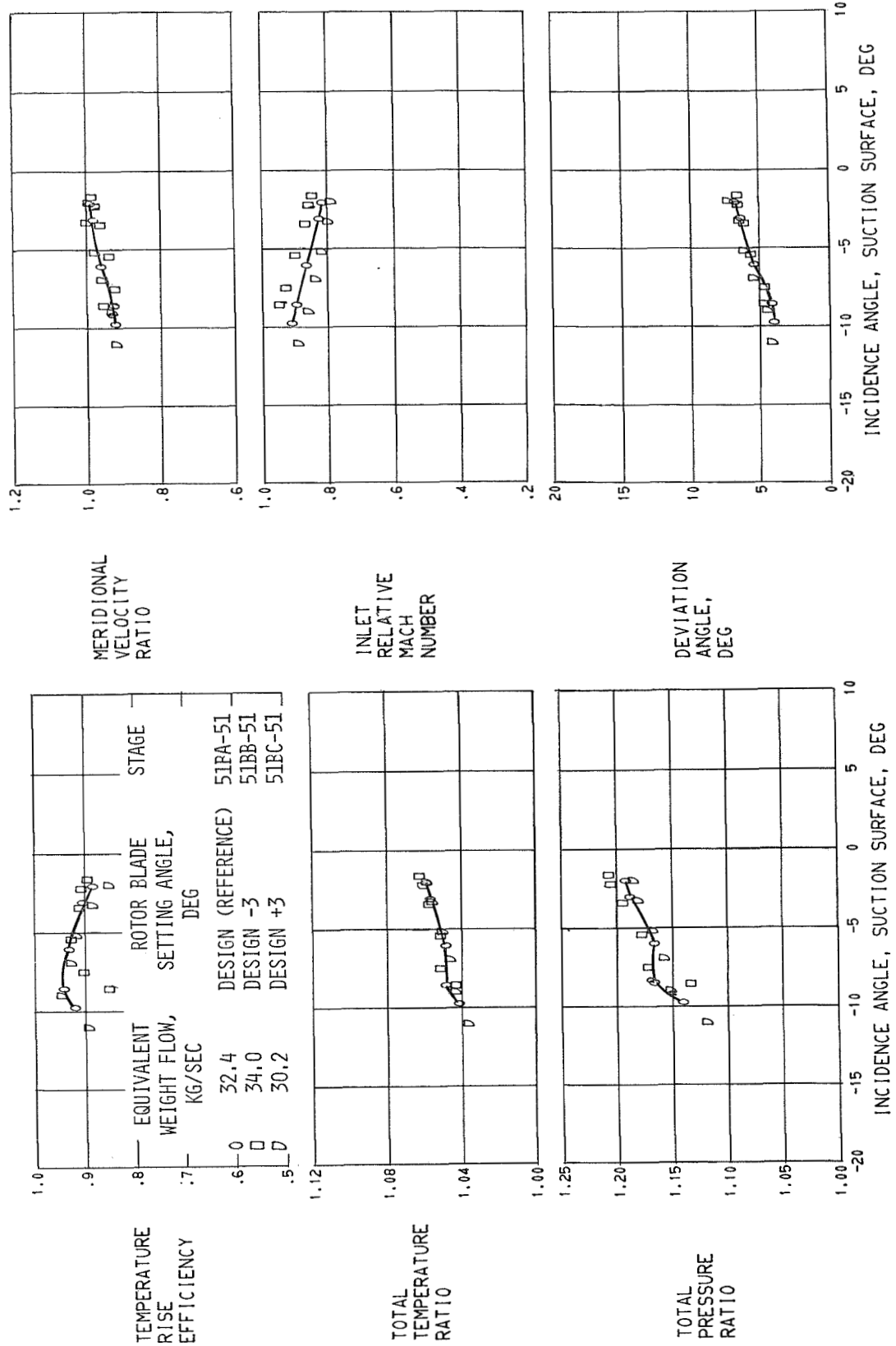


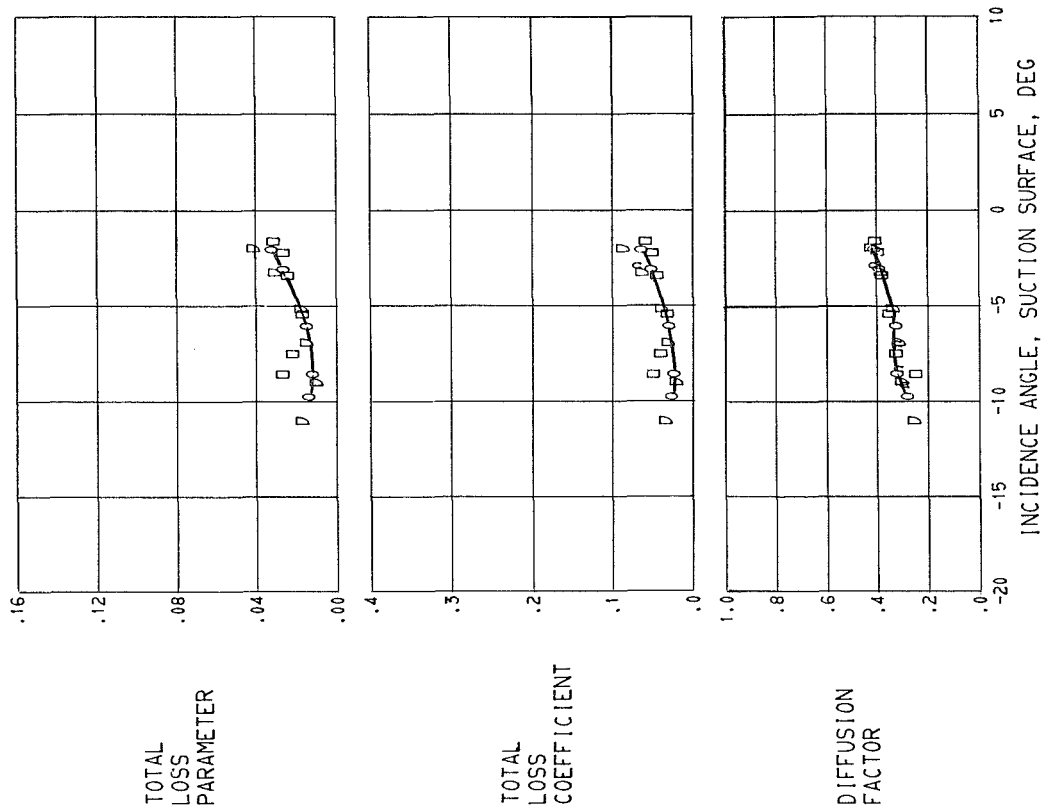
FIGURE 10. - RADIAL DISTRIBUTION OF PERFORMANCE FOR STATOR 51 AT PEAK EFFICIENCY FOR THREE ROTOR BLADE SETTING ANGLES AT 100 PERCENT DESIGN SPEED.



(A) 5.0 PERCENT SPAN.

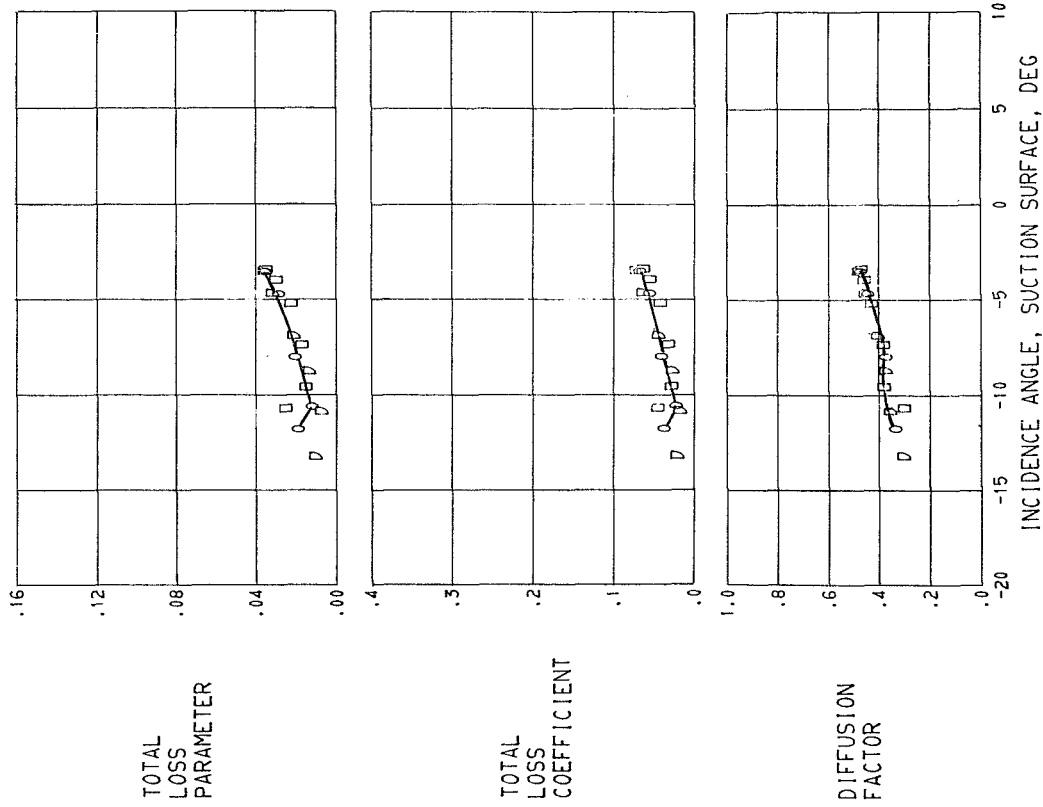
FIGURE 11. - BLADE-ELEMENT PERFORMANCE FOR ROTOR 51P FOR THREE ROTOR PLADE SETTING ANGLES AT 100 PERCENT DESIGN SPEED.





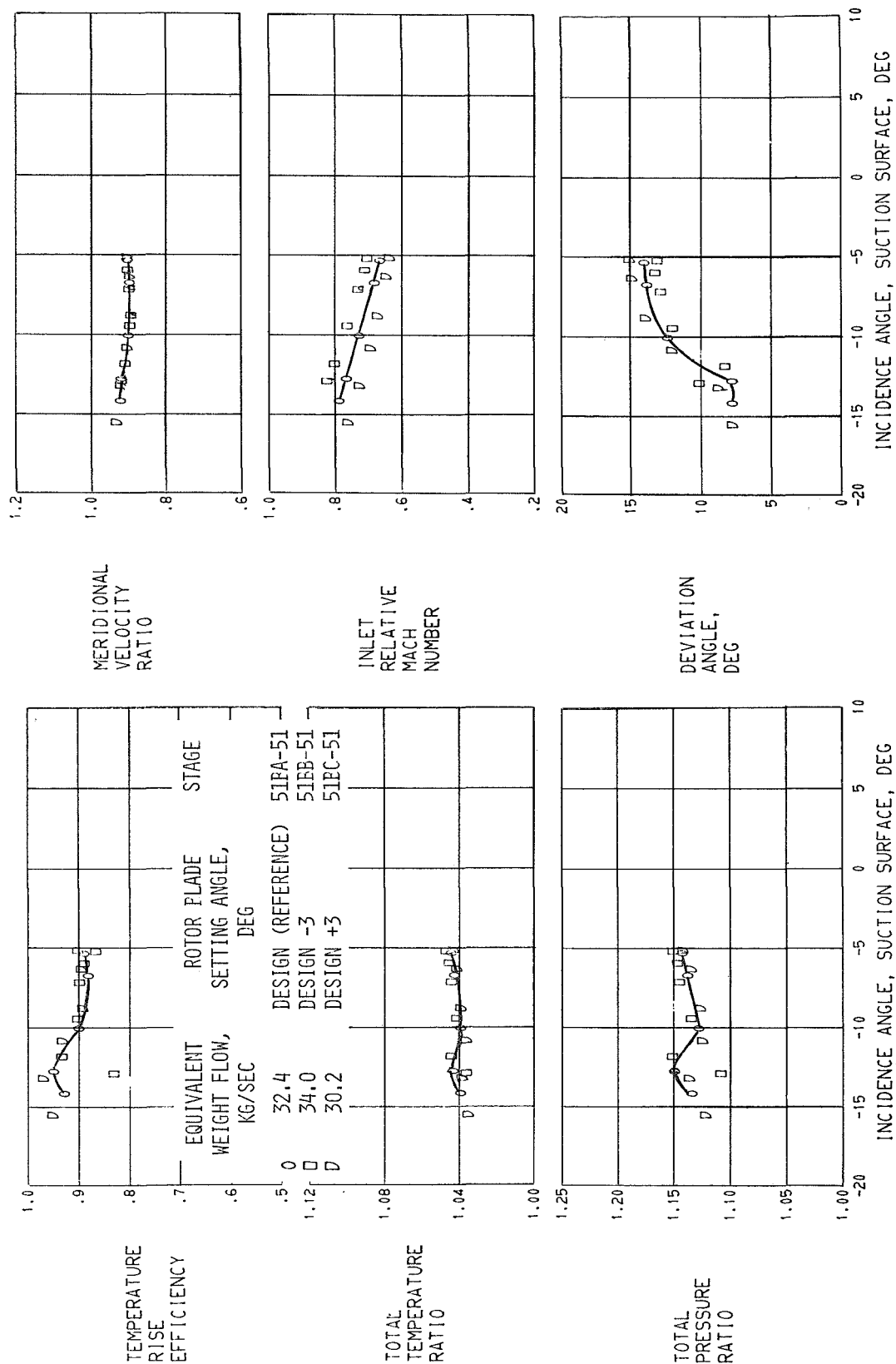
(B) 10.0 PERCENT SPAN.

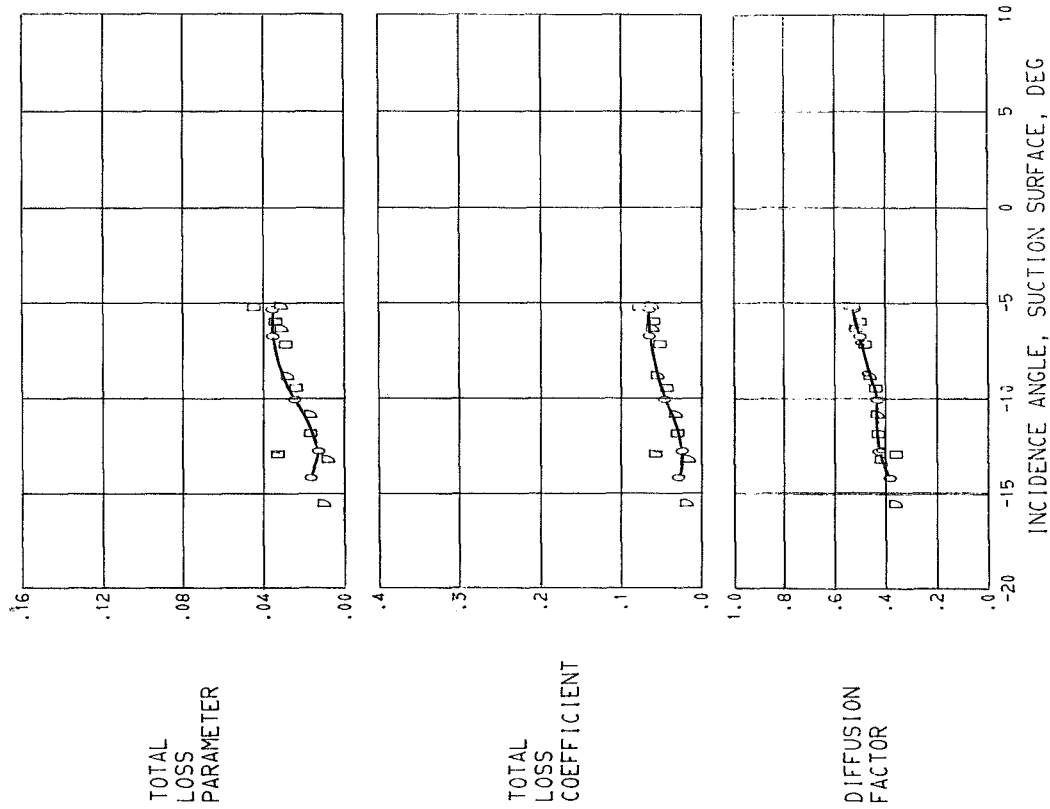
FIGURE 11. - CONTINUED.



(C) 30.0 PERCENT SPAN.

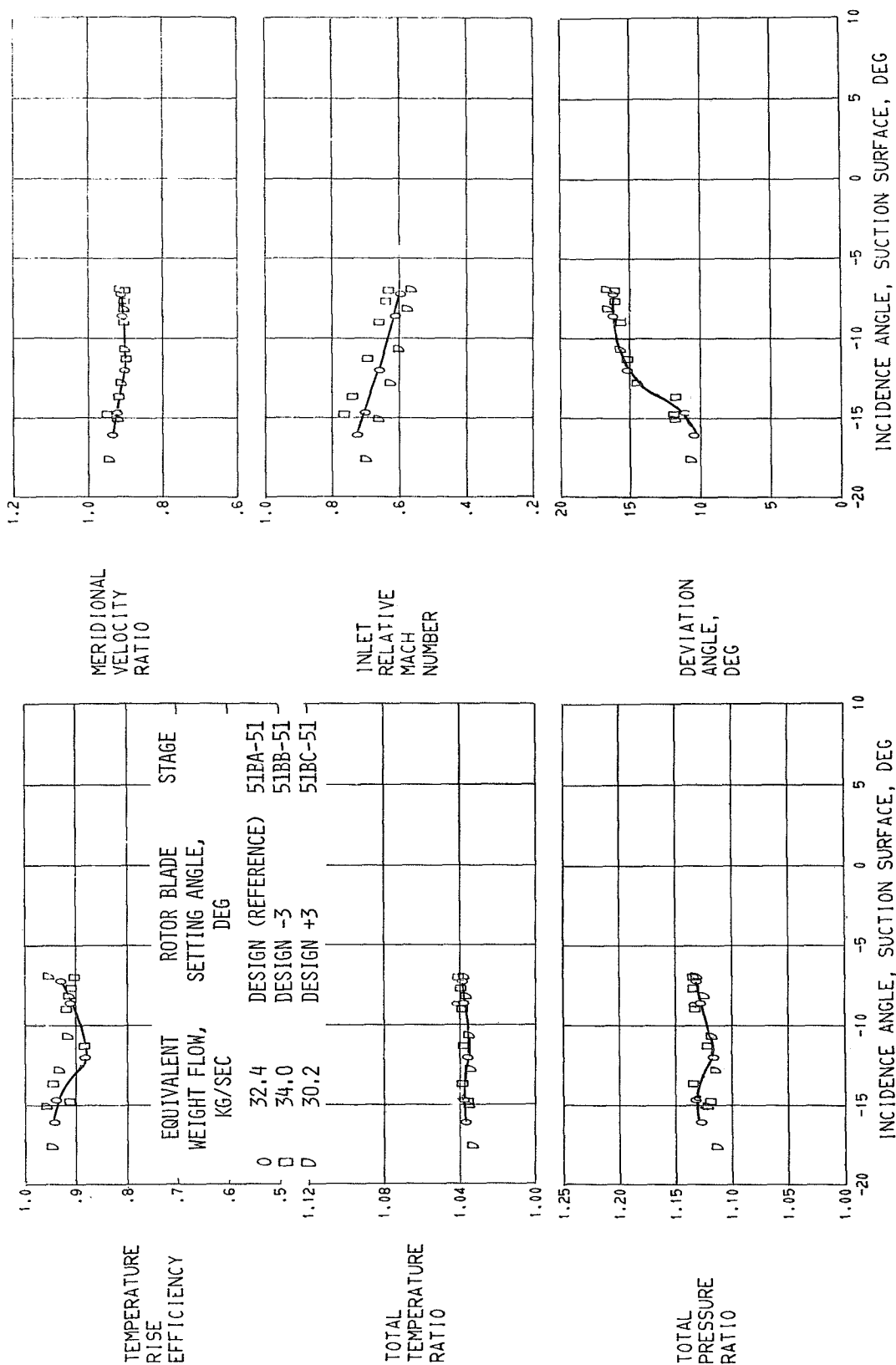
FIGURE 11. - CONTINUED.

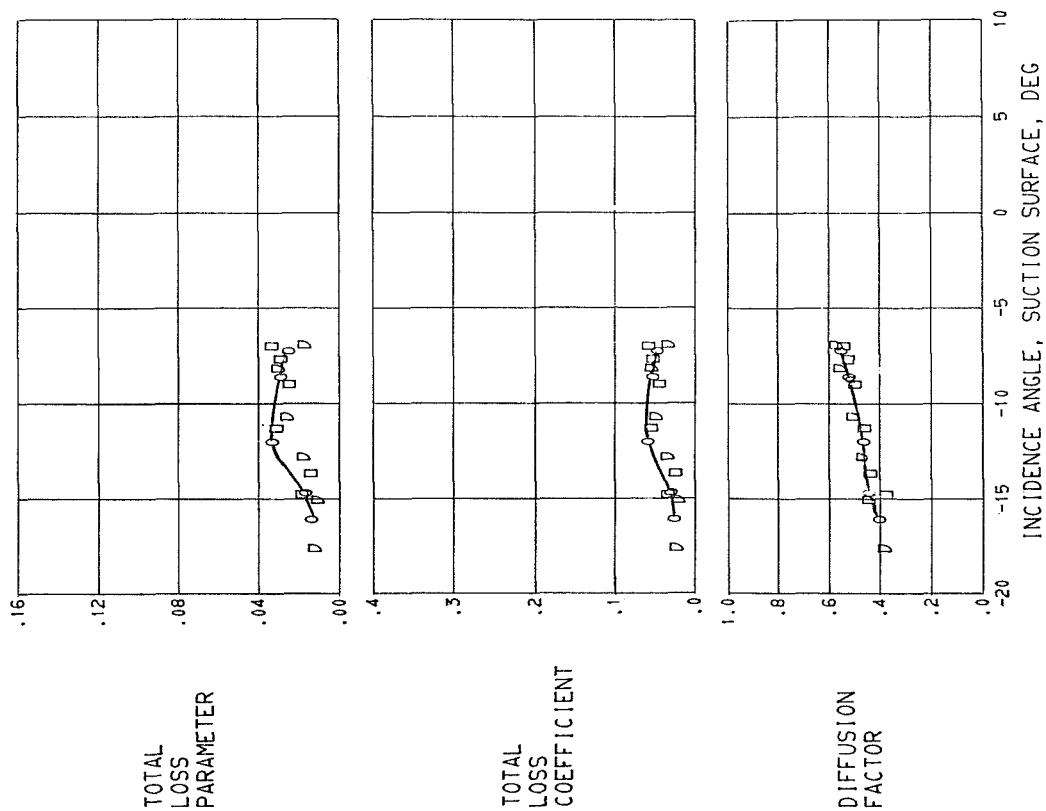




(D) 50.0 PERCENT SPAN,

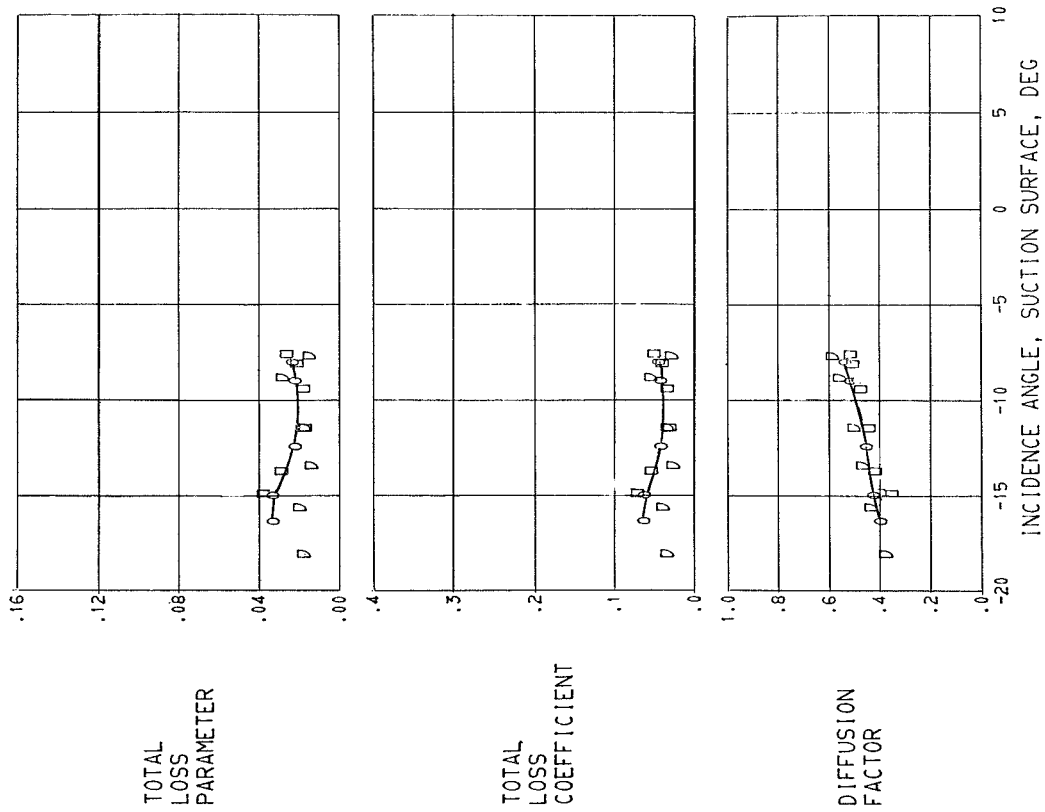
FIGURE 11. - CONTINUED.





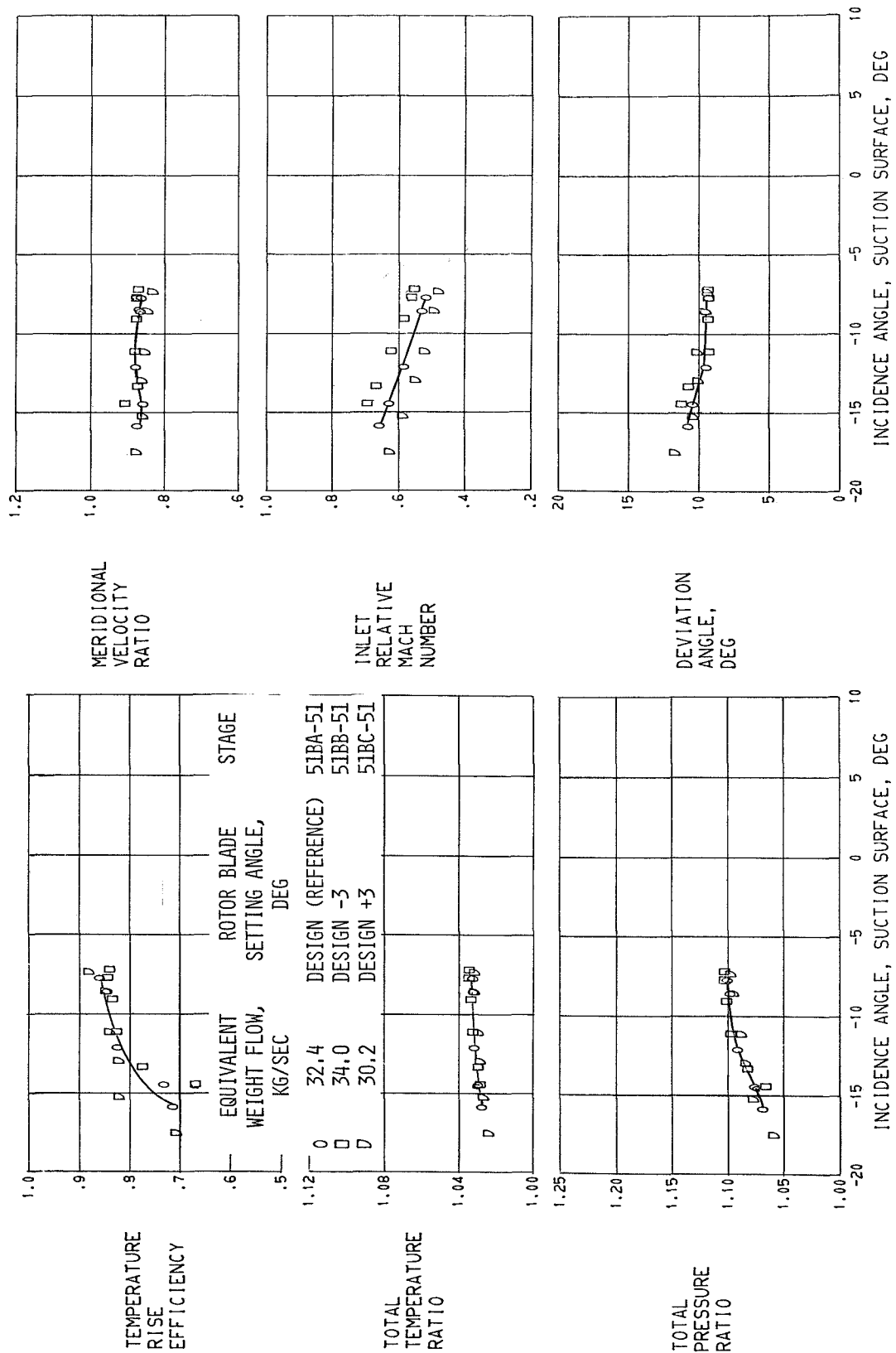
(E) 70.0 PERCENT SPAN.

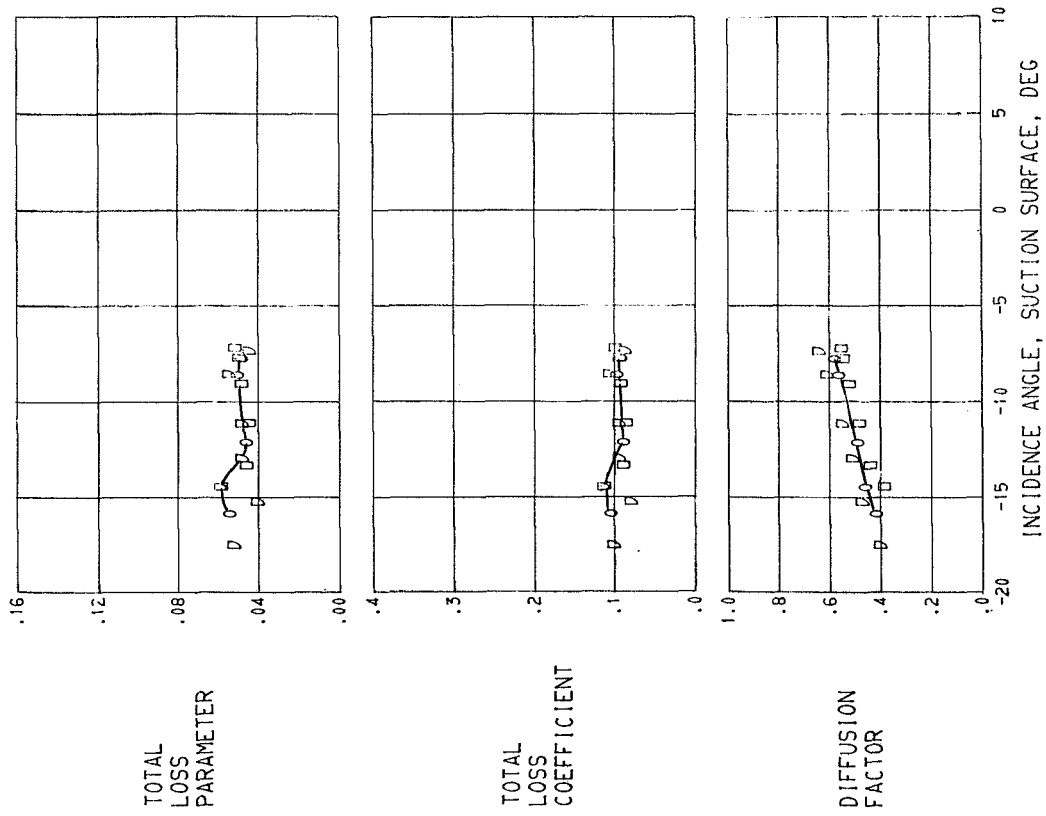
FIGURE 11. - CONTINUED.



(F) 90.0 PERCENT SPAN.

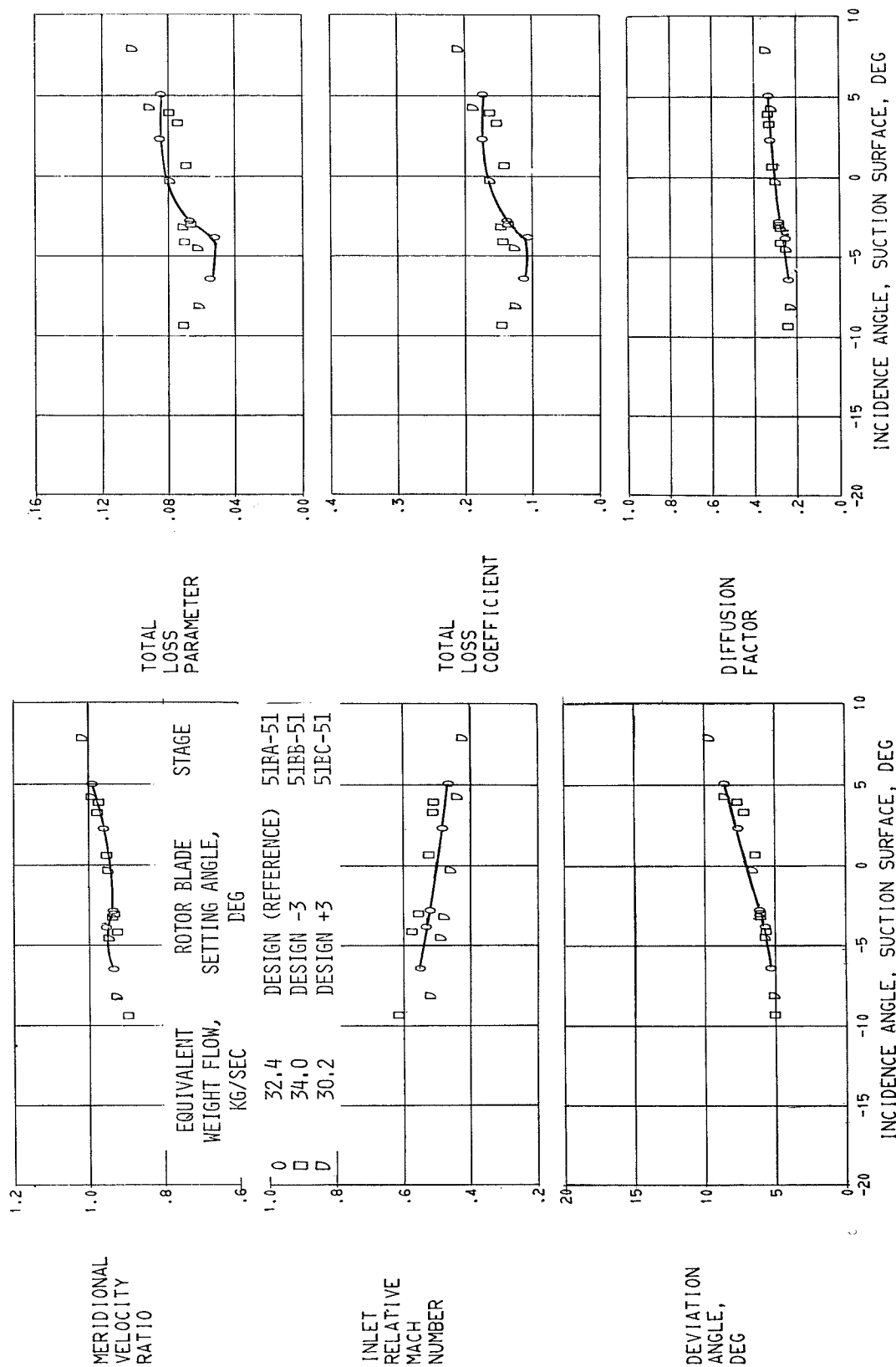
FIGURE 11, - CONTINUED.





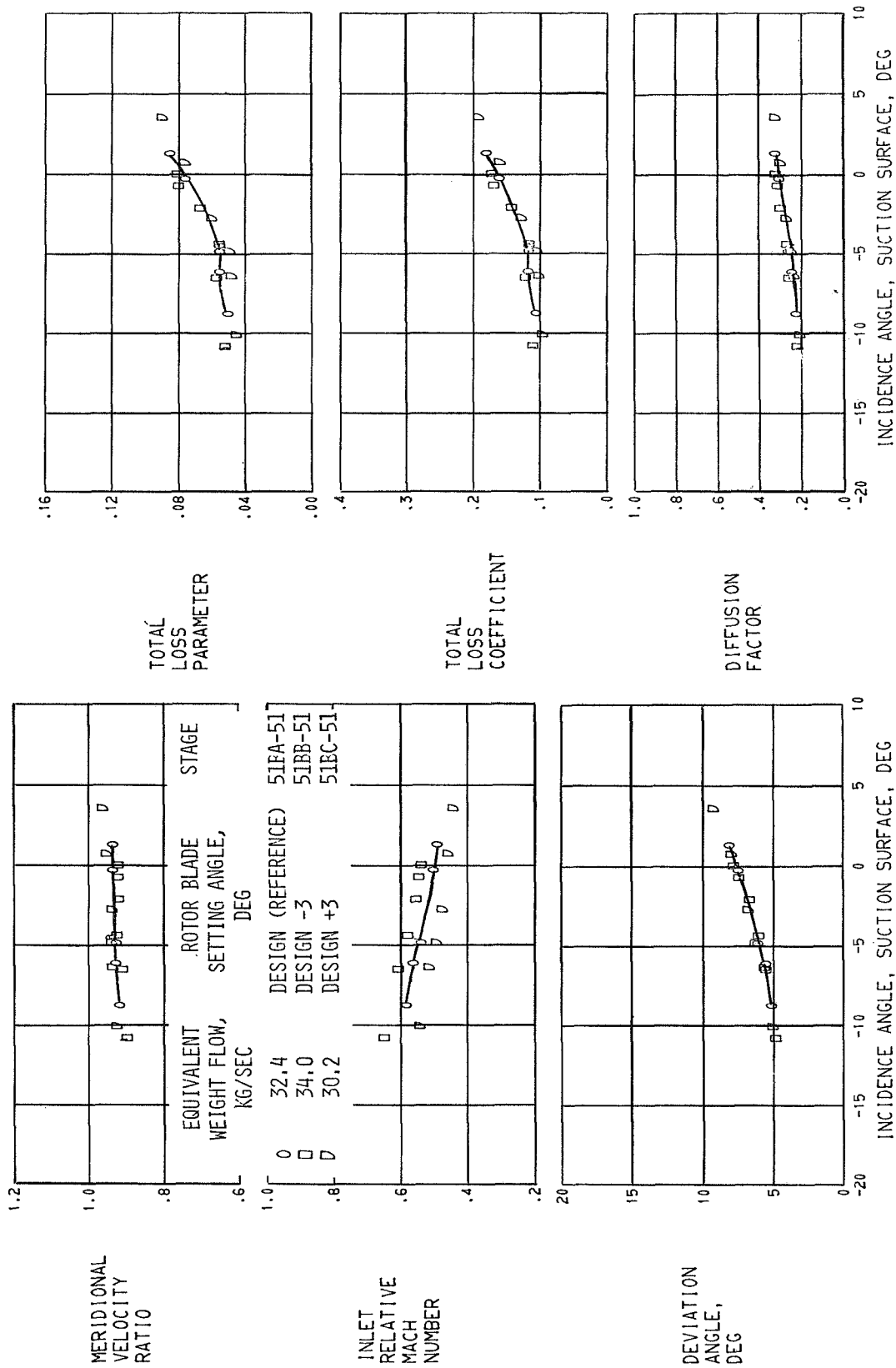
(G) 95.0 PERCENT SPAN.

FIGURE 11. - CONCLUDED.



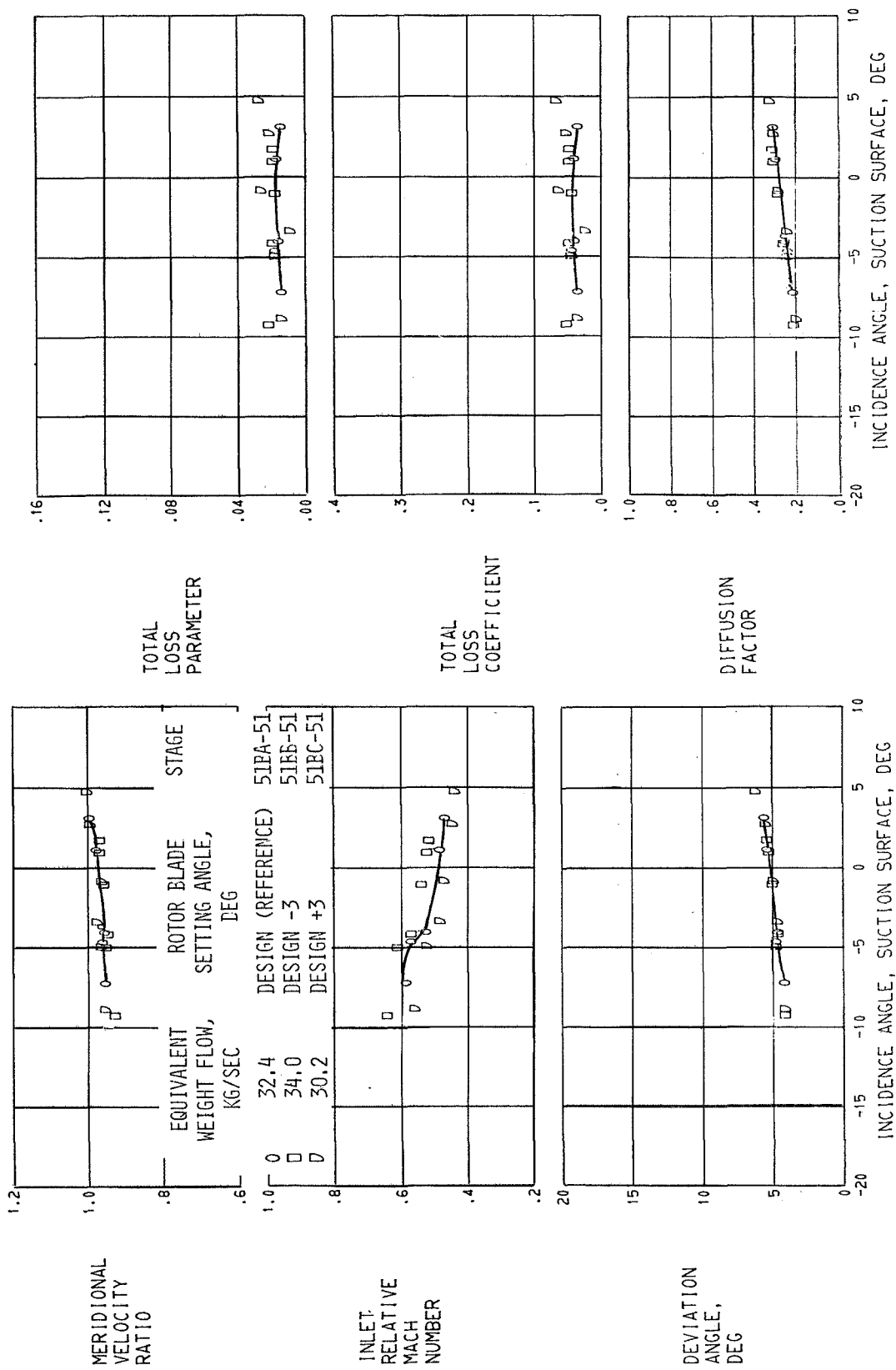
(A) 5.0 PERCENT SPAN.

FIGURE 12. - BLADE-ELEMENT PERFORMANCE FOR STATOR 51 FOR THREE ROTOR BLADE SETTING ANGLES AT 100 PERCENT DESIGN SPEED.



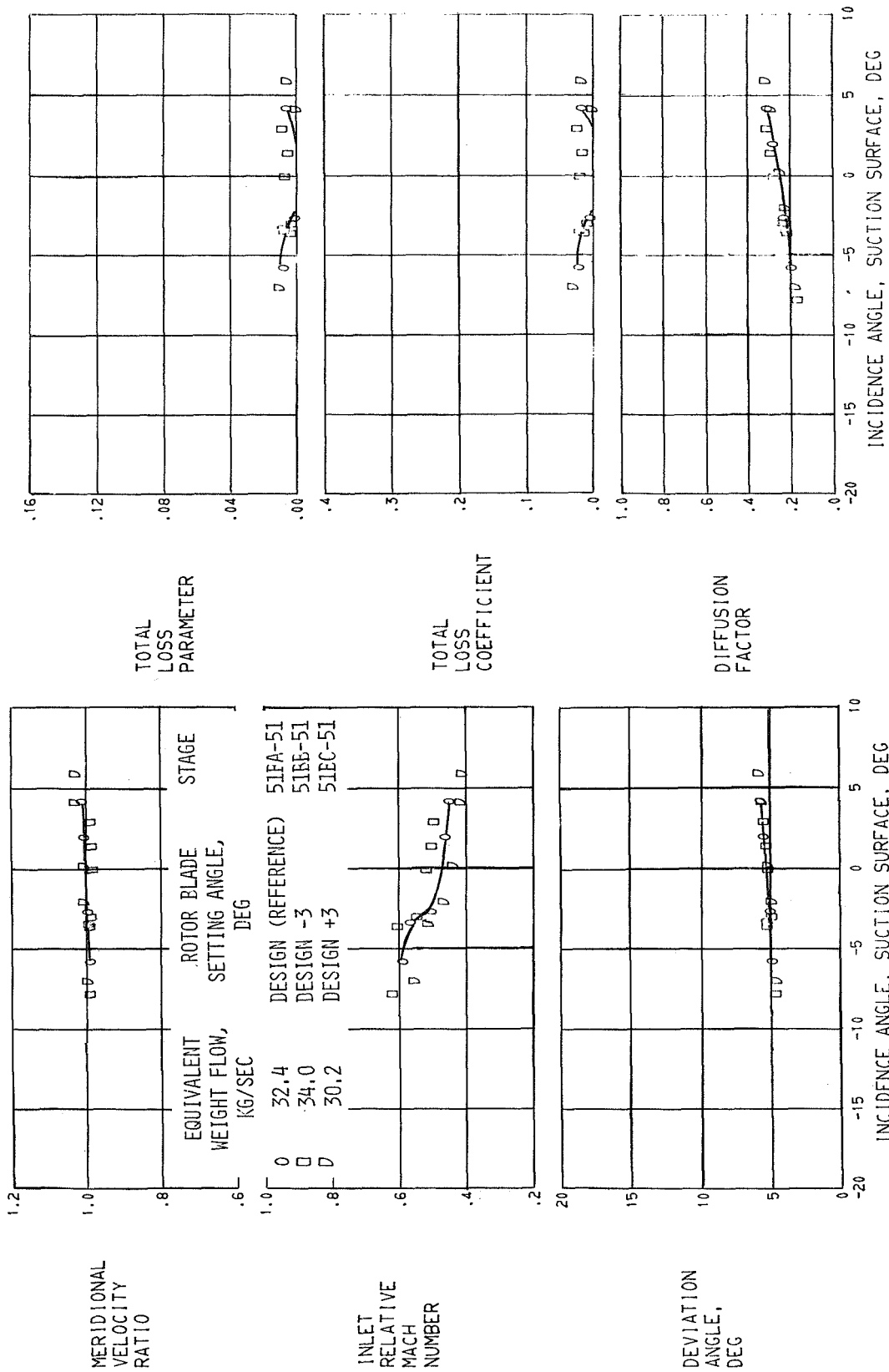
(B) 10.0 PERCENT SPAN.

FIGURE 12. - CONTINUED.



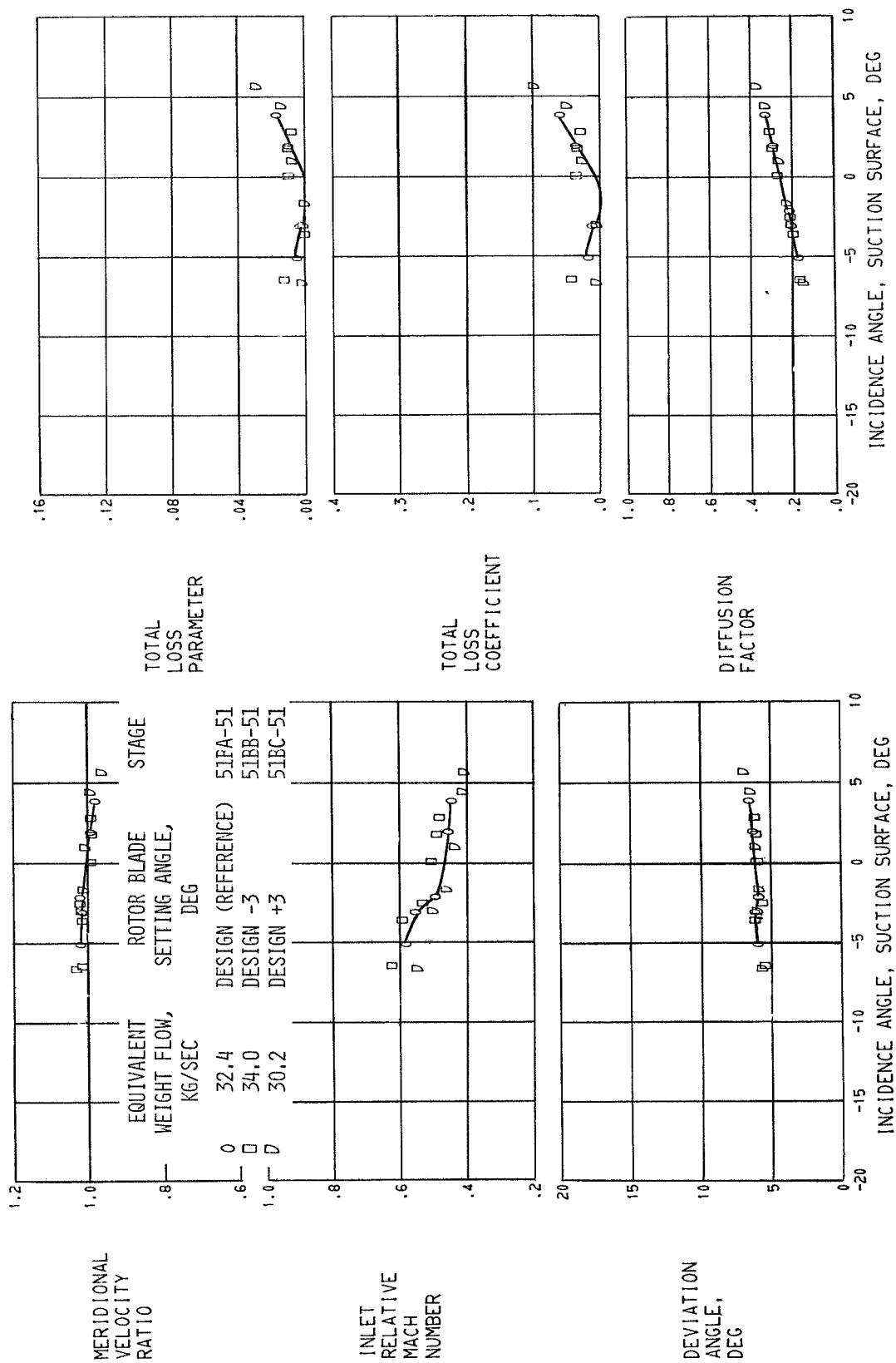
(C) 30.0 PERCENT SPAN.

FIGURE 12. - CONTINUED.



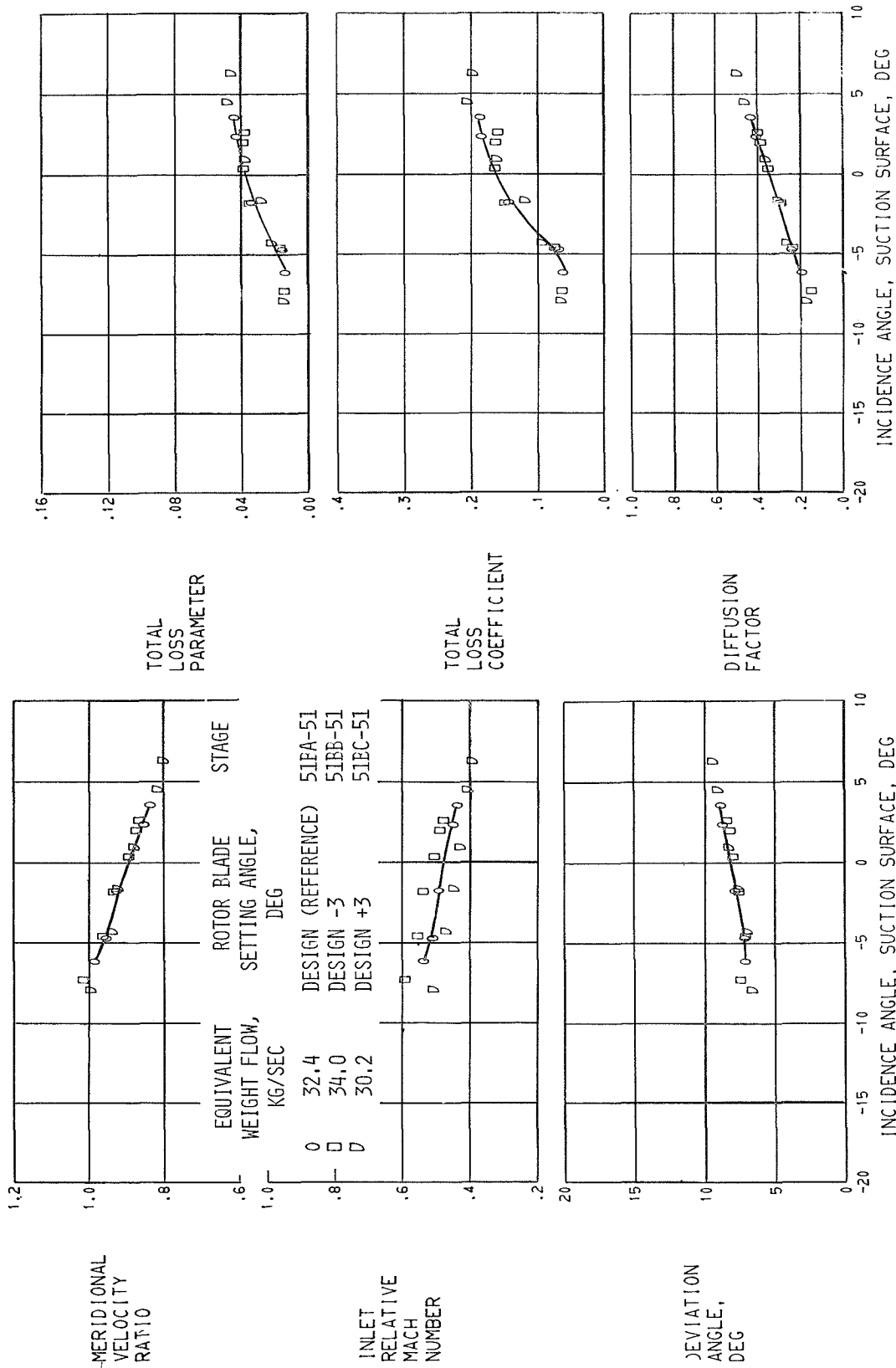
(D) 50.0 PERCENT SPAN.

FIGURE 12. - CONTINUED.

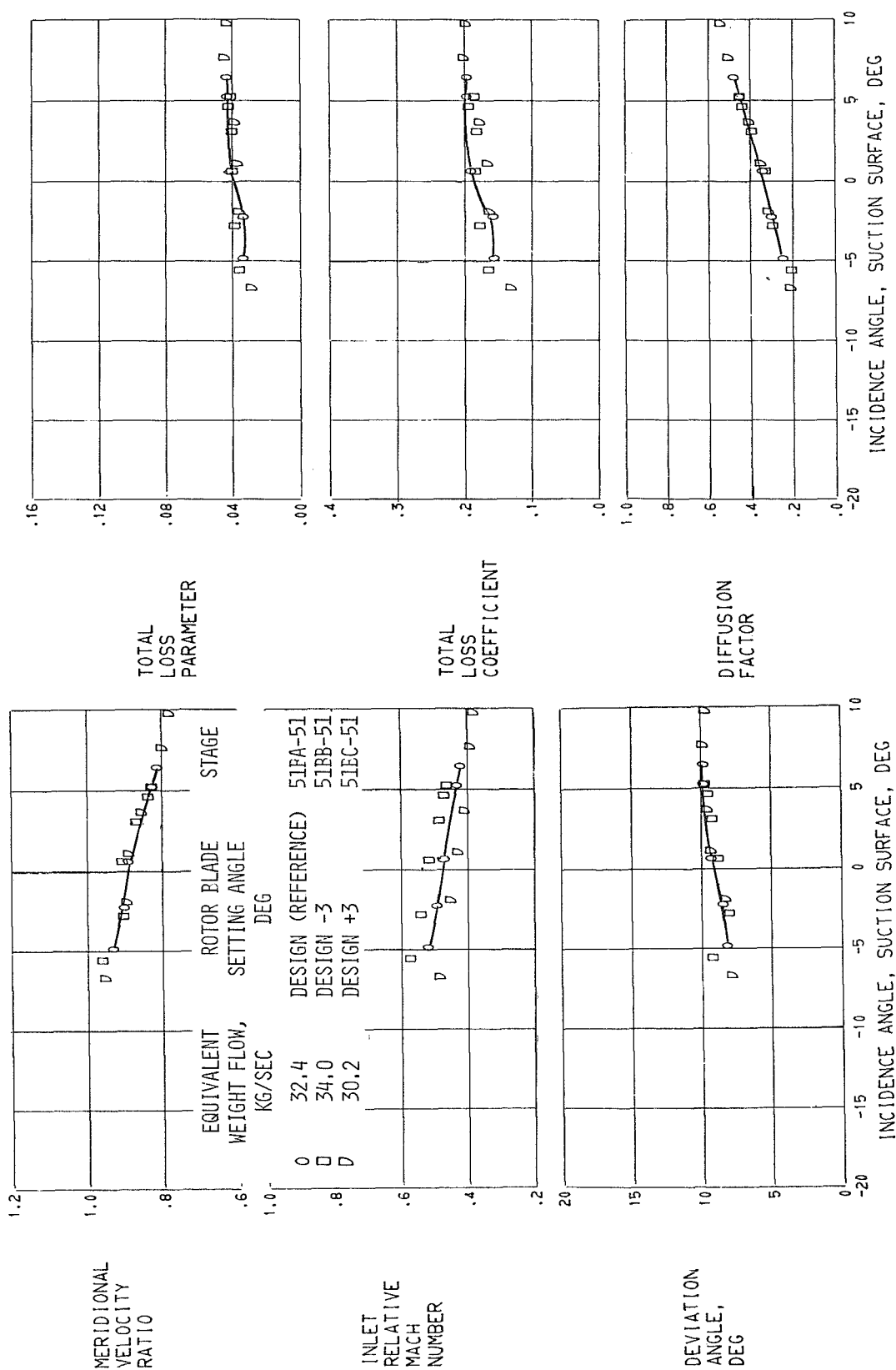


(E) 70.0 PERCENT SPAN.

FIGURE 12. - CONTINUED.



(F) 90.0 PERCENT SPAN,
FIGURE 12. - CONTINUED.



(G) 95.0 PERCENT SPAN.

FIGURE 12. - CONCLUDED.

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